# 2018 LIMITED SCOPE SUPPLEMENTAL DRAFT ENVIRONMENTAL IMPACT STATEMENT <br> And Section 4(f) Evaluation 

Submitted Pursuant to 42 U.S.C. 4332 (2)(c) and 49 U.S.C. 303
By the
U.S. Department of Transportation

Federal Highway Administration
and
Wisconsin Department of Transportation
COOPERATING AGENCY
U.S. Army Corps of Engineers (pursuant to 33 CFR 230)


FHWA will issue a single Limited Scope Supplemental Final Environmental Impact Statement and Record of Decision document pursuant to 23 U.S.C. 139(n)(2) unless FHWA determines statutory criteria or practicability considerations preclude issuance of the combined document pursuant to Section 139.

## ABSTRACT

Wisconsin Highway 23 is part of the National Highway System (NHS) and is a rural principal arterial that connects Fond du Lac and Sheboygan in east central Wisconsin. Both west and east ends of the project are located in the growing urban areas of Fond du Lac and Plymouth. 19.1 miles in length, this highway corridor serves high traffic volumes near the urban areas and lower traffic volumes in rural areas. This document evaluates the No-Build Alternative, several Build Alternatives, and a series of corridor preservation alternatives for future transportation improvements. The Preferred Alternative reconstructs WIS 23 to a 4-lane divided highway on the existing alignment and creates interchanges, connector roads, and a trail. The Preferred Alternative also includes corridor preservation for future transportation improvements.

FHWA and WisDOT have prepared this Limited Scope Supplemental Draft Environmental Impact Statement (LS SDEIS) in accordance with 23 CFR 771.130. This LS SDEIS:

- Evaluates new and changed impacts to the human and natural environment since the 2014 LS SFEIS.
- Updates and explains the methodology used to develop traffic forecasts.
- Explains the role of demographic data in traffic forecasts.
- Reviews the evaluation of reasonable alternatives.

Comments on this Limited Scope Supplemental Draft Environmental Impact Statement are due by July 31, 2018 or 60 days after the Notice of Availability is published in the Federal Register, whichever is later, and should be sent to:

## NATIONAL ENVIRONMENTAL POLICY ACT STATEMENT

The National Environmental Policy Act (NEPA), 42 USC 4321-4347, became effective January 1, 1970. This law requires that all federal agencies have prepared for every recommendation or report on proposals for legislation and other major federal actions significantly affecting the quality of the human environment a detailed Environmental Impact Statement (EIS). The Federal Highway Administration (FHWA) is therefore required to have prepared an EIS on proposals that are funded under its authority if the proposal is determined to be a major action significantly affecting the quality of the human environment.

EISs are required for many transportation projects as outlined in NEPA. This Limited Scope Supplement Draft Environmental Impact Statement will follow the same procedure as a normally prepared EIS. The processing of an EIS is carried out in two stages. Draft EISs are first written and forwarded for review and comment to federal, state, and local agencies with jurisdiction by law or special expertise and are made available to the public. This availability to the public must occur at least 15 days before the public hearing and no later than the time of the first public hearing notice or notice of opportunity for a hearing. Normally, 45 days plus mailing time will be allowed for comments to be made on the Draft EIS unless a time extension is granted by the Bureau of Technical Services (Wisconsin Department of Transportation). Supplemental Draft EISs are prepared whenever there are changes, new information, or further developments on a project that result in significant environmental impacts not identified in the most recently distributed version of the DEIS [23 CFR 771.130]. They have the same review period and hearing requirements as a Draft EIS. After this period has elapsed for a Draft EIS or Supplement Draft EIS, preparation of the Final EIS can begin. The Final EIS includes:

1. Basic content of the Draft Statement (or Supplemental Draft Statement), as amended, due to internal agency comments, editing, additional alternatives being considered, and changes due to the time lag between the Draft, Supplemental Draft, and Final EIS.
2. Summary of public hearing environmental comments.
3. Copies of comments received on the Draft Statement or Supplemental Draft Statement.
4. Evaluation and disposition of each substantive comment.

The Draft, Supplemental Draft, and Final EIS are full-disclosure documents, which provide a full description of the proposed project, the existing environment, and an analysis of the anticipated beneficial or adverse environmental effects.

The name, address, and telephone number of the individual from whom additional information can be obtained is listed on the cover of this document.

## GENERAL REVIEWER INFORMATION

A gray box provided at the beginning of each section provides an introduction to the section and describes what has changed since the 2014 LS SFEIS


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# TECHNICAL MEMORANDUM 

To: Bryan Lipke P.E. - Wisconsin Department of Transportation, Northeast Region
Jennifer Murray, AICP - Wisconsin Department of Transportation, Forecasting
Dawn Krahn, P.E. - Wisconsin Department of Transportation, Bureau of State Highway Programs
From: Thomas W. Lynch, P.E., PTOE
Joseph M. Urban, P.E.
Strand Associates, Inc. ${ }^{\circledR}$
Date: May 11, 2018
Re: ID 1440-13/15-00
Fond du Lac to Plymouth
WIS 23
Fond du Lac and Sheboygan Counties
DHV for WIS 23 Evaluation
May 11, 2018 update: The statistical analysis and recommendations included in this memorandum were completed in September 2017 and were documented in the October 5, 2017 version of this memorandum. WisDOT reviewed and approved the recommendations in the October 5, 2017 memorandum. Updates to this memorandum have been made to reflect changes in the WisDOT FDM implemented on March 16, 2018, to reflect the date of the most current traffic forecasts (April 6, 2018) for the study, and to expand on the background section.

## Background

This memorandum documents evaluation of traffic data used to develop inputs for the traffic operations analysis within the Wisconsin State Highway (WIS) 232018 Limited Scope Supplemental Environmental Impact Statement (LS SEIS) project limits. The study limits are the US Highway 151 (US 151)/WIS 23 interchange on the west end and County P/Pioneer Road (County P) on the east end. The corridor is mostly a 2-lane rural highway, with relatively short stretches of 4-lane highway on both ends of the corridor. The traffic analysis for this study focuses on the two-lane highway portion of the corridor from County UU to County P, which is nearly 18 miles long.

This memo focuses on a review of hourly traffic characteristics of roadways near the WIS 23 corridor and provides a recommendation for a K value and directional distribution (DD) factor to determine the Design Hour Volume (DHV). Also reviewed is traffic count data, truck percentage data, Peak Hour Factor (PHF), and the analysis software to use for the traffic analysis. More information on other traffic modeling inputs are located in the Traffic Modeling Methodology memorandum in Appendix A of the 2018 LS SEIS.

The DHV is a design criterion used to design roadway improvements with an appropriate traffic volume. The DHV was developed to promote roadway designs that provide a reasonable Level of Service (LOS) for the majority of the hours within the year. An appropriate DHV is chosen to avoid "Over Building" a roadway to accommodate traffic demands that occur only a few hours of every year.

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According to the WisDOT Facilities Development Manual (FDM), Section 11-5-3.5.1.1, it is WisDOT policy to use the 30 th highest hour volume (K30) as the DHV for both multilane highways and rural two-lane facilities. The FDM further states:
"There may be unique circumstances where K30 is not realistic to use because of exceptionally high hourly volume peaking characteristics. These conditions may occur on routes with a higher level of recreational traffic or routes that are in close proximity to a stadium, seasonal shopping mall or other special event traffic generator. A higher design hour may be justified when the LOS using the 30th highest hour cannot be achieved because of social and environmental constraints, or if the project is financially cost prohibitive."

When higher design volumes are justified, the FDM states that LOS evaluation should also consider the 100th highest hour (K100) for rural or small to medium urban areas and the 200th (K200) or 250th highest hour (K250) for highly urbanized areas ( $>200,000$ population) with heavy daily traffic but that the Federal Highway Administration (FHWA) must approve deviations from the K30 design hour on interstate projects.

In the summer of 2017 , traffic counts were performed by WisDOT along the WIS 23 study corridor. However, this data does not provide yearly data for use in determining the DHV. There are two continuous count sites, or Automatic Traffic Recorders (ATRs), near the study corridor that could be considered to determine the DHV. The FDM 11-5-3.5.1.1 states:

The design hour evaluation should be made by analyzing the traffic volume data from the most applicable continuous traffic count site locations.

Figure 1 illustrates the study corridor and the two most applicable ATRs that were available to provide data regarding regional travel peaking characteristics.


Figure 1 ATRs used for Review

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## Methodology

The study took the following steps in its review:

1. Review 2016 ATR traffic profile data for peaking characteristics. Weekday (Monday through Thursday), Friday, and Sunday peaking characteristics are reviewed. This review helps identify the type of traffic using WIS 23, commuter, recreational, or both.
2. Review 2016 ATR data for hourly ranking. For each ATR the 30th and 100th highest hour in each direction is identified, and the corresponding non-peak direction is obtained. From these values a K value and DD is developed.
3. Provide recommendations for K value, and DD to use in the operations analysis.
4. Review hourly turning movement counts to identify the PHF that currently exists for the morning and evening peak hours.
5. Provide recommendations for which PHF to use in the operations analysis.
6. Review available truck data from roadway counts and WIS 23 ATR.
7. Provide recommendations on truck percentages to use in the operations analysis.

## Area Background

The 19.1-mile WIS 23 study corridor is largely a rural corridor that connects two metropolitan urban areas, Fond du Lac and Sheboygan. The Fond du Lac core urban statistical area amounts to about 101,600 while the Sheboygan core urban statistical area amounts to $115,500 .{ }^{1}$ I-41 is a major northsouth corridor that connects the Fond du Lac area to Milwaukee and the Fox Valley and Green Bay. I-43 is a major north-south corridor that serves the Sheboygan area and connects it to Milwaukee and Green Bay. WIS 23 is one of the few, higher mobility, roadways that travel east-west through the region connecting these two interstate highways.

Peak traffic hours for I-41 and I-43 are affected by special events in Green Bay, specifically Packer games. They also provide access to summer vacation destinations in northern Wisconsin, including the Door County peninsula. WIS 23 does not provide a direct route to Green Bay and therefore Packer games probably have a more limited effect. WIS 23 provides access to the two urban areas. It also provides access to, and therefore is influenced by, recreational destinations in the Sheboygan area and Lake Michigan lakefront. These recreational areas include Kohler's Blackwolf Run golf course, Whistling Straights golf course, Kohler-Andreas state park, and Elkhart Lake Road America race track.

The two ATRs being used for this review are located on I-41 (201305) west of the corridor, and on WIS 23 (590608) east of the corridor, as shown in Figure 1.

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## Hourly Volume Profile

Figure 2 illustrates the hourly volume profile for the I-41 ATR site in both the northbound and southbound directions during the summer months. The grey line shows typical commuting patterns with morning and evening rush hour peaks. The dashed orange and blue lines indicate there is a recreational component for I-41 traffic. This is illustrated by the large northbound movement on Friday evenings, and large southbound movement on Sunday afternoons.


Figure 2 I-41 Traffic Volume Profile - Summer Months (ATR 201305)
Figure 3 illustrates the hourly volume profile for the WIS 23 ATR site in each direction of travel during the summer months. It has a distinctly different profile from that of the I-41 profile. The Friday profile essentially matches the profile of the weekday traffic. And the Sunday volume profile is less pronounced.


Figure 3 WIS 23 Traffic Volume Profile - Summer Months (ATR 590608)

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For reasons previously stated, the study team believes that the WIS 23 ATR provides a better representation of traffic characteristics in the WIS 23 study corridor.

## Hourly Volume Ranking

Three types of hourly ranking for K30 and K100 are provided for the two ATR sites. The I-41 ATR site uses 342 days of data in $2016^{2}$ for analysis, with an AADT volume of 44,446 vehicles per day (vpd). The WIS 23 ATR uses 356 days of data in $2016^{3}$ for the analysis. The I-41 ATR had the following 2016 AADT:

| Southbound | $22,218 \mathrm{vpd}$ |
| :--- | :--- |
| Northbound | $22,228 \mathrm{vpd}$ |
| Two-way | $44,446 \mathrm{vpd}$ |


| I-41 Northbound Peak Hours |  |  |  |
| :---: | :---: | :---: | :---: |
| K30 |  | K100 |  |
| $\begin{gathered} \hline \text { Friday } 7 / 1 / 16, \\ 7 \mathrm{pm} \\ \hline \end{gathered}$ | 2,929 vph NB | $\begin{gathered} \hline \text { Friday } 7 / 1 / 16, \\ 5 \mathrm{pm} \\ \hline \end{gathered}$ | 2,552 vph NB |
|  | 900 vph SB |  | 1,657 vph SB |
| Total | $3,829 \mathrm{vph}$ | Total | 4,209 vph |
| Percent of NB <br> AADT | 13.18 | Percent of NB <br> AADT | 11.48 |
| Percent of twoway AADT | 8.61 | Percent of twoway AADT | 9.47 |
| DD | 77/23 | DD | 61/39 |
| Beginning of a three-day summer holiday weekend |  | Beginning of a three-day summer holiday weekend |  |
| I-41 Southbound Peak Hours |  |  |  |
| K30 |  | K100 |  |
| Sunday $7 / 31 / 16$, 12 noon | $2,087 \mathrm{vph} \mathrm{NB}$ | $\begin{gathered} \text { Monday } 9 / 5 / 16, \\ 6 \mathrm{pm} \\ \hline \end{gathered}$ | 953 vph NB |
|  |  |  | 2,404 vph SB |
| Total | 4,901 vph | Total | 3,357 vph |
| Percent of SB AADT | 12.67 | Percent of SB AADT | 10.82 |
| Percent of twoway AADT | 11.03 | Percent of twoway AADT | 7.55 |
| DD | 57/43 | DD | 72/28 |
| Packer Family Night |  | End of a three-day summer holiday weekend |  |

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| I -41 Combined Peak Hours |  |  |  |
| :---: | ---: | :---: | ---: |
| K30 |  | K100 |  |
| Friday $4 / 29 / 16, ~$ <br> 4 pm | $2,729 \mathrm{vph} \mathrm{NB}$ | Sunday $8 / 7 / 16$, | $1,714 \mathrm{vph} \mathrm{NB}$ |
|  | $2,221 \mathrm{vph} \mathrm{SB}$ | 2 pm | $2,831 \mathrm{vph} \mathrm{SB}$ |
| Total | $4,950 \mathrm{vph}$ | Total | $4,545 \mathrm{vph}$ |
| Percent of two- <br> way AADT | 11.14 | Percent of two- <br> way AADT | 10.23 |
| DD | $55 / 45$ | DD | $62 / 38$ |

The WIS 23 ATR had the following 2016 AADT:

| Westbound | $11,802 \mathrm{vpd}$ |
| :--- | :--- |
| Eastbound | $12,131 \mathrm{vpd}$ |
| Two-way | $23,933 \mathrm{vpd}$ |


| K30 |  | K100 |  |
| :---: | :---: | :---: | :---: |
| Thurs 12/15/16, | 1,555 vph EB | Thurs 1/28/16, | 1,495 vph EB |
| 7 am | 704 vph WB | 7 am | 643 vph WB |
| Total | $2,259 \mathrm{vph}$ | Total | 2,138 vph |
| Percent of EB AADT | 12.82 | Percent of EB AADT | 12.32 |
| Percent of twoway AADT | 9.44 | Percent of twoway AADT | 8.93 |
| DD | 69/31 | DD | 70/30 |
| Winter Weekday |  | Winter Weekday |  |


| WIS 23 Westbound Peak Hours |  |  |  |
| :---: | :---: | :---: | :---: |
| K30 |  | K100 |  |
| Sat 6/8/16, | 1,375 vph WB | Weds 4/13, | 1,325 vph WB |
| 4 pm | 896 vph EB | 4 pm | 938 vph EB |
| Total | 2,271 vph | Total | 2,263 vph |
| Percent of WB AADT | 11.65 | Percent of WB <br> AADT | 11.23 |
| Percent of twoway AADT | 9.49 | Percent of twoway AADT | 9.46 |
| DD | 61/39 | DD | 59/41 |
|  |  | Weekday |  |

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| WIS 23 Combined Peak Hours |  |  |  |
| :---: | :---: | :---: | :---: |
| K30 |  | K100 |  |
| $\begin{gathered} \text { Fri } 12 / 9 / 16, \\ 4 \mathrm{pm} \\ \hline \end{gathered}$ | 1,000 vph EB | $\begin{gathered} \text { Weds } 11 / 16, \\ 4 \mathrm{pm} \end{gathered}$ | 1,014 vph EB |
|  | 1,403 vph WB |  | 1,326 vph WB |
| Total | 2,403 vph | Total | 2,340 vph |
| Percent of twoway AADT | 10.04 | Percent of twoway AADT | 9.78 |
| DD | 58/42 | DD | 57/43 |
| Weekend |  | Weekday |  |

For the WIS 23 ATR, both the peak direction and the combined direction K30 and K100 values are relatively close. The peak direction K30 and K100 had a half percent or less difference. The combined direction K30 and K100 had about a quarter percent difference. Additionally, the K30 and K100 hours do not correspond with typical recreational peak periods, with most of them occurring during a weekday. This suggests that WIS 23 has travel peaking characteristics that are more typical of a commuter route than a recreational route. Figure 4 graphically shows the hourly volume ranking (combined directions) for both I-41 and WIS 23. The shape of the curves illustrates the recreational/special event peaking characteristics of I-41 and the commuter characteristics of WIS 23.

For WIS 23, the peak direction K values may not be as applicable for operations analysis as the combined K value. Twolane operations analysis uses the nonpeak directional volume as it considers opportunities to pass. Therefore, the eastbound K30 and K100 directional distribution of 69/31 percent and 70/30 percent respectively may bias the effect estimate from the two-lane analysis. Conversely, the combined K30 and K100 provide directional distributions of 58/42 percent and $57 / 43$ percent, respectively. These values are likely to provide a better and more representative two-lane operational analysis.


Figure 4 Peak Hour Ranking

Because the WIS 23 ATR (590608) used for the analysis is outside of the study limits, hourly volume trends from sites within the study limits were compared to the ATR hourly volume trends for similar timeframes. The study reviewed four count sites, each of which are 48 -hour averages of weekdays in June 2017. ATR 590608 data from two weekdays in June 2016 was used to keep the datasets similar. The roadway counts used in this analysis are two-way volumes and were not factored or seasonally adjusted. Figure 5 shows the results of the ATR hourly volume vs. coverage count hourly volume comparison.

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Figure 5 WIS 23 Hourly Volume, ATR vs. Coverage Counts
The results of the ATR hourly volume vs. Coverage Count (i.e. the 48-hour roadway counts performed in June 2017) hourly volume comparison show that the counts within the study corridor are similar to the ATR during peak times (7-8 AM and 4-5 PM). The ATR hourly volume has more pronounced peaking characteristics, with volumes dropping to a greater amount between 9 AM to 12 PM. However, the difference in mid-day traffic trends are less important when considering the study's usage of the ATR data for the design hour volume. The study intends to use the ATR data to develop K30 and K100 factors for traffic analysis within the study limits. Further evaluation of the top 30 hours in terms of total roadway volume (i.e two-way volume) revealed that 23 of the top 30 hours of 2016 occurred from 4 to 5 PM , 5 of the top 30 hours occurred from 3 to 4 PM , and 2 of the top 30 hours occurred from 7 to 8 AM. This data indicates that the ATR is a fair representation of the trends within the study limits because 25 of the top 30 hours (or 83 percent) occurred during the AM and PM peak hours.

If the ATR data was not used to develop the DHV as suggested in FDM 11-5-3.5.1.1, WisDOT forecasting developed K30 factors at three count sites based on statewide averages for the facility type.

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These K30 factors were provided in the traffic forecast report dated April 6, 2018. The K30 factors at three locations in Fond du Lac County range from 10.7 percent to 12.3 percent.

This study recommends using a K30 factor of 10.0 percent based on the combined direction 2016 ATR data for the WIS 23 mainline traffic analysis.

## Analysis Software

The study used Highway Capacity Software (HCS) Version 7.5 for the traffic operations analysis. This was the most recently available version of HCS as of April 6,2018 , the date of the most current traffic forecasts. Since the initial traffic analysis in September 2017, the FDM has been updated to include HCS Version 7 as an accepted software for traffic analysis. ${ }^{4}$ This version of HCS follows practices from the Highway Capacity Manual (HCM) 6th edition. ${ }^{5}$

## Traffic Counts

Traffic counts were taken by WisDOT during the summer of 2017 along the WIS 23 study corridor at 11 roadway sites and at 14 intersections. A summary of where and when the roadway counts were taken is shown in the table below.

| Location: West to East |  |  | Count Data |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| County | Site ID | Roadways | Count Length | Count Dates (2017) | Truck data? |
| Fond du Lac | 201185 | Wisc American - County K | 48 hr | 5/08-5/10 | Yes |
|  | 200219 | East of County K | 48 hr | 7/25-7/27 | No |
|  | 201147 | County UU - Taft | 48 hr | 6/27-6/29 | Yes |
|  | 206104 | West of County W (S) | 48 hr | 6/27-6/29 | Yes |
|  | 200222 | West of County W (N) | 48 hr | 6/27-6/29 | Yes |
|  | 200224 | Triple T-Hillview | 48 hr | 6/27-6/29 | Yes |
|  | 201153 | West of County G | 24 hr | 6/27-6/28 | Yes |
| Sheboygan | 590118 | Division - Chickadee | 48 hr | 6/27-6/29 | Yes |
|  | 591421 | County T (S) - Sugarbush | 48 hr | 6/26-6/28 | No |
|  | 591422 | County A - Plank | 48 hr | 6/26-6/28 | No |
|  | 590195 | West of County P | 48 hr | 7/17-7/19 | No |

Peak period intersection traffic counts were performed in July and August 2017. The intersection counts were performed from 6-9 AM and 3-6 PM at each location. More information on how the intersection counts were used in the traffic operations analysis is located in the Traffic Modeling Methodology memorandum in Appendix A of the 2018 LS SEIS.

## Truck Percentages

In order to determine a truck percentage value to use in the traffic analysis, the study analyzed available truck volume data at the summer 2017 roadway count sites throughout the study corridor and the 2016 ATR 590608 count site along WIS 23. Within the 2-lane portion of the study limits (just west of County UU to County P), truck data was available at five sites in Fond du Lac County and at one site in

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Sheboygan County. The study analyzed AM peak hour, PM peak hour, and daily truck volumes and truck percentages at each of these sites. The results of this analysis are shown below.

|  |  |  | A | B | C | D | E | F | G |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location: West to East |  |  | Truck Volume Information Data (Two-way) |  |  |  |  |  |  |
| County | Site ID | Roadways | 7-8 AM <br> Truck Vol | $\begin{aligned} & \text { 7-8 AM } \\ & \text { Truck \% } \end{aligned}$ | 4-5 PM <br> Truck Vol | $\begin{aligned} & \text { 4-5 PM } \\ & \text { Truck \% } \end{aligned}$ | Total <br> Daily <br> Traffic | Daily Truck Vol | Daily <br> Truck \% |
| Fond du Lac | 201185 | Wisc Am - County K | 120 | 8.5\% | 88 | 7.2\% | 14,482 | 1,616 | 11.2\% |
|  | 201147 | County UU-Taft | 127 | 21.8\% | 105 | 16.3\% | 8,013 | 1,818 | 22.7\% |
|  | 206104 | West of County W (S) | 144 | 25.3\% | 119 | 18.6\% | 7,937 | 2,040 | 25.7\% |
|  | 200222 | West of County W (N) | 133 | 23.2\% | 114 | 17.9\% | 8,009 | 1,864 | 23.3\% |
|  | 200224 | Triple T-Hillview | 149 | 26.6\% | 97 | 16.1\% | 7,488 | 1,888 | 25.2\% |
|  | 201153 | West of County G | 131 | 23.8\% | 101 | 17.6\% | 7,065 | 1,730 | 24.5\% |
| Sheboygan | 590118 | Division - Chickadee | 119 | 21.4\% | 76 | 13.1\% | 7,133 | 1,546 | 21.7\% |
|  | 590608 (ATR) | East of WIS 32 | 111 | 5.5\% | 89 | 4.1\% | 26,544 | 1,732 | 6.5\% |

Columns A-G represent averages of the available count data (typically a 48-hour period btwn Tues and Thurs).
Columns A-G volume data is not seasonally adjusted and is being used here for vehicle classification purposes.

The analysis shows that the amount of truck traffic from Wisconsin American Drive to east of WIS 32 remains relatively consistent during the AM and PM peak hours. There are fluctuations with daily truck traffic. While the truck volumes are consistent, the truck percentages are lower in the 4 -lane sections (Wisconsin American Drive to County K and east of WIS 32) because of the relatively consistent number of trucks, yet higher amount of passenger vehicles at these locations (as shown in Columns E and $F$ of the table above). Daily truck volumes are not used directly in the operations analysis, but provide an overall picture of the mix of traffic along the study corridor.

As mentioned earlier, 23 of the top 30 two-way hourly volumes at ATR 590608 occurred during the PM peak hour (4-5 PM) in 2016 and another 5 of the top 30 two-way hourly volumes occurred during the hour before the PM peak hour (3-4 PM). For this reason, the study proposes to use the weighted average PM peak hour truck percentages from the field data between County UU and County G for analysis in Fond du Lac County and the truck percentage from Coverage Count Site 590118 for analysis in Sheboygan County. These values correspond to 17.4 percent for Fond du Lac County and 13.1 percent for Sheboygan County. Because HCS software only accepts rounded truck percentage values, the study used 17.0 percent for Fond du Lac County and 13.0 percent for Sheboygan County, in the peak hour traffic operations analysis. See the Traffic Modeling Methodology memorandum in Appendix A of the 2018 LS SEIS for more information on how these truck percentages were applied in the traffic operations analysis.

## Peak Hour Factor

The PHF is the hourly volume during the maximum-volume hour of the day divided by the peak 15minute flow rate within the peak hour; a measure of traffic demand fluctuations within the peak hour. PHF is used in operational analysis to account for the volume fluctuations during a typical rush hour. In rural areas a typical PHF is 0.88 based on default values provided in Chapter 15 of the HCM 6th edition. In urban or more saturated conditions, a PHF can be 0.92 or greater. The FDM 3.5.2.1 policy for PHF on Facility Segments states:

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The PHF for the existing conditions can be based on existing field data. If field data does not exist, the recommended HCM default can be used. For design year conditions use a PHF of 1.0.

This policy accounts for the flattening of volume variation within the design hour that occurs as traffic increases and roadways become more congested in the design year. For a highway like WIS 23 that is not saturated, the policy may mute the actual peak hour variations that are likely to occur, even with traffic growth. For this reason, the study performed a sensitivity analysis of the operations results by varying the PHF from the current WisDOT policy. To determine the PHF to use in the sensitivity analysis, the study used peak hour counts that were performed by WisDOT at the majority of intersections along WIS 23 during the summer 2017. While the PHF for each leg of an intersection is important for intersection analysis, the PHF for the WIS 23 mainline is most important for the WIS 23 mainline sensitivity analysis. The following table shows an average WIS 23 PHF of 0.87 for the morning and of 0.89 for the evening peak hours. These values represent higher volume variations during the peak hour.

| Location | AM Peak |  |  |  |  | PM Peak |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SB | WB | NB | EB | Int | SB | WB | NB | EB | Int |
| WIS 23 \& County UU | 0.56 | 0.94 | 0.68 | 0.85 | 0.92 | 0.50 | 0.85 | 0.72 | 0.91 | 0.92 |
| WIS 23 \& County S | 0.25 | 0.90 | 0.65 | 0.80 | 0.89 | 0.50 | 0.86 | 0.67 | 0.83 | 0.85 |
| WIS 23 \& Sugarbush Road | 0.69 | 0.92 | 0.31 | 0.81 | 0.87 | 0.25 | 0.80 | 0.50 | 0.92 | 0.89 |
| WIS 23 \& County A | 0.81 | 0.88 | 0.61 | 0.88 | 0.91 | 0.65 | 0.83 | 0.66 | 0.95 | 0.94 |
| WIS 23 \& 7 Hills Road | 0.67 | 0.85 | 0.79 | 0.86 | 0.89 | 0.75 | 0.88 | 0.62 | 0.84 | 0.90 |
| WIS 23 \& American Drive | 0.00 | 0.95 | 0.57 | 0.89 | 0.92 | 0.00 | 0.91 | 0.95 | 0.93 | 0.97 |
| WIS 23 \& County G | 0.94 | 0.79 | 0.87 | 0.95 | 0.89 | 0.67 | 0.94 | 0.74 | 0.92 | 0.94 |
| WIS 23 \& County K | 0.79 | 0.97 | 0.75 | 0.83 | 0.91 | 0.69 | 0.88 | 0.71 | 0.89 | 0.93 |
| WIS 23 \& County U | 0.00 | 0.93 | 0.70 | 0.78 | 0.87 | 0.00 | 0.88 | 0.67 | 0.90 | 0.89 |
| WIS 23 \& County W/Hinn Road WIS 23 \& County W/Loehr | 0.75 | 0.84 | 0.81 | 0.89 | 0.87 | 0.37 | 0.91 | 0.82 | 0.92 | 0.91 |
| Road | 0.87 | 0.87 | 0.67 | 0.94 | 0.91 | 0.78 | 0.95 | 0.75 | 0.88 | 0.94 |
| WIS 23 \& Hillview Road | 0.50 | 0.80 | 0.50 | 0.93 | 0.90 | 0.50 | 0.93 | 0.56 | 0.87 | 0.89 |
| WIS 23 \& Tower Road | 0.52 | 0.87 | 0.37 | 0.82 | 0.92 | 0.71 | 0.94 | 0.58 | 0.90 | 0.91 |
| WIS 23 \& Scenic View Road | 0.75 | 0.84 | 0.00 | 0.83 | 0.88 | 0.50 | 0.83 | 0.25 | 0.89 | 0.86 |
| Average |  | 0.881 |  | 0.863 | 0.897 |  | 0.886 |  | 0.897 | 0.911 |
|  |  | Mainline Average PHF (rounded) $=0.87$ |  |  |  |  | Mainline Average PHF (rounded) $=0.89$ |  |  |  |

As mentioned earlier, 23 of the top 30 two-way hourly volumes at ATR 590608 occurred during the PM peak hour ( $4-5 \mathrm{PM}$ ) in 2016 and another 5 of the top 30 two-way hourly volumes occurred during the hour before the PM peak hour (3-4 PM). For this reason, the study used the average mainline PM peak hour PHF of 0.89 from the field data in the sensitivity analysis.

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## K and Peak Hour Factor Sensitivity Analysis

As mentioned, the WIS 23 ATR provides traffic data patterns that best reflect the traffic on the study corridor. Several design hour (K), PHF, and DD combinations were reviewed to see how they would affect the volumes used in the operations analysis. These variables include:

- Using peak K30 for each direction of WIS 23.
- Using K30 for the combined WIS 23 (i.e. both directions of travel).
- Using peak K100 for each direction of WIS 23.
- Using K100 for the combined WIS 23.
- Using PHF of 1.0 per current policy.
- Using measured PHF of 0.89 .

Operational analyses are performed for the peak 15 minutes of the peak hour. The following table illustrates the volumes that could be used in the operational analysis using the following assumptions.

1. Using the K30 WB design hour and corresponding EB hour, PHF of 1.0 Using the K30 EB design hour and corresponding WB hour, PHF of 1.0
2. Using the combined K30 design hour, DD of $58 / 42$, PHF of 1.0
3. Using K100 WB design hour and corresponding EB hour, PHF of 0.89 Using K100 EB design hour and corresponding WB hour, PHF of 0.89
4. Using combined K100 hour, DD of $57 / 43$, PHF of 0.89

The following table illustrates the 15 -minute peak volume that would be used with each option. Note that the example volumes used in this table were not used directly in the WIS 23 operations analysis.

| Analysis Options | Direction | AADT | K <br> Factor | DD | PHF | DHV* | 15-min Peak |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \frac{\text { Option } 1}{\text { K30 EB and }} \\ \text { WB } \\ \text { PHF }=1.0 \end{gathered}$ | EB | 12,131 | 12.82\% | 69 | 1.00 | 1,555 | 389 |
|  | WB |  |  | 31 | 1.00 | 704 | 198 |
|  | Total |  |  |  |  | 2,259 | 587 |
|  | WB | 11,802 | 11.65\% | 61 | 1.00 | 1,375 | 344 |
|  | EB |  |  | 39 | 1.00 | 896 | 252 |
|  | Total | -- | -- | -- |  | 2,271 | 596 |
| $\begin{gathered} \frac{\text { Option } 2}{\text { K3O Two- }} \\ \text { Way } \\ \text { PHF }=1.0 \end{gathered}$ | EB | -- | -- | 58 | 1.00 | 1,394 | 348 |
|  | WB | -- | -- | 42 | 1.00 | 1,009 | 252 |
|  | Total | 23,933 | 10.04\% |  |  | 2,403 | 601 |
| $\begin{gathered} \frac{\text { Option } \mathbf{3}}{} \\ \text { K100 EB and } \\ \text { WB } \\ \text { PHF } 0.89 \end{gathered}$ | EB | 12,131 | 12.32\% | 70 | 0.89 | 1,495 | 420181 |
|  | WB |  |  | 30 |  | 1,405 643 |  |
|  | Total |  |  |  |  | 2,138 | 600 |
|  | WB | 11,802 | 11.23\% | 59 | 0.89 | 1,325 | 372 |
|  | EB |  |  | 41 |  | 938 | 263 |
|  | Total | -- | -- | -- |  | 2,263 | 636 |
| $\begin{gathered} \frac{\text { Option } 4}{} \\ \text { K100 Two- } \\ \text { Way } \\ \text { PHF } 0.89 \end{gathered}$ | EB | -- | -- | 57 | 0.89 | 1,334 | 375 |
|  | WB | -- | -- | 43 | 0.89 | 1,006 | 283 |
|  | Total | 23,933 | 9.78\% |  |  | 2,341 | 658 |

*Directional DHV Calculation (Options 1 and 3) = AADT x K Factor
Existing PHF 0.89
PHF = Hourly Volume / ( $4 \times$ Peak 15-minute Volume)

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## Summary

## Design Hour Volume (K) and Directional Distribution (DD)

The study used the combined K30 factor and the corresponding combined roadway DD of 58/42 for the operations analysis. Reasons for this include the following:

- WIS 23 exhibits peaking patterns that are characteristic of a commuter route. The difference between the K30 and K100 is only a quarter of a percent. Using the K30, as per policy, will not produce peak hour volumes that are unduly influenced (i.e. higher) by special events or recreational traffic.
- The combined K30 produced more balanced DD than the single direction K30 values. In twolane roadway analysis the non-peak direction influences the LOS. Determining the DD through analyzing single-direction K factors produced unreasonable DD splits. This occurred for the EB direction of travel where the DD for K30 and K100 was closer to 70/30 and was during the AM peak hour. Whereas the combined K30 provided a DD of $58 / 42$, which is more balanced and will provide better two-lane operations analysis.


## Peak Hour Factor

The study performed mainline operations analysis using a PHF of 0.89 and 1.0. The operations analysis using a PHF of 1.0 is per WisDOT policy and assumes no variations in demand over the peak hour in the design year. These results were used directly in the body of the 2018 LS SEIS.

An operations sensitivity analysis using a PHF of 0.89 was performed to compare WIS 23's future operation with its existing operation assuming no variations in demand over the peak hour in the design year. These results are included in the Traffic Modeling Methodology memorandum located in Appendix A of the 2018 LS SEIS.

## Truck Percentages

The study used a peak hour truck percentage of 17 percent for Fond du Lac County mainline analysis and 13 percent for Sheboygan County mainline analysis. These values are consistent with the peak hour truck percentages obtained from the summer 2017 traffic counts. Because WIS 23 is a commuter route with relatively little difference between K 30 , K 100 , and K 250 , the count site truck percentages provide a reasonable representation of trucks during the K30 design hour. Daily truck volumes along the 2-lane portion of the study corridor range from 22 to 26 percent, but are not used directly in the operations analysis.

## Analysis Software

The study used HCS Version 7.5. The Traffic Modeling Methodology memorandum includes discussion on software inputs, assumptions, and the use of the traffic forecasts in the analysis. HCS Version 7 is an accepted WisDOT HCM-Based Deterministic Tool per WisDOT FDM 11-5-3.7.1.1. This separate memorandum is included in Appendix A of the 2018 LS SEIS.

## Summary

A summary of the factors that will be used in the WIS 23 mainline operations analysis is below.

$$
\begin{aligned}
& \mathbf{K 3 0}=10.0 \% \\
& \mathbf{D D}=58 / 42
\end{aligned}
$$

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$\mathbf{P H F}=1.00$, and a $\mathrm{PHF}=0.89$ as a sensitivity analysis to compare with existing conditions
Mainline truck percentage (Fond du Lac County) $=17.0 \%$
Mainline truck percentage (Sheboygan County) $=13.0 \%$
Analysis Software: HCS Version 7.5

# TECHNICAL MEMORANDUM 

To: Bryan Lipke P.E. - Wisconsin Department of Transportation, Northeast Region<br>Dawn Krahn, P.E. - Wisconsin Department of Transportation, Bureau of State Highway Programs<br>Ben Rouleau - Wisconsin Department of Transportation, Bureau of Traffic Operations

From: Thomas W. Lynch, P.E., PTOE
Joseph M. Urban, P.E.
Strand Associates, Inc. ${ }^{\circledR}$
Date: May 11, 2018
Re: ID 1440-13/15-00
Fond du Lac to Plymouth
WIS 23
Fond du Lac and Sheboygan Counties
Traffic Modeling Methodology

## Section 1: Background

This memorandum documents the traffic analysis software and methodology used for traffic modeling within the Wisconsin State Highway (WIS 23) 2018 Limited Scope Supplemental Environmental Impact Statement (LS SEIS) project limits. The study limits are the US Highway 151 (US 151)/WIS 23 interchange on the west end and County P/Pioneer Road (County P) on the east end. The corridor is mostly a 2-lane rural highway, with relatively short stretches of 4-lane highway on both ends of the corridor. The traffic analysis for this study focuses on the two-lane highway portion of the corridor from County UU to County P , which is nearly 18 miles long.

The alternatives being considered for this study will require the following types of traffic analyses:

1. Two-lane highway analysis
2. Interchange segment analysis
3. Intersection analysis

There are no traffic signal or roundabout-controlled intersections within the existing study corridor and none are proposed along the WIS 23 mainline as part of this study. Roundabout-controlled intersections are included at the ramp terminals for proposed interchanges.

Further information on the alternatives being considered can be found in Section 2 of the 2018 LS SEIS. Schematic maps displaying the alternatives are shown in Attachment A of this memorandum.

Roadway and intersection traffic counts were performed in the summer of 2017 along the study corridor. Traffic forecasts were prepared by Wisconsin Department of Transportation (WisDOT) Traffic Forecasting Section (TFS) on April 6, 2018 using the 2017 count data as the existing conditions, or base year, and 2040 as the design year. The development and results of the traffic forecasts are presented in the traffic forecasting memorandum prepared by WisDOT TFS included in

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Appendix B of the 2018 LS SEIS. Mainline traffic forecasts were prepared at 11 locations along the WIS 23 mainline throughout the study corridor for each alternative. Intersection forecasts were prepared at a majority of the locations where intersection traffic counts were performed.

## Section 2: Traffic Analysis Software Selection

According to the WisDOT Facilities Development Manual (FDM), Section 11-5-3.7.3 ${ }^{1}$, WisDOT prefers the use of Highway Capacity Manual 6th edition ${ }^{2}$ (HCM) based analysis methods for most traffic studies. The policy states "The methodologies of the HCM should be the primary way of determining the performance measures required for a variety of traffic study projects reviewed and/or commissioned by WisDOT".

Per WisDOT FDM 11-5-3.7.1.1, the supported programs that implement the HCM methodology for capacity analysis are Highway Capacity Software 7 (HCS) - Version 7, Synchro Version 10, and SIDRA Intersection Version 7 (for roundabouts only).

1. Two-Lane Highway Analysis
a. HCM Definition

Two-lane highway analysis is appropriate for the WIS 23 corridor because the study limits consist primarily of two-lane highway (County UU to County P) and there is uninterrupted flow throughout the two-lane portion of the corridor (i.e. no traffic signals, roundabouts, or all-way-stop-controlled intersections). The HCM defines uninterrupted flow as "where there are no traffic control devices that interrupt traffic and where no platoons are formed by upstream traffic signals" (HCM 6th edition 15-1). Furthermore, the HCM states that generally any segment that is 2.0 to 3.0 miles away from the nearest signalized intersection may be considered as an uninterrupted flow segment.

For WIS 23, the nearest signalized intersection to the west of the two-lane study limits are the US 151 ramp terminal intersections, nearly 2 miles west of County UU, and to the east of the two-lane study limits (County P) the nearest signal is over 13 miles away. Because there are no traffic control devices within the two-lane study limits and that signals are far enough away to minimize platooning, two-lane highway analysis is the most appropriate methodology to analyze the mainline operations for WIS 23.
b. Software Selection

WisDOT currently supports HCS and PTV Vissim (a microsimulation program) for twolane highway analysis, per WisDOT FDM 11-5-3.7.3.11. Because HCS directly implements the HCM methodology for capacity analysis it is more appropriate to use for the two-lane highway analysis than PTV Vissim, which is a form of microscopic traffic simulation software (microsimulation). Microsimulation tools typically require

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significantly more traffic data, time, and effort for calibration than HCM-based analysis tools, such as HCS, and are not considered necessary for the WIS 23 traffic analysis. HCS also has the ability to model passing lanes using methods directly from the HCM.

The HCM states on Page 15-11 that there are currently no other alternative deterministic tools (outside of the HCM methodology implemented by HCS) that are in common use for two-lane highway analysis.

For these reasons, the study team used HCS for the two-lane highway analysis.

## 2. Four-Lane Highway and Interchange Segment Analysis

Similar to the two-lane analysis, HCS is also supported by WisDOT for four-lane highway and interchange analysis per WisDOT FDM 11-5-3.7.3.9. Portions of the proposed alternatives for this study will include merge, diverge, and basic segments.

For consistency in software with the two-lane highway analysis, the study team used HCS for modeling of proposed four-lane highway and interchange segments.

## 3. Stop-Controlled Intersection Analysis

For stop-controlled intersection analysis the WisDOT FDM indicates in section 3.7.3.2 that HCS, Synchro, and PTV Vissim are supported WisDOT software. Both HCS and Synchro are HCMbased tools that could be used for WIS 23.

For consistency in software with the two-lane highway, four-lane highway, and interchange merge/diverge analyses, the study team used HCS for modeling of existing and proposed stopcontrolled intersections.

The study team used HCS Version 7.5 in each of the traffic analyses discussed above. This is the most current version of HCS as of April 6, 2018, when the most recent traffic forecasts for the study were completed by the WisDOT TFS. This version of HCS follows practices from the HCM 6th edition.

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## Section 3: Two-Lane Highway Analysis

Table 1 shows the different inputs and/or assumptions used in the two-lane highway HCS analysis.

| Category | WIS 23 HCS Input Value | Source |
| :---: | :---: | :---: |
| Analysis Direction Volume (or DDHV) | Weighted Average AADT x K30 x DD | FDM 11-5-3.5.1.1 Design Hour Volume for Freeways, Multilane Highways, and Two-Lane Highways |
| Opposing Direction Volume | Weighted Average AADT $\times$ K $30 \times(1-$ DD $)$ |  |
| Shoulder Width | No-Build $=8 \mathrm{ft}$ <br> Build Alts (Passing Lanes) $=8 \mathrm{ft}$ | Field conditions and proposed Build conditions |
| Lane Width | No-Build and Build Alts $=12 \mathrm{ft}$ | Field conditions and proposed Build conditions. |
| Segment Length | County UU to County G $=9.8 \mathrm{mi}$ County G to County P = 8.0 mi (analyzed length is slightly less) <br> Varying lengths for passing lanes Alts | Base and No-Build: Field conditions. Passing lane effective lengths: HCM 6th Edition (15-31) |
| Highway Type | Class I Highway | HCM 6th Edition (15-4) |
| Terrain | Varies between Level and Rolling | FDM 11-5-3.5.5 Rural Roadway Conditions. See "Terrain Type" section below for more information. |
| Peak Hour Factor | Existing $=0.89$ <br> $2040=1.0$ per WisDOT policy and $2040=$ <br> 0.89 to compare with existing conditions | "DHV for WIS 23 Evaluation" Memo (originally dated 10/5/2017, updated 5/11/2018) |
| Truck and Bus Percentage | Fond du Lac County = 17.0\% <br> Sheboygan County = 13.0\% <br> Weighted average truck percentages used for overlapping Passing Lane segments |  |
| Recreational Vehicle Percentage | 0\% | Recreational vehicle volumes not separated in field data. |
| Access Points | Varies | See Table 6 and exhibits in Attachment D. |
| Mainline base free-flow speed | 60 mph | Assumed to be posted +5 mph , or equivalent to a typical design speed for a highway posted at 55 mph . |
| No-Passing Zone Percentages | Varies | Measured from field, see Table 7 and Attachment E . |

DDHV = Directional Design Hour Volume, AADT = Average Annual Daily Traffic Volume, DD = Directional Distribution

## Table 1: Inputs and Assumptions for HCS Two-Lane Analysis

The following describes the factors and assumptions in the traffic analysis shown in Table 1 where further detail is beneficial.

1. Analysis Direction Volume and Opposing Direction Volume

The analysis direction (i.e. the higher-volume direction of travel) and the opposing direction volume were determined for each analysis section using a weighted Average Annual Daily Traffic (AADT) volume derived from traffic forecasts provided by WisDOT TFS. Mainline AADT volumes were provided by WisDOT TFS on April 6, 2018 for base year (2017), design year (2040) conditions, and two future interim year (2020 and 2030) conditions.

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Mainline traffic forecast volumes were provided at 11 locations along the study corridor between US 151 and County P. Of the 11 sites, 9 sites are located within the 2 -lane highway section of WIS 23 between County UU and County P and 2 sites are located in the 4-lane highway section of WIS 23 between US 151 and Whispering Springs Drive ( $\sim 2 / 3$ of a mile west of County UU). For the purposes of the two-lane highway operations analysis, the 9 sites located within the 2-lane section of WIS 23 are used to determine the weighted average analysis volumes.

The base conditions and 2040 No-Build analyses are broken up into two sections, County UU to County G (mostly in Fond du Lac County) and County G to County P (mostly in Sheboygan County). The analyses are divided because 2017 volumes are slightly higher east of County G. The steps to determine the weighted average volume for each analysis section are as follows:
a. Step 1: Calculate Weighted Average AADT Volume (Two-way traffic).
b. Step 2: Determine Two-Way Design Hour Volume (DHV). This is calculated by applying the K30 factor of $10.0 \%$ to the Weighted Average AADT Volume.
c. Step 3: Apply Directional Distribution (DD) factor of $58 \%$ to the Two-Way DHV to determine the Analysis Direction Volume.
d. Step 4: Apply ( $1-\mathrm{DD}$ ) factor of $42 \%$ to the Two-Way DHV to determine the Opposing Direction Volume.

Table 2 and Figure 1 show a breakdown of the 11 WIS 23 mainline count locations in 2017 where traffic forecasts were provided.

| Site ID <br> (West to <br> East) | 2017 WIS 23 Mainline <br> Count Location | Roadway Limits AADT <br> Applied to in WIS 23 <br> Two-Lane Traffic Analysis | Approximate Distance (mi) <br> Rounded to nearest hundredth |
| :--- | :--- | :--- | :---: |
| 201185 | Wisconsin American <br> Drive to County K | Not used - within 4-lane section | --- |
| 201022 | East of County K | Not used - within 4-lane section | --- |
| 201147 | County UU to Taft Road | County UU to Tower Road | 1.99 |
| 206104 | West of County W <br> (south) | Tower Road to <br> County W (south)/Hinn Road | 3.03 |
| 200222 | West of County W <br> (north) | County W (south)/Hinn Road to <br> County W (north)/Loehr Road | 0.49 |
| 200224 | Triple T to Hillview | County W (north)/Loehr Road to <br> Hillview Road | 3.22 |
| 201153 | West of County G | Hillview Road to County G | 1.03 |
|  | Fond du Lac County (County UU to County G) Subtotal |  | $\mathbf{9 . 7 5}$ |
| 590118 | Division - Chickadee | County G to County T (north) | 3.71 |
| 591421 | County T (south) to <br> Sugarbush | County T (north) to County A | 1.41 |
| 591422 | County A to Plank | County A to County S | 1.84 |
| 590195 | West of County P | County S to County P | 1.05 |
|  | Sheboygan County (County G to County P) Subtotal |  | $\mathbf{8 . 0 1}$ |

Table 2: WIS 23 Mainline Count Locations and Forecast Sites

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Table 3 shows a breakdown of the base conditions (2017) and projected 2040 No-Build AADT volumes at each of the WIS 23 mainline sites within the two-lane highway analysis sections.

| Site ID <br> (West to <br> East) | Roadway Limits | Approximate <br> Distance (mi) | 2017 Count <br> AADT | 2040 No- <br> Build AADT |
| :---: | :--- | :---: | :---: | :---: |
| 201147 | County UU to Taft Road | 1.99 | 7,400 | 8,300 |
| 206104 | West of County W <br> (south) | 3.03 | 7,300 | 7,900 |
| 200222 | West of County W <br> (north) | 0.49 | 7,400 | 7,800 |
| 200224 | Triple T to Hillview | 3.22 | 6,900 | 7,100 |
| 201153 | West of County G | 1.03 | 6,800 | 6,900 |
| County UU to County G Weighted Average AADT | 7,140 | 7,610 |  |  |
| 590118 | Division - Chickadee | 3.71 | 6,700 | 6,800 |
| 591421 | County T (south) to <br> Sugarbush | 1.41 | 7,800 | 7,900 |
| 591422 | County A to Plank | 1.84 | 8,400 | 8,700 |
| 590195 | West of County P | 1.05 | 9,400 | 9,700 |
| County G to County P Weighted Average AADT |  | 7,640 | 7,810 |  |

Table 3: WIS 23 Mainline 2017 and 2040 No-Build AADT Volumes

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The weighted average AADT volumes shown in Table 3 are calculated by the following equation:

$$
\text { Weighted Average } A A D T=\frac{(\text { Length } 1 \times A A D T 1)+(\text { Length } 2 \times A A D T 2)+\ldots}{\text { Total Length }}
$$

An example calculation for the County UU to County $G$ weighted average AADT volume in the 2040 No-Build Alternative is shown in the formula below:

$$
\begin{aligned}
& \text { Weighted Average AADT }= \\
& \frac{[(1.99 \times 8,300)+(3.03 \times 7,900)+(0.49 \times 7,800)+(3.22 \times 7,100)+(1.03 \times 6,900)]}{9.76}
\end{aligned}
$$

## Weighted Average AADT $=7,610 v p d$

It should be noted that the calculations above are performed in a spreadsheet, where the individual section lengths in the Weighted Average AADT volume calculations are not rounded. The spreadsheet calculation provides a volume of $7,607.09$ vehicles per day (vpd), which is rounded to the nearest ten at $7,610 \mathrm{vpd}$. This may lead to relatively minor differences if comparing values hand-calculated based on the information in this memo and spreadsheet values; however, the spreadsheet calculations are being used in the traffic analysis as they provide a more exact and appropriate evaluation of the weighted average AADT volumes.

Using the weighted average AADT volumes for each analysis section, the Two-Way DHV, Analysis Direction Volume and Opposing Direction Volume can be calculated with units of vehicles per hour (vph). Table 4 shows each of these values for the 2040 No-Build analysis sections. The analysis sections involving climbing lanes are discussed further in the next section.

| Analysis Section | 2017 Count <br> Weighted Average AADT (vpd) | 2040 No-Build Weighted Average AADT (vpd) | 2040 No-Build <br> Two-Way DHV (vph) ${ }^{[1]}$ | $\begin{aligned} & \hline 2040 \text { No-Build } \\ & \text { Analysis } \\ & \text { Direction } \\ & \text { Volume (vph) }{ }^{[2]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2040 \text { No-Build } \\ & \text { Opposing } \\ & \text { Direction } \\ & \text { Volume (vph) }{ }^{[3]} \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| EB/WB: County UU to County G | 7,140 | 7,610 | 761 | 441 | 320 |
| EB: County G to Climbing Lane | 7,140 | 7,260 | 726 | 421 | 305 |
| EB: County G to west of County P | 7,570 | 7,740 | 774 | 449 | 325 |
| WB: Climbing Lane | 8,910 | 9,210 | 921 | 534 | 387 |
| WB: Climbing Lane to County G | 7,290 | 7,430 | 743 | 431 | 312 |

[1] Two-way DHV = Weighted Average AADT x K30 Factor
[2] Analysis Direction Volume = Two-Way DHV x DD Factor
[3] Opposing Direction Volume $=$ Two-Way DHV x (1.0 - DD Factor)
Note: K30 Factor $=10.0 \%, D D=58 \%$
Table 4: WIS 23 Mainline 2040 No-Build Analysis Volumes

Example calculations for the County UU to County G 2040 No-Build Two-Way DHV, Analysis Direction Volume, and Opposing Direction Volume are shown below:

```
Two-way DHV \(=7,610 \mathrm{vpd} \times 0.10=761 \mathrm{vph}\)
Analysis Direction Volume \(=761 \mathrm{vpd} \times 0.58=441 \mathrm{vph}\)
Opposing Direction Volume \(=761 \mathrm{vpd} \times(1-0.58)=320 \mathrm{vph}\)
```

The Analysis Direction Volume and Opposing Direction Volume values are directly input into HCS for the two-lane highway operations analysis.

## 2. Analysis Section Length

For the two-lane highway analysis for the No-Build conditions and for the with passing lanes analysis, effective lengths of the passing lanes and/or climbing lanes need to be calculated. Figure 2 shows the locations of the proposed passing lanes for the Passing Lane Alternative and the locations of the existing climbing lanes.


Figure 2: Proposed Passing Lane Locations and Existing Climbing Lane Locations
Section 2 of the 2018 LS SEIS provides more detail on the locations of the existing climbing lanes and the passing lanes proposed within the study limits. Page 15-32 of the HCM defines how to divide a roadway into 4 regions for a passing lane analysis. These 4 regions are defined as the following, along with the recommendations for inclusion from the HCM on Page 15-32:
a. $\quad L_{u}=$ Length upstream of the passing lane (optional to include)
b. $\mathrm{L}_{\mathrm{pl}}=$ Length of the passing lane (required)
c. $\mathrm{L}_{\mathrm{de}}=$ Length downstream of the passing lane within its effective length (strongly recommended to include)
d. $L_{d}=$ Length downstream of the passing lane beyond its effective length (optional to include)

The analysis regions are required to add up to the total length of the analysis section. Per the HCM on Page 15-33:

The length of the conventional two-lane highway segment upstream of the passing lane $L_{u}$ is determined by the actual or planned placement of the passing lane within the analysis segment. The length of the downstream highway segment within the effective

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length of the passing lane $L_{d e}$ is determined from Exhibit 15-24. Any remaining length of the analysis segment downstream of the passing lane is included in $L_{d}$.

Page 15-34 of the HCM advises that the effective downstream distance of a passing lane should generally not be truncated. In cases where the effective downstream distance is truncated, the location at which the distance is truncated should occur where any of the following conditions are met as per Page 15-34 of the HCM:

- The environment of the highway radically changes, as in the case of entering a small town or developed area from a rural segment;
- A major unsignalized intersection is present, leading to a change in the demand flow rate;
- A proximite signalized intersection begins to affect the operation of the two-lane segment;
- The terrain changes significantly; or
- Lane or shoulder widths change significantly.

Page $15-10$ of the HCM states that all segments with grades of 3 percent or more that cover a length of 0.6 miles or more must be analyzed as specific grades, rather than as a general terrain type such as "rolling". For WIS 23, the climbing lane in the WB direction of travel between Twinkle Lane and Ridge Road fits this definition with a length of 1.1 miles and an up-grade of approximately 4.6 percent for approximately 0.62 miles. In the EB direction of travel, the climbing lane between Plank Road and Ridge Road is approximately 0.5 miles in length with an up-grade of approximately 4 percent. For climbing lanes, the HCM recommends on Pages 15-36 and 15-37 that $\mathrm{L}_{\mathrm{u}}, \mathrm{L}_{\mathrm{de}}$, and $\mathrm{L}_{\mathrm{d}}$ are each set to zero unless the climbing lane ends before the grade does.

Through discussion with WisDOT Bureau of Traffic Operations (BTO), the study team decided to analyze the EB climbing lane as a passing lane in order to be able to appropriately capture the two-lane highway segment downstream of the climbing lane between Ridge Road and County P. If the EB climbing lane is analyzed in isolation as a specific-grade, then a short section (approximately 1.3 miles) of WIS 23 EB between the climbing lane and County P would remain. If this short section of WIS 23 EB is analyzed separately as a two-lane highway analysis, it would not capture the operational effects of the upstream climbing lane. Additionally, the up-grade for the EB climbing lane (4 percent) is less than the WB side (4.6 percent), which was analyzed as a specific grade, and the EB climbing lane length ( 0.5 miles) is less than the length of 0.6 miles or more required by the HCM for specific-grade analysis.

The four regions ( $\mathrm{L}_{\mathrm{u}}, \mathrm{L}_{\mathrm{pl}}, \mathrm{L}_{\mathrm{de}}$, and $\mathrm{L}_{\mathrm{d}}$ ) for each passing lane analysis were calculated following the guidelines indicated in the HCM. The following sections were analyzed in each Alternative:

1. No-Build - Eastbound
a. County UU to County G
b. County G to Climbing Lane
c. Climbing Lane (analyzed as a passing lane)

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2. No-Build - Westbound
a. Climbing Lane (analyzed as a specific grade)
b. Climbing Lane to County G
c. County G to County UU
3. Passing Lane Alternative (see Alternative 2 labeling in Figure 4)
a. Eastbound: 2A, 2C, and existing climbing lane (as passing lane)
b. Westbound: 2B, 2D, and existing climbing lane (as specific grade)
4. Hybrid Alternative (See Alternative 2 labeling in Figure 5)
a. Eastbound: 2C, and existing climbing lane (as passing lane)
b. Westbound: 2D, and existing climbing lane (as specific grade)

Figure 3 shows the two-lane highway analysis sections along WIS 23 for the base conditions and 2040 No-Build alternative.


Figure 3: 2017 and 2040 No-Build Two-Lane Highway Analysis Sections

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Table 5 details the four regions for each passing lane analysis in the Passing Lane Alternative. Each of the lengths were originally calculated in feet and are rounded to the nearest tenth of a mile for presentation purposes in Table 5.

| Analysis Section | Passing Lane Location (including tapers) | Upstream <br> Length $\mathrm{L}_{\mathrm{u}}$ (mi) | Passing Lane Length $\mathrm{L}_{\mathrm{pl}}$ (mi) | Calculated <br> Downstream <br> Length (mi) ${ }^{[1]}$ | Modeled Downstream Length $\mathrm{L}_{\text {de }}$ (mi) | Total Length $\begin{gathered} \mathrm{L}_{\mathrm{u}}+\mathrm{L}_{\mathrm{pl}}+\mathrm{L}_{\mathrm{de}} \\ \text { (mi) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2A (EB) | $\begin{gathered} \text { Sta } 325+00 \text { to } \\ 382+00 \\ \hline \end{gathered}$ | $2.3{ }^{[2]}$ | 1.1 | 7.7 | $6.4{ }^{[3]}$ | 9.8 |
| 2B (WB) | $\begin{gathered} \text { Sta } 550+50 \text { to } \\ 618+00 \\ \hline \end{gathered}$ | 1.9 | 1.3 | 7.7 | $6.6{ }^{[4]}$ | 9.8 |
| 2C (EB) | $\begin{gathered} \text { Sta } 730+90 \text { to } \\ 793+80 \\ \hline \end{gathered}$ | 6.6 | 1.2 | 7.8 | $4.2{ }^{[5]}$ | 12.0 |
| 2D (WB) | $\begin{gathered} \hline \text { Sta } 848+65 \text { to } \\ 907+65 \\ \hline \end{gathered}$ | 2.9 | 1.1 | 7.8 | $4.3{ }^{[6]}$ | 8.3 |
| CL EB | Plank to Ridge | 4.2 | 0.8 | 7.4 | $1.3{ }^{[7]}$ | 6.3 |
| CL WB | Twinkle to Ridge | 0 | 0.62 | 0 | 0.48 | 1.1 |

[1] Calculated downstream lengths are developed from Exhibit 12-23 of the HCM using Percent Time Spent Following
(PTSF) as the performance measure. The directional demand value is based on the 2040 analysis direction volume (i.e. the peak direction) for the Passing Lane Alternative.
[2] Upstream two-lane length is set to end at County UU due to change in volume and for consistency with the base conditions and No-Build analysis limits. The lane drop from two EB lanes to one EB lane is approximately 0.2 miles west of County UU.
[3] Modeled length is less than calculated length because the next proposed passing lane is 6.6 miles downstream of the end of the taper for passing lane 2 A . This qualifies as a significant change to mainline geometrics and therefore the downstream effective length was truncated to County G , which is a high volume unsignalized intersection approximately 6.4 miles downstream and consistent with the modeling limits of the No-Build analysis.
[4] Modeled length is less than calculated length because the expansion to two lanes WB along WIS 23 is 7.1 miles downstream of the end of the taper for passing lane 2B. This qualifies as a significant change to mainline geometrics and therefore the downstream effective length was truncated to County UU, which is a high volume unsignalized intersection approximately 6.6 miles downstream and consistent with the modeling limits of the No-Build analysis.
[5] Modeled length is less than calculated length because the climbing lane along WIS 23 EB is 4.2 miles downstream of the end of the taper for passing lane 2 C . This qualifies as a significant change to mainline geometrics.
[6] Modeled length is less than calculated length because the next proposed passing lane is 4.3 miles downstream of the end of the taper for passing lane 2D.
[7] Modeled length is less than calculated length because the expansion to 2 lanes EB along WIS 23 is 1.3 miles downstream of the end of the climbing lane.

## Table 5: WIS 23 Passing Lane Alternative: Region Lengths

It should be noted that there are overlapping analysis areas when defining the passing lane segments. This is necessary in order to reasonably replicate the downstream effective lengths recommended within HCM methodology. For example, in the Passing Lane Alternative the downstream effective length ( $\mathrm{L}_{\mathrm{de}}$ ) for Analysis Section 2A overlaps with the upstream length ( $\mathrm{L}_{u}$ ) of Analysis Section 2C.

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Figure 4 shows the two-lane highway analysis sections along WIS 23 for the 2040 Passing Lane Alternative.


Figure 4: Passing Lane Alternative: Two-Lane Highway Analysis Sections

In the Hybrid Alternative, two different passing lane sections and the existing climbing lanes were analyzed. Table 6 details the four regions for each two-lane highway analysis performed in the Hybrid Alternative.

| Analysis Section | Passing Lane Location (including tapers) | Upstream Length $\mathrm{L}_{\mathrm{u}}$ (mi) | Passing Lane Length $\mathrm{L}_{\mathrm{pl}}$ (mi) | Calculated Downstream Length (mi) ${ }^{[1]}$ | Modeled Downstream Length $\mathrm{L}_{\mathrm{de}}$ (mi) | $\begin{gathered} \text { Total Length } \\ \mathrm{L}_{\mathrm{u}}+\mathrm{L}_{\mathrm{pl}}+\mathrm{L}_{\text {de }} \\ (\mathrm{mi}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 C (EB) | $\begin{gathered} \hline \text { Sta } 730+90 \text { to } \\ 793+80 \end{gathered}$ | $0.2{ }^{[2]}$ | 1.2 | 7.4 | $4.2{ }^{[3]}$ | 5.7 |
| 2D (WB) | $\begin{gathered} \hline \text { Sta } 848+65 \text { to } \\ 907+65 \end{gathered}$ | 2.9 | 1.1 | 7.4 | $2.5{ }^{[4]}$ | 6.5 |
| CLEB | Plank to Ridge | 4.2 | 0.8 | 7.0 | $1.3{ }^{[5]}$ | 6.3 |
| CL WB | Twinkle to Ridge | 0 | 0.62 | 0 | 0.48 | 1.1 |

[1] Calculated downstream lengths are developed from Exhibit 12-23 of the HCM using PTSF as the performance measure. The directional demand value is based on the 2040 analysis direction volume (i.e. the peak direction) for the Hybrid Alternative. The calculated downstream length for the hybrid alternative is less than those of the Passing Lane Alternative due to higher 2040 analysis direction volumes in the Hybrid Alternative analysis.
[2] Upstream two-lane length is set to end at County G interchange due to significant change in geometry.
[3] Modeled length is less than calculated length because the climbing lane along WIS 23 EB is 4.2 miles downstream of the end of the taper for passing lane 2 C . This qualifies as a significant change to mainline geometrics.
[4] Modeled length is less than calculated length because the County G interchange (and 4-lane section west of County G) is 2.5 miles downstream, which constitutes as a significant change in mainline geometry.
[5] Modeled length is less than calculated length miles because the expansion to 2 lanes EB along WIS 23 is 1.3 miles downstream of the end of the climbing lane.

## Table 6: WIS 23 Hybrid Alternative: Region Lengths

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Figure 5 shows the two-lane highway analysis sections along WIS 23 for the 2040 Hybrid Alternative. The four-lane highway analysis is discussed in Section 4 of this memorandum.


Figure 5: Hybrid Alternative: Two-Lane Analysis Sections
The region lengths discussed in this section include several $\mathrm{L}_{\mathrm{de}}$ (downstream effective lengths) that are truncated due to significant changes in geometry along the mainline. Explanations for each truncated downstream effective length are in the footnotes of Tables 5 and 6 . Because there are several $L_{d e}$ that needed to be truncated, the analysis team did not include $L_{d}$ (downstream length of the passing lane beyond its $L_{d e}$ ) in any of the region length calculations for consistency in the traffic analysis of each individual passing lane. The HCM indicates on Page $15-32$, as stated previously, that $L_{d}$ is an optional region and inclusion is at the discretion of the analyst.

It should be noted that the weighted average AADT volumes for the No-Build, Passing Lane Alternative and the Hybrid Alternative are based on the total lengths indicated in Figures 3-5 (and shown in Tables 5 and 6). Larger versions of Figures 3, 4, and 5 are included in Attachment B. The weighted average AADT volumes, two-way DHV volumes, analysis direction volumes, opposing direction volumes, and truck percentages for each of the two-lane highway analysis sections of each alternative are shown in Attachment C.

## 3. Highway Type

WIS 23 is classified as a Class I two-lane highway based on the HCM 6th edition definitions. Per page 15-4 of the HCM:

Class I two-lane highways are highways where motorists expect to travel at relatively high speeds. Two-lane highways that are major intercity routes, primary connectors of major traffic generators, daily commuter routes, or a major link in state or national highway networks are generally assigned to Class I. These facilities serve mostly longdistance trips or provide connections between facilities that serve long-distance trips.

WIS 23 fits the HCM definition of a Class I highway. The nearly 18 mile WIS 23 study corridor is largely a rural corridor that connects two metropolitan urban areas, Fond du Lac and Sheboygan. The Fond du Lac core urban statistical area is home to about 101,600 people while the Sheboygan core urban statistical area is home to about 115,500 people ${ }^{3}$. I-41 is a major north-south corridor that connects the Fond du Lac area to Milwaukee and the Fox Valley and Green Bay. I-43 is a major north-south corridor that serves the Sheboygan area and connects it to Milwaukee and Green Bay. WIS 23 is one of the few higher mobility roadways that travel east-west through the region connecting these two interstate highways.

## 4. Terrain Type

The HCM allows classifications of level, rolling, or mountainous to be selected for terrain type in a two-lane highway analysis.

Per FDM 11-5-3.5.5 Rural Roadway Conditions on terrain type:
Wisconsin highways use only the level and rolling terrain classifications. Level terrain generally includes corridors that contain grades of no more than 3 percent. These corridors include any combination of horizontal and vertical alignment permitting heavy vehicles to maintain approximately the same speed as passenger cars.

Rolling terrain generally includes grades of significant length greater than 3 percent grade and will cause heavy vehicles to reduce their speed substantially below the speed of passenger cars. Typically, rolling terrain corridors are similar to those found near the Wisconsin River Valley, in the southwestern part of the State.

For WIS 23, level terrain is used for all two-lane highway and passing lane analyses except for the Eastbound Climbing Lane analysis in each alternative. For this analysis, rolling terrain is used because the grades along WIS 23 are over 3 percent within the segment limits. For the Westbound Climbing Lane, as mentioned previously, a specific-grade analysis is performed.

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## 5. Access Point Density

Per page $15-16$ of the HCM: The access point density is calculated by dividing the total number of unsignalized intersections and driveways on both sides of the roadway segment by the length of the segment (in miles). Table 7 shows a summary of the number of access points and the access point density for each analysis section.

| Alternative and Analysis Section | \# of Access Points | Access Points per Mile |
| :---: | :---: | :---: |
| No-Build: County UU to County G | 134 | 14 |
| No-Build: County G to Climbing Lane EB | 62 | 11 |
| No-Build: Climbing Lane EB Analysis County G to West of County P | 81 | 10 |
| No-Build: Climbing Lane WB Analysis Twinkle to Ridge | 11 | 10 |
| No-Build: Climbing Lane WB to County G | 68 | 11 |
| No-Build: County G to County UU | 134 | 14 |
| Passing Lane 2A: County UU to County G | 134 | 14 |
| Passing Lane 2B: County G to County UU | 134 | 14 |
| Passing Lane 2C: 2A to Climbing Lane EB | 149 | 12 |
| Passing Lane 2D: Climbing Lane WB to 2B | 94 | 11 |
| Hybrid 2C: County G to Climbing Lane EB | 62 | 11 |
| Hybrid 2D: Climbing Lane WB to County G | 68 | 11 |
| Passing Lane and Hybrid Alts: Climbing Lane EB Analysis - 2C to West of County P | 61 | 10 |
| Passing Lane and Hybrid Alts: Climbing Lane WB Analysis - Twinkle to Ridge | 11 | 10 |

Table 7: Access Point Density Summary
Attachment D shows a more detailed corridor map used for the access point density calculations along with summary tables for each analysis section.

It should be noted that recent acquisitions since the 2014 LS SFEIS are not included in the access point density calculations used for the operations analysis. The recent acquisitions result in a net change of 3 fewer access points along the corridor based on a review performed by WisDOT Northeast region staff. The results of the two-lane highway operations analysis are not anticipated to substantially change based on testing performed with the No-Build Alternative. ${ }^{4}$

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## 6. No-Passing Zone Percentages

No-passing zone percentages were calculated for each analysis section using stationing from alignment files provided by WisDOT on September 28, 2017, Google Maps Aerials, and Google Street View. Google Street View along the corridor is up-to-date as of November 2016.

Two analyses are performed for the Passing Lane Alternative. The first includes no geometric improvements at intersections throughout the corridor. The second includes the addition of mainline left-turn bays at 9 intersections within the study limits. The addition of mainline leftturn lanes increases the amount of no-passing zones within the corridor due to increased storage lengths and/or the addition of medians at the proposed intersection improvement locations. Calculations for the no-passing zone percentages for the No-Build, Passing Lane Alternative (without lefts), Passing Lane Alternative (with lefts), and the Hybrid Alternative (which includes the left-turn improvements at two-lane intersections in Sheboygan County) are shown in Attachment E. A summary of the no-passing zone percentages is shown in Table 8.

| Alternative and Analysis Section | No-Passing Zone \% <br> (without lefts) | No-Passing Zone \% <br> (with lefts) |
| :--- | :---: | :---: |
| No-Build: County UU to County G | $45 \%$ |  |
| No-Build: County G to Climbing Lane EB | $32 \%$ |  |
| No-Build: Climbing Lane EB Analysis: <br> County G to West of County P | $50 \%$ | Not Analyzed |

Table 8: Mainline No-Passing Zone Percentage Summary

## 7. No-Passing Zone Percentages

No-passing zone percentages were calculated for each analysis section using stationing from alignment files provided by WisDOT Northeast region staff.

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## Section 4: Four-lane Highway and Interchange Merge/Diverge Analysis

The four-lane highway analysis for this study uses controlling (i.e. highest volume) 2040 peak hour volumes to determine the controlling basic, merge or diverge segment to analyze at proposed interchanges. In the 4-lane On-alignment Alternative, interchanges are proposed at WIS 23/County UU and at WIS 23/County G. Attachment C shows a breakdown of the projected 2040 AM and PM peak hour traffic volumes for the WB merge, WB diverge, EB merge, EB diverge, and basic segments at each interchange location. The WB merge during the 2040 PM peak hour was determined to be the controlling interchange segment at each location. At the proposed WIS 23/County G interchange, the EB diverge was reviewed as well due to slightly higher ramp volumes.

To determine the mainline volume upstream of the WB merge, the K30 Analysis Direction Volume was found from Site 201147 for the County UU interchange and from Site 590118 for the County G interchange. A similar process was used for the EB diverge analysis at County G. The basic sections of WIS 23 east and west of each interchange were also reviewed for the 4-lane highway analysis. The mainline volumes for the HCS analysis are also shown in Attachment C, along with the corresponding ramp volume and upstream or downstream ramp volume for each interchange location. The results for the interchange analysis are intended to show the "worst-case" 4-lane segment within the study corridor.

## Section 5: Intersection Analysis

The intersections being analyzed in this study are County UU, County W/Loehr Road, and County G.

Inputs into the intersection analysis include:

1. Volumes: From WisDOT AM and PM peak hour traffic forecasts prepared April 6, 2018.
2. Peak Hour Factor: Overall intersection value from traffic counts performed in Summer 2017 per FDM 11-5-3.5.3.2.2.
3. Truck Percentage: Intersection approach value from traffic counts performed in Summer 2017. For the Restricted Crossing U-Turn (RCUT), or J-Turn, analysis, the truck percentages for individual movements were used in order to accurately represent the U-turn movements with this intersection treatment.
4. Headway Factors: Default headway settings were used for the two-way stop control analysis. For the U-turn movements at the proposed J-Turns, critical headway and follow-up headway values were calculated based on guidance from Page 23-77 of the HCM. These calculations are included in Attachment F.
5. Median Storage (No-Build): Per site conditions
6. Median Storage (Passing Lane with lefts, Hybrid, 4-Lane): One vehicle

WisDOT forecasts were provided for the No-Build and 4-lane On-alignment Alternative at each location analyzed. For the Passing Lane Alternative, the mainline forecasts are slightly higher than the No-Build forecasts within the two-lane portion of the corridor. In order to analyze the same intersections with the Passing Lane Alternative, the study team factored the 2040 No-Build intersection forecasts up (all movements) based on the relationship between the Passing Lane mainline forecast and No-Build mainline forecast on both sides of the study intersection. Similarly for the Hybrid Alternative,

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the 2040 4-lane On-alignment Alternative forecasts were factored down (all movements) based on the relationship between the Hybrid and 4-lane On-alignment mainline forecasts. These example calculations are shown in Attachment F.

At the proposed interchanges in the Hybrid Alternative and 4-lane On-alignment Alternative, singlelane roundabouts are proposed at the ramp terminal intersections. The alternative intersection methodology (HCM Chapter 23) will be used to supplement the control-delay based operations analysis of the proposed J-Turn at the County W/Loehr Road intersection in the Hybrid Alternative and 4-lane On-alignment Alternative.

## Section 6: Summary

## 1. WisDOT Review

The study team received approval from the WisDOT BTO on the proposed software (HCS) and modeling methodology for the WIS 23 traffic analysis on October 5, 2017. A peer review of the HCS files were performed by WisDOT BTO in April 2018 based on the April 6, 2018 traffic forecasts. The two-lane mainline analysis and results were approved on April 9, 2018. The fourlane mainline and intersection analyses were approved on April 12, 2018. The peer review documentation is located in Attachment G.

## 2. Operations Results

Summary tables detailing results of the mainline and intersection operations results are included in Attachment H. The mainline operations analysis contains two sets of results based on varying Peak Hour Factor (PHF) inputs, as described in the "DHV for WIS 23 Evaluation" memo located in Appendix A of the 2018 LS SEIS. The fully uniform analysis (PHF of 1.0) follows WisDOT policy and is used to report operations in the body of the 2018 LS SEIS. The existing peak hour pattern (PHF of 0.89 ) is a sensitivity analysis used to evaluate 2040 conditions along WIS 23 if peaking patterns remain the same as 2017 conditions.

Analysis of probe data (GPS data from phones or vehicles) for the WIS 23 corridor indicates that travel speeds on WIS 23 vary from those predicted by HCS. The probe data speeds, from the National Performance Management Research Data Set (NPMRDS), were downloaded from June 2017 to coincide with the dates the mainline traffic counts were taken along the two-lane sections of WIS 23. Average speeds from the NPMRDS probe data were found to be approximately 58 miles per hour along WIS 23. Average travel speeds predicted with HCS are around 48 miles per hour for 2017 conditions.

The NPMRDS travel speed data is considered more reliable than HCS by WisDOT for use in evaluating speeds and travel times along WIS 23 because the probe data reflects observed, and not predicted, travel speeds. For the 2040 alternatives analysis, the relative difference in speeds predicted by HCS was used in combination with the 2017 probe data to estimate 2040 speeds and travel times along the corridor. Attachment H shows example calculations of estimated speeds and travel times for the existing conditions and alternatives analysis.

ATTACHMENT A SCHEMATIC MAPS OF MAINLINE ALTERNATIVES

## WIS 23 (US 151 - County P) Alternatives

Passing Lane Alternative


Hybrid Alternative


4-lane On-alignment Alternative


ATTACHMENT B



PASSING LANE ALTERNATIVE


Westbound
HYBRID ALTERNATIVE

ATTACHMENT C
WIS 23 MAINLINE TRAFFIC ANALYSIS INPUT WORKSHEETS

## Projected Traffic Volumes: No Build Alternative

| CTH UU to CTH G | Site ID | Distance (ft) | Distance (mi) | Forecast Data |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 2017 | 2020 | 2030 | 2040 |
| CTH UU to Tower | 201147 | 10,490 | 2.0 | 7,400 | 7,500 | 7,900 | 8,300 |
| Tower to Hinn/W | 206104 | 15,980 | 3.0 | 7,300 | 7,400 | 7,600 | 7,900 |
| Hinn/W to Loehr/W | 200222 | 2,610 | 0.5 | 7,400 | 7,500 | 7,600 | 7,800 |
| Loehr/W to Hillview | 200224 | 17,000 | 3.2 | 6,900 | 7,000 | 7,000 | 7,100 |
| Hillview to CTH G | 201153 | 5,420 | 1.0 | 6,800 | 6,800 | 6,800 | 6,900 |


|  |  | 2017 | 2020 | 030 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CTH UU to CTH G (used 2017 base conditions and no-build) |  |  |  |  |  |
| Weigh |  | 7,140 | 7,230 | 7,380 | 7,610 |
| K30 | 0.10 | 714 | 723 | 738 | 761 |
| Peak Dir | 0.58 | 414 | 419 | 428 | 441 |
| Opp Dir | 0.42 | 300 | 304 | 310 | 320 |

Total Dist (ft) Total Dist (mi)
$51,500 \quad 9.8$ CTH UU to CTH G

Truck \% = 1
errain = Level (<3\%)


Truck \% = 13
Terrain $=$ Rolling ( $>3 \%$ in areas)
Note: All AADT volumes reported are from WisDOT forecast completed 4-6-2018, Appendix A (NERTDM only)

|  |  | 17 | 2020 | 2030 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| EB: CTH G to Climbing Lane |  |  |  |  |  |
| Weighted AADT |  | 7,140 | 7,150 | 7,160 | 7,260 |
| K30 | 0.10 | 714 | 715 | 716 | 726 |
| Peak Dir | 0.58 | 414 | 415 | 415 | 421 |
| Opp Dir | 0.42 | 300 | 300 | 301 | 305 |
| EB: CTH G to west of CTH P (Climbing Lane analysis) |  |  |  |  |  |
| Weighted AADT |  | 7,570 | 7,610 | 7,640 | 7,740 |
|  | 0.10 | 757 | 761 | 764 | 774 |
|  | 0.58 | 439 | 441 | 443 | 449 |
|  | 0.42 | 318 | 320 | 321 | 325 |

WB: Climbing Lane only

| Weighted AADT |  | 8,910 | 9,010 | 9,110 | 9,210 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| K30 | $\mathbf{0 . 1 0}$ | 891 | 901 | 911 | 921 |
| Peak Dir | $\mathbf{0 . 5 8}$ | 517 | 523 | 528 | 534 |
| Opp Dir | $\mathbf{0 . 4 2}$ | 374 | 378 | 383 | 387 |

WB: Climbing Lane to CTH G

| Weighted AADT | 7,290 | 7,310 | 7,330 | 7,430 |  |
| :--- | :--- | ---: | ---: | ---: | ---: |
| K30 | $\mathbf{0 . 1 0}$ | 729 | 731 | 733 | 743 |
| Peak Dir | $\mathbf{0 . 5 8}$ | 423 | 424 | 425 | 431 |
| Opp Dir | $\mathbf{0 . 4 2}$ | 306 | 307 | 308 | 312 |

Assumptions
K30 from ATR 590608
DD from ATR 590608
Truck \% from field data (PM peak)
See DHV for WIS 23 Evaluation memo and Traffic Modeling Methodology memo for more background.

Passing Lane Length, Volume, and Truck Percentage Summary: Passing Lane Alternative and Hybrid Alternativ

|  |  | Distance (t) | Distance (mi) | 2017 | Forecast Data |  | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Road Segment | Site ID |  |  |  | 2020 | 2030 |  |
| CTHUU to Tower | 201147 | 10,490 | 2.0 | 7,400 | 7,500 | 8,000 | 8,500 |
| Tower to Hinn/W | 206104 | 15,980 | 3.0 | 7,300 | 7.400 | 7.800 | 8.100 |
| Hinn/W to Loenr/W | 200222 | 2,610 | 0.5 | 7,400 | 7,500 | 7,700 | 8,000 |
| Loehrw to Hillview | 200224 | 17,000 | 3.2 | 6,900 | 7,000 | 7,100 | 7,300 |
| Hillvew to CTH G | 201153 | 5,420 | 1.0 | 6,800 | 6,800 | 7,000 | 7,100 |
| SHEBOYGAN COUNTY |  |  |  |  |  |  |  |
| CTH G to CTH P - Passing Lane Alternative |  | Distance (ft) | Distance (mi) |  | Forecast Data |  | 2040 |
| Road Segment | Site ID |  |  | 2017 | 2020 | 2030 |  |
| CTH G to CTH T (N) | 590118 | 19,600 | 3.7 | 6,700 | 6,700 | 6,900 | 7,000 |
| CTH T (N) to CTH A | 591421 | 7,450 | 1.4 | 7,800 | 7,800 | 8,000 | 8,100 |
| СтНA to Стн S | 591422 | 9,730 | 1.8 | 8,400 | 8,500 | 8,700 | 8,800 |
| CTH S to CTH P | 590195 | 5,520 | 1.0 | 9,400 | 9,500 | 9,700 | 9,900 |
| SHEBOYGAN COUNTY |  |  |  |  |  |  |  |
| CTH G to CTH P - Hybrid Alternative |  | Distance (ft) |  |  | Forecast Data |  |  |
| Road Segment | Site ID |  | Distance (mi) | 2017 | 2020 | 2030 | 2040 |
| CTH G to CTH T (N) | 590118 | 19,600 | 3.7 | 6,700 | 6,800 | 7,400 | 7,900 |
| CTH T (N) to CTH A | 591421 | 7,450 | 1.4 | 7,800 | 7,900 | 8,500 | 9,000 |
| CTHA to CTH S | 591422 | 9,730 | 1.8 | 8,400 | 8,600 | 9,100 | 9,600 |
| CTH to $^{\text {CTH }} \mathrm{P}$ | 590195 | 5,520 | 1.0 | 9,400 | 9,600 | 10,100 | 10,600 |
| TRUCK PERCENTAGES |  |  |  |  |  |  |  |
| Fond du Lac County | 17.0\% | from field data |  |  |  |  |  |
| Sheboygan County | 13.0\% | from field data |  |  |  |  |  |
| Weighted Average Truck Percentages for Passing Lane Analysis HCM Exhibit 15-23 Downstream |  |  |  |  |  |  |  |
| Scenario | ${ }^{\text {FDL }}$ | Sheb | Truck \% |  | Directional | Length |  |
| 2 A - Passing Lane Alt | $\frac{\text { dist (mi) }}{9.8}$ | $\frac{\text { dist (mi) }}{0.0}$ |  |  |  | PTSF (mi) | ATS (m) |
| 2 B - Passing Lane Alt | 9.8 | 0.0 | 17.0\% |  | <200 | 13.0 | 1.7 |
| 2 C - Passing Lane Alt | 6.4 | 5.7 | 15.1\% |  | 300 | 11.6 | 1.7 |
| 2D - Passing Lane Alt | 1.9 | 6.4 | 13.9\% |  | 400 | 8.1 | 1.7 |
| CLEB - Passing Lane Alt | 0.0 | 6.3 | 13.0\% |  | 500 | 7.3 | 1.7 |
| CL WB - Passing Lane Alt | 0.0 | 1.1 | 13.0\% |  | 600 | 6.5 | 1.7 |
| 2 C - Hybrid Alt | 0.0 | 5.7 | 13.0\% |  | 700 | 5.7 | 1.7 |
| 2 D - Hybrid Alt | 0.0 | 6.5 | 13.0\% |  | 800 | 5.0 | 1.7 |
| CL EB-Hybrid Alt | 0.0 | 6.3 | 13.0\% |  | 900 | 4.3 | 1.7 |
| CL WB-Hybrid Alt | 0.0 | 1.1 | 13.0\% |  | >1,000 | 3.6 | 1.7 |
| Divider for FDL vs. Sheb measured from CTH G , just west of actual county line. |  |  |  |  |  |  |  |
| 2A - Passing Lane Alternative |  |  |  |  |  |  |  |
| Category |  | Length | Limits |  |  |  |  |
|  | Upstream | 2.3 | E of Tower to CTH UUSta $332+00$ to $375+00$ |  |  |  |  |
| Passing Lane <br> Passing Lane Tapers |  | ${ }_{7} 300$ |  |  |  |  |  |
|  |  | 700 |  |  |  |  |  |
| Passing Lane Length + Tapers <br> Downstream Eff. Length |  | 1.1 6.4 |  |  |  |  | Total |
| Downstream in Eff. Length (HCM) |  | 7.7 |  |  |  |  | 9.8 |

2C - Passing Lane Alternative

| Category | Length | Limits |  |
| :---: | :---: | :---: | :---: |
| Upstream | 6.6 | to end of 2 A (East of Poplar) |  |
| Passing Lane | 4890 | Sta $737+90$ to $786+80$ |  |
| Passing Lane Tapers | 700 | $770{ }^{\circ}$ on each end |  |
| Passing Lane Length + Tapers | $\begin{aligned} & 1.2 \\ & 4.2 \end{aligned}$ | end of PL to Climbing Lane | Total |
| Downstream Eff. Length (HCM) | 7.8 | based on 434 vph | 12.0 |

2C - Hybrid Alternative


CLEB - Passing Lane Alternative

| Category | Length | Limits |  |
| :---: | :---: | :---: | :---: |
| Upstream | 4.2 | end of PL to Climbing Lane |  |
| Passing Lane | 3890 |  |  |
| Passing Lane Tapers (1) | 140 | Only on west end |  |
| Passing Lane Length + Tapers | 0.8 |  |  |
|  | $\begin{aligned} & 1.3 \\ & 7.4 \\ & \hline \end{aligned}$ | based on 483 vph | ${ }_{\text {Total }}{ }_{6}$ |



CL WB - Passing Lane and Hybrid Alternative


2D - Hybrid Alternative



WEIGHTED AVERAGE VOLUMES (WESTBOUND)
CL WB - Passing Lane Alternative

| Weighted ADT |  | 2017 | 2020 | 2030 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 8,910 | 9,010 | 9,210 | 9,360 |
| K30 | 0.10 | 891 | 901 | 921 | 936 |
| Peak Dir | 0.58 | 517 | 523 | 534 | 543 |
| Opp Dir | 0.42 | 374 | 378 | 387 | 393 |

CL WB - Hybrid Alternative


2D - Passing Lane Alternative


2D - Hybrid Alternative


2B - Passing Lane Alternative

te: All AADT volumes reported are from WisDOT forecast completed 4-6-2018, Appendix A (NERTDM only)
$\frac{\text { Assumptions }}{\text { K30 from ATR }} 5$
DD from ATR 590608
Truck \% from field data (PM peak)
See DHV for WIS 23 Evaluation memo and Traffic Modeling Methodology memo for more
ackground.

## Projected Traffic Volumes: 4-Lane On-Alignment Alternative (4 lanes CTH G to CTH P)

4/9/2018

| FOND DU LAC COUNTY |  |  |  | Forecast Data |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| CTH UU to CTH G |  |  |  |  |  |  |  |
| Road Segment | Site ID | Distance $(\mathrm{ft})$ | Distance (mi) | $\mathbf{2 0 1 7}$ | $\mathbf{2 0 2 0}$ | $\mathbf{2 0 3 0}$ | $\mathbf{2 0 4 0}$ |
| CTH UU to Tower | 201147 | 10,490 | 2.0 | 7,400 | 8,000 | 10,000 | 11,900 |
| Tower to Hinn/W | 206104 | 15,980 | 3.0 | 7,300 | 7,900 | 9,800 | 11,700 |
| Hinn/W to Loehr/W | 200222 | 2,610 | 0.5 | 7,400 | 7,900 | 9,600 | 11,200 |
| Loehr/W to Hillview | 200224 | 17,000 | 3.2 | 6,900 | 7,300 | 8,700 | 10,100 |
| Hillview to CTH G | 201153 | 5,420 | 1.0 | 6,800 | 7,200 | 8,500 | 9,900 |


| CTH UU to CTH G - not used in 4-lane operations analysis |
| :--- |
|  |
| Weighted AADT |
| 2017 |
| K30 |



| WB Merge Analysis <br> (2040 PM ramp vols) |  |
| ---: | ---: |
| Mainline Vol | 658 |
| Ramp Vol | 39 |

EB Diverge Analysis (2040 PM ramp vols)
Mainline Vol $\qquad$

## P SHEBOYGAN COUNTY



Note: All AADT volumes reported are from WisDOT forecast completed 4-6-2018, Appendix A (NERTDM only)

## Assumptions

K30 from ATR 590608
DD from ATR 590608
Truck \% from field data (PM peak)
See DHV for WIS 23 Evaluation memo and Traffic Modeling Methodology memo for more background.

| Traf |  |
| :---: | :--- |
|  |  |
| Site(s) | Route(s) |
| 201147 |  |
| 206104 | STH 23 |
| 200222 |  |
|  |  |
|  |  |


| Design Values (\%) |  |  |  |  |  |  |  |  | $\begin{array}{\|l\|l\|} \hline \text { AADTT } & 2 \mathrm{D} \\ \hline \end{array}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume(s) | Site Growth \% | K250 | K100 | K30 | P | D(Dsgn. Hr.) | T(DHV) | T(PHV) |  |  |
| 8300 | 0.53\% | 9.3 | 10.0 | 10.7 | 12.4 | 60/40 | 19.1 | 10.2 | 1680 | 9.6 |
| 7890 | 0.34\% | 9.3 | 10.0 | 10.7 | 12.4 | 60/40 | 21.6 | 11.6 | 1880 | 12.1 |
| 7810 | 0.23\% | 9.3 | 10.0 | 10.7 | 12.5 | 60/40 | 19.6 | 10.5 | 1730 | 9.8 |




| Design Values (\%) |  |  |  |  |  |  |  |  |  |  | Truck Classification |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site(s) | Route(s) | Volume(s) | Site Growth \% | K250 | K100 | K30 | P | D(Dsgn. Hr.) | T(DHV) | T(PHV) | AADTT | 2D | 3AX | 2S1+2S2 | 3-S2 | DBL-BTM | Total \% |
| 201147 | STH 23 | 8520 | 0.66\% | 9.3 | 10.0 | 10.7 | 12.4 | 60/40 | 19.1 | 10.2 | 1680 | 9.6 | 2.6 | 2.1 | 8.1 | 0.2 | 22.7\% |
| 206104 |  | 8120 | 0.48\% | 9.3 | 10.0 | 10.7 | 12.4 | 60/40 | 20.6 | 11.0 | 1790 | 10.1 | 2.8 | 2.3 | 9.0 | 0.2 | 24.5\% |
| 200222 |  | 7990 | 0.34\% | 9.3 | 10.0 | 10.7 | 12.5 | 60/40 | 18.7 | 10.0 | 1650 | 7.5 | 2.1 | 2.6 | 9.9 | 0.2 | 22.3\% |



## Symbol Count

## -000-2017 Count

*000* 2011 Count
bolded, and underlined (000) 2020 AADT [000] 2030 AADT

0002040 AADT

## NOTES ON THE FORECAST:

1. This projection assumes that no major new traffic generators will be added to the development already included in the 2010/2045 Northeast Regional Travel Demand Model.
2. Design values provided on forecast report are statewide average values. Design values employed in operational analysis are specific to the STH 23 corridor
3. Single-unit and combination-unit truck percentages were taken from observed 2017 Wisconsin vehicle classification data. Statewide average data (RoadRunner 2016 AC14 report) were used to assign percentages to individual vehicle classifications.
4. From USH 151 to CTH UU, STH 23 is a Factor Group II (Urban-Other) roadway (indicating low to moderate fluctuation in traffic from a seasonal perspective). From CTH UU to CTH P, STH 23 is a Factor Group IV (Rural-Other) roadway (indicating low to moderate fluctuation in traffic from a seasonal perspective). From USH 151 to CTH UU, STH 23 is functionally classified as an Urban Principal Arterial ([14] - in count purposes.
5. The 2010/2045 Northeast Regional Travel Demand Model was used to complete this forecast.
6. Roadway improvements coded within the existing plus committed ( $\mathrm{E}+\mathrm{C}$ ) network of the 2010/2045 Northeast Regional Travel Demand Model (in addition to the STH 23 Majors Project - Passing Lanes Alternative) were assumed to be in place for the purposes of developing this forecast.


| Design Values (\%) |  |  |  |  |  |  |  |  |  |  | Truck Classification |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site(s) | Route(s) | Volume(s) | Site Growth \% | K250 | K100 | K30 | P | D(Dsgn. Hr.) | T(DHV) | T(PHV) | AADTT | 2D | 3AX | 2S1+2S2 | 3-S2 | DBL-BTM | Total \% |
| 201147 | STH 23 | 11940 | 2.67\% | 9.9 | 11.1 | 12.1 | 14.8 | 60/40 | 19.1 | 10.2 | 1680 | 9.6 | 2.6 | 2.1 | 8.1 | 0.2 | 22.7\% |
| 206104 |  | 11730 | 2.62\% | 9.9 | 11.1 | 12.1 | 14.8 | 60/40 | 21.6 | 11.6 | 1880 | 12.1 | 3.3 | 2.1 | 8.0 | 0.2 | 25.7\% |
| 200222 |  | 11230 | 2.24\% | 10.0 | 11.2 | 12.2 | 14.8 | 60/40 | 19.6 | 10.5 | 1730 | 9.8 | 2.7 | 2.2 | 8.4 | 0.2 | 23.3\% |



| Full Vehicle Classification |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\mathbf{N}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site(s) $\quad$ Route(s) | MC | CARS | SU2-4 | BUSES | SU2-6 | SU3 | SU4+ | ST4- | ST5 | ST6+ | MU5- | MU6 | MU7+ | TRUCKS | TOTAL |  |
| STH 23 | 0.5 | 58.6 | 18.2 | 2.1 | 7.6 | 1.8 | 0.8 | 2.1 | 7.6 | 0.5 | 0.1 | 0.0 | 0.0 | 22.7 | 100.0 |  |
|  | 0.5 | 56.4 | 17.5 | 2.6 | 9.5 | 2.3 | 1.0 | 2.1 | 7.5 | 0.5 | 0.1 | 0.0 | 0.0 | 25.7 | 100.0 |  |
|  | 0.5 | 58.2 | 18.1 | 2.1 | 7.7 | 1.9 | 0.8 | 2.2 | 7.9 | 0.5 | 0.1 | 0.0 | 0.0 | 23.3 | 100.0 |  |
|  | 0.5 | 56.7 | 17.6 | 2.8 | 10.3 | 2.5 | 1.1 | 1.7 | 6.2 | 0.4 | 0.1 | 0.0 | 0.0 | 25.2 | 100.0 |  |
|  | 0.5 | 57.3 | 17.8 | 2.2 | 8.0 | 1.9 | 0.8 | 2.3 | 8.5 | 0.5 | 0.1 | 0.1 | 0.0 | 24.5 | 100.0 |  |
| 590118 | 0.5 | 58.9 | 18.3 | 1.6 | 5.9 | 1.4 | 0.6 | 2.6 | 9.4 | 0.6 | 0.1 | 0.1 | 0.0 | 22.3 | 100.0 |  |
| SITE ID = Colored, bolded, and underlined |  |  | NOTES ON THE FORECAST: |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Symbol Count | Symbol | Forecast |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -000-2017 Count | (000) | 2020 AADT | 2. Design values provided on forecast report are statewide average values. Design values employed in operational analysis are specific to the STH 23 corridor. <br> 3. Single-unit and combination-unit truck percentages were taken from observed 2017 Wisconsin vehicle classification data. Statewide average data (RoadRunner 2016 AC14 report) were used to assign percentages to individual vehicle classifications. <br> 4. From USH 151 to CTH UU, STH 23 is a Factor Group II (Urban-Other) roadway (indicating low to moderate fluctuation in traffic from a seasonal perspective). From CTH UU to CTH P, STH 23 is a Factor Group IV (Rural-Other) roadway (indicating low to moderate fluctuation in traffic from a seasonal perspective). From USH 151 to CTH P, STH 23 is functionally classified as an expressway (in the STH 23 Majors - Four-Lane Build Alternative) for count purposes. <br> 5. The 2010/2045 Northeast Regional Travel Demand Model was used to complete this forecast. |  |  |  |  |  |  |  |  |  |  |  |  |  |
| *000* 2011 Count | [000] | 2030 AADT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| +000+ 2005 Count |  | 2040 AADT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 6. Roadway improvements coded within the existing plus committed ( $E+C$ ) network of the 2010/2045 Northeast Regional Travel Demand Model (including the STH 23 Majors Project - Four-Lane Build) were assumed to be in place for the purposes of developing this forecast. |  |  |  |  |  |  |  |  |  |  |  |  |  |

ATTACHMENT D ACCESS DENSITY CALCULATIONS


WIS 23 Two-Lane Highway Analysis: Access Point Summary
October 2, 2017
"starting" limit included in each segment
Access Point Summary: EB Analyses

| Sideroads or Landmarks |  | Lengths by Stations |  |  | \# of Access Points | Access Points |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | End | $\begin{gathered} \text { STA } \\ \text { (start) } \end{gathered}$ | $\begin{aligned} & \text { STA } \\ & \text { (end) } \end{aligned}$ | Total (ft) |  | Dist (mi) | per Mile |
| CTH UU | Tower Rd | 203+50 | 308+40 | 10,490 | 32 | 2.0 | 16 |
| Tower Rd | 2A start | $308+40$ | $325+00$ | 1,660 | 6 | 0.3 | 19 |
| 2A start | 2A end | $325+00$ | 382+00 | 5,700 | 9 | 1.1 | 8 |
| 2A end | 7 Hills Rd | 382+00 | 415+00 | 3,300 | 9 | 0.6 | 14 |
| Tower Rd | 7 Hills Rd | 308+40 | 415+00 | 10,660 | 24 | 2.0 | 12 |
| 7 Hills Rd | W (S) | 415+00 | 468+00 | 5,300 | 12 | 1.0 | 12 |
| W (S) | W (N) | 468+00 | $494+25$ | 2,625 | 9 | 0.5 | 18 |
| W (N) | Log Tavern | 494+25 | 535+10 | 4,085 | 8 | 0.8 | 10 |
| Log Tavern | Pit | 535+10 | 580+00 | 4,490 | 11 | 0.9 | 13 |
| Pit | Banner | 580+00 | 607+60 | 2,760 | 7 | 0.5 | 13 |
| Banner | Triple T | 607+60 | $633+50$ | 2,590 | 11 | 0.5 | 22 |
| Triple T | Hillview | $633+50$ | 662+60 | 2,910 | 6 | 0.6 | 11 |
| Hillview | CTH G | 662+60 | 718+50 | 5,590 | 14 | 1.1 | 13 |
| CTH G | 2C start | 718+50 | 730+90 | 1,240 | 6 | 0.2 | 26 |
| 2C start | 2C end | 730+90 | 793+80 | 6,290 | 14 | 1.2 | 12 |
| 2C end | CTH U | $793+80$ | 804+50 | 1,070 | 2 | 0.2 | 10 |
| CTH G | Division Rd | 718+50 | 745+50 | 2,700 | 9 | 0.5 | 18 |
| Division Rd | CTH U | $745+50$ | $804+50$ | 5,900 | 13 | 1.1 | 12 |
| CTH U | Spring Valley Dr | 804+50 | $861+25$ | 5,675 | 12 | 1.1 | 11 |
| Spring Valley Dr | Scenic View Dr | $861+25$ | $888+80$ | 2,755 | 4 | 0.5 | 8 |
| Scenic View Dr | CTH T (N) | $888+80$ | $914+90$ | 2,610 | 5 | 0.5 | 10 |
| CTH T (N) | Sugarbush Rd | 914+90 | 970+10 | 5,520 | 8 | 1.0 | 8 |
| Sugarbush Rd | CTH A | 970+10 | 988+00 | 1,790 | 3 | 0.3 | 9 |
| CTH A | CL start | 988+00 | 1018+00 | 3,000 | 8 | 0.6 | 14 |
| CL start | CL end | 1018+00 | 1058+00 | 4,000 | 6 | 0.8 | 8 |
| CL end | CTH S | 1058+00 | 1086+00 | 2,800 | 5 | 0.5 | 9 |
| CTH S | W of CTH P | 1086+00 | 1126+50 | 4,050 | 8 | 0.8 | 10 |
| No-Build - CTH UU to CTH G |  |  |  |  | 134 | 10 | 14 |
| No-Build - CTH G to Climbing Lane Start No-Build - Climbing Lane Analysis: CTH G to W of CTH P |  |  |  |  | 62 | 6 | 11 |
|  |  |  |  |  | 81 | 8 | 10 |
| Passing Lane Alt 2A - CTH UU to CTH G |  |  |  |  | 134 | 10 | 14 |
| Passing Lane Alt 2C-End of 2A to Climbing Lane Start |  |  |  |  | 149 | 12 | 12 |
| Passing Lane Alt - Climbing Lane Analysis: End of 2C to W of CTH P |  |  |  |  | 61 | 6 | 10 |
| Hybrid Alt - CTH UU to CTH G (4-Lane) |  |  |  |  | --- | --- | --- |
| Hybrid Alt 2C - CTH G to Climbing Lane Start |  |  |  |  | 62 | 6 | 11 |
| Hybrid Alt - Climbing Lane Analysis: End of 2C to W of CTH P |  |  |  |  | 61 | 6 | 10 |

Note: Starting sideroad included in each segment, counted from west to east.

WIS 23 Two-Lane Highway Analysis: Access Point Summary
October 2, 2017
"starting" limit included in each segment
Access Point Summary: WB Analyses

| Sideroads or Landmarks |  | Lengths by Stations |  |  | \# of Access Points | Access Points |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | End | $\begin{gathered} \text { STA } \\ \text { (start) } \end{gathered}$ | $\begin{aligned} & \text { STA } \\ & \text { (end) } \end{aligned}$ | Total (ft) |  | Dist (mi) | per Mile |
| CTH UU | Tower Rd | 203+50 | 308+40 | 10,490 | 32 | 2.0 | 16 |
| Tower Rd | 7 Hills Rd | 308+40 | 415+00 | 10,660 | 24 | 2.0 | 12 |
| 7 Hills Rd | W (S) | 415+00 | 468+00 | 5,300 | 12 | 1.0 | 12 |
| W (S) | W (N) | 468+00 | 494+25 | 2,625 | 9 | 0.5 | 18 |
| W (N) | Log Tavern | $494+25$ | 535+10 | 4,085 | 8 | 0.8 | 10 |
| Log Tavern | Pit | 535+10 | 580+00 | 4,490 | 11 | 0.9 | 13 |
| Log Tavern | $2 B$ end | 535+10 | 550+50 | 1,540 | 5 | 0.3 | 17 |
| 2B end | 2B start | 550+50 | 618+00 | 6,750 | 18 | 1.3 | 14 |
| 2B start | Triple T | 618+00 | $633+50$ | 1,550 | 6 | 0.3 | 20 |
| Pit | Banner | 580+00 | 607+60 | 2,760 | 7 | 0.5 | 13 |
| Banner | Triple T | 607+60 | 633+50 | 2,590 | 11 | 0.5 | 22 |
| Triple T | Hillview | $633+50$ | 662+60 | 2,910 | 6 | 0.6 | 11 |
| Hillview | CTH G | 662+60 | 718+50 | 5,590 | 14 | 1.1 | 13 |
| CTH G | Division Rd | 718+50 | 745+50 | 2,700 | 9 | 0.5 | 18 |
| Division Rd | CTH U | 745+50 | $804+50$ | 5,900 | 13 | 1.1 | 12 |
| CTH U | Spring Valley Dr | $804+50$ | $861+25$ | 5,675 | 12 | 1.1 | 11 |
| CTH U | 2D end | $804+50$ | $848+65$ | 4,415 | 12 | 0.8 | 14 |
| 2D end | 2D start | $848+65$ | 907+65 | 5,900 | 7 | 1.1 | 6 |
| 2D start | CTH T (N) | 907+65 | 914+90 | 725 | 2 | 0.1 | 15 |
| Spring Valley Dr | Scenic View Dr | $861+25$ | $888+80$ | 2,755 | 4 | 0.5 | 8 |
| Scenic View Dr | CTH T (N) | $888+80$ | 914+90 | 2,610 | 5 | 0.5 | 10 |
| CTH T (N) | Sugarbush Rd | 914+90 | 970+10 | 5,520 | 8 | 1.0 | 8 |
| Sugarbush Rd | CTH A | 970+10 | 988+00 | 1,790 | 3 | 0.3 | 9 |
| CTH A | CL end (Ridge) | 988+00 | 1058+00 | 7,000 | 14 | 1.3 | 11 |
| CL end | CTH S | 1058+00 | 1086+00 | 2,800 | 5 | 0.5 | 9 |
| CTH S | CL start (Twinkle) | 1086+00 | 1115+00 | 2,900 | 6 | 0.5 | 11 |
| Twinkle | W of CTH P | 1115+00 | 1126+50 | 1,150 | 2 | 0.2 | 9 |
| No-Build - CTH G to CTH UU <br> No-Build - Climbing Lane End to CTH G <br> No-Build - Climbing Lane Analysis: Twinkle to Ridge |  |  |  |  | 134 | 10 | 14 |
|  |  |  |  |  | 68 | 6 | 11 |
|  |  |  |  |  | 11 | 1 | 10 |
| Passing Lane Alt 2B - CTH G to CTH UU |  |  |  |  | 134 | 10 | 14 |
| Passing Lane Alt 2D-Climbing Lane End to Start of 2B |  |  |  |  | 94 | 8 | 11 |
| Passing Lane Alt - Climbing Lane Analysis: Twinkle to Ridge |  |  |  |  | 11 | 1 | 10 |
| Hybrid Alt - CTH G to CTH UU (4-Lane) |  |  |  |  | --- | --- | --- |
| Hybrid Alt 2D-Climbing Lane End to CTH G |  |  |  |  | 68 | 6 | 11 |
| Hybrid Alt - Climbing Lane Analysis: Twinkle to Ridge |  |  |  |  | 11 | 1 | 10 |

Note: Starting sideroad included in each segment, counted from west to east.

ATTACHMENT E NO-PASSING ZONE CALCULATIONS

## WIS 23 Two-Lane Highway Analysis: No-Passing Zone Summary

October 2, 2017

## Eastbound No-Passing Zone Calcs



## WIS 23 Two-Lane Highway Analysis: No-Passing Zone Summary (With Left-turn Lanes)

October 2, 2017

| Sideroads or Landmarks |  | Lengths by Stations |  |  | Measured from Google Aerials and Street View (Nov 2016) |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Distances (ft) |  |  | Passing \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | End | $\begin{gathered} \text { STA } \\ \text { (start) } \end{gathered}$ | STA <br> (end) | Total ( ft ) | Length 1 (ft) <br> Westernmost |  | Length 2 (ft) |  | Length 3 (ft) |  | Length 4 (ft) |  | Length 5 (ft) |  | Length 6 (ft) |  | Length 7(ft) |  | Length 8 (ft) | Passing | $\begin{gathered} \text { No } \\ \text { Passing } \\ \hline \end{gathered}$ | Total |  |
| CTH UU | Tower Rd | 203+50 | 308+40 | 10,490 | 1,050 | NP | 3,360 | Pass | 820 | NP | 2,150 | Pass | 880 | NP | 945 | Pass | 1,285 | NP |  | 6,455 | 4,035 | 10,490 | 38\% |
| Tower Rd | 2A start | 308+40 | $325+00$ | 1,660 | 1,660 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 1,660 | 1,660 | 100\% |
| 2A start | 2 A end | $325+00$ | $382+00$ | 5,700 | 2,320 | Pass | 1,400 | NP | 1,700 | Pass | 280 | NP |  |  |  |  |  |  |  | 4,020 | 1,680 | 5,700 | 29\% |
| 2 A end | 7 Hills Rd | 382+00 | $415+00$ | 3,300 | 3,300 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 3,300 | 3,300 | 100\% |
| Tower Rd | 7 Hills Rd | 308+40 | $415+00$ | 10,660 | 1,660 | Pass | 2,320 | Pass | 1,400 | NP | 1,700 | Pass | 3,580 | NP |  |  |  |  |  | 5,680 | 4,980 | 10,660 | 47\% |
| 7 Hills Rd | w (s) | $415+00$ | 468+00 | 5,300 | 770 | NP | 735 | NP | 2,035 | Pass | 1,690 | NP | 70 | NP |  |  |  |  |  | 2,035 | 3,265 | 5,300 | 62\% |
| W (s) | W ( N ) | $468+00$ | 494+25 | 2,625 | 2,625 | nP |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 2,625 | 2,625 | 100\% |
| W (N) | Log Tavern | 494+25 | 535+10 | 4,085 | 240 | NP | 575 | Pass | 1,190 | NP | 415 | Pass | 1,665 | NP |  |  |  |  |  | 990 | 3,095 | 4,085 | 76\% |
| Log Tavern | Pit | 535+10 | 580+00 | 4,490 | 1,660 | Pass | 1,230 | NP | 1,600 | Pass |  |  |  |  |  |  |  |  |  | 3,260 | 1,230 | 4,490 | 27\% |
| Pit | Banner | 580+00 | 607+60 | 2,760 | 690 | Pass | 1,540 | NP | 530 | Pass |  |  |  |  |  |  |  |  |  | 1,220 | 1,540 | 2,760 | 56\% |
| Banner | Triple T | 607+60 | 633+50 | 2,590 | 440 | Pass | 2,150 | NP |  |  |  |  |  |  |  |  |  |  |  | 440 | 2,150 | 2,590 | 83\% |
| Triple T | Hillview | 633+50 | 662+60 | 2,910 | 1,740 | Pass | 1,170 | NP |  |  |  |  |  |  |  |  |  |  |  | 1,740 | 1,170 | 2,910 | 40\% |
| Hillview | CTH G | 662+60 | 718+50 | 5,590 | 2,740 | NP | 1,000 | Pass | 650 | NP | 1,200 | NP |  |  |  |  |  |  |  | 1,000 | 4,590 | 5,590 | 82\% |
| CTH G | 2C start | $718+50$ | 730+90 | 1,240 | 1,240 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 1,240 | 1,240 | 100\% |
| 2C start | 2 Cend | 730+90 | 793+80 | 6,290 | 1,460 | NP | 2,110 | NP | 1,330 | Pass | 1,160 | NP | 230 | NP |  |  |  |  |  | 1,330 | 4,960 | 6,290 | 79\% |
| 2 C end | CTH U | 793+80 | 804+50 | 1,070 | 1,070 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 1,070 | 1,070 | 100\% |
| CTH G | Division Rd | $718+50$ | 745+50 | 2,700 | 2,700 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 2,700 | 2,700 | 100\% |
| Division Rd | CTH U | $745+50$ | 804+50 | 5,900 | 2,110 | np | 1,330 | Pass | 1,160 | NP | 1,300 | NP |  |  |  |  |  |  |  | 1,330 | 4,570 | 5,900 | 77\% |
| CTH U | Spring Valley Dr | 804+50 | 861+25 | 5,675 | 1,650 | NP | 4,025 | Pass |  |  |  |  |  |  |  |  |  |  |  | 4,025 | 1,650 | 5,675 | 29\% |
| Spring Valley Dr | Scenic View Dr | 861+25 | 888+80 | 2,755 | 170 | Pass | 2,585 | NP |  |  |  |  |  |  |  |  |  |  |  | 170 | 2,585 | 2,755 | 94\% |
| Scenic View Dr | CTH T ( $)^{\text {) }}$ | 888+80 | 914+90 | 2,610 | 520 | NP | 2,090 | NP |  |  |  |  |  |  |  |  |  |  |  | 0 | 2,610 | 2,610 | 100\% |
| CTH T ( N ) | Sugarbush Rd | 914+90 | 970+10 | 5,520 | 1,285 | NP | 4,235 | Pass |  |  |  |  |  |  |  |  |  |  |  | 4,235 | 1,285 | 5,520 | 23\% |
| Sugarbush Rd | CTH A | $970+10$ | $988+00$ | 1,790 | 105 | Pass | 1,685 | NP |  |  |  |  |  |  |  |  |  |  |  | 105 | 1,685 | 1,790 | 94\% |
| Стн A | CL start | $988+00$ | 1018+00 | 3,000 | 1,290 | NP | 1,200 | Pass | 510 | NP |  |  |  |  |  |  |  |  |  | 1,200 | 1,800 | 3,000 | 60\% |
| CL start | CL end | 1018+00 | 1058+00 | 4,000 | 4,000 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 4,000 | 4,000 | 100\% |
| CL end | CTH S | 1058+00 | 1086+00 | 2,800 | 2,800 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 2,800 | 2,800 | 100\% |
| CTH S | W of CTH P | 1086+00 | $1126+50$ | 4,050 | 4,050 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 4,050 | 4,050 | 100\% |
|  | No-Passing stationing due to added left-turn lanes (NP overlap exists at some locations today) | 294+75 | $324+20$ | Tower | 2,945 | NP | Modified from "without left-turns" analysis |  |  |  | No-Passing Zone Calculations for HCS Analysis |  | No-Build - CTH UU to CTH G No-Build - CTH G to Climbing Lane Start No-Build - Climbing Lane Analysis: CTH G to W of CTH P |  |  |  |  |  |  | --- | --- | --- | -- |
|  |  | 398+95 | $430+05$ | 7 Hills | 3,110 | NP |  |  |  |  |  |  | --- | --- | --- | --- |  |
|  |  | 450+40 | 469+90 | CTH W (S) | 1,950 | NP |  |  |  |  |  |  | --- | --- | --- | --- |  |
|  |  | $500+00$ | $511+90$ | CTH W ( N ) | 1,190 | NP |  |  |  |  |  |  | Passing Lane Alt 2A - CTH UU to CTH G Passing Lane Alt 2C - End of 2A to Climbing Lane Start |  |  |  |  |  |  | 21,160 | 30,340 | 51,500 | 59\% |
|  |  | $700+00$ | $710+00$ | CTH G | 1,000 | NP |  |  |  |  |  |  | 21,750 | 41,850 | 63,600 | 66\% |  |
|  |  | 789+60 | $821+00$ | СтН U | 3,140 | NP |  |  |  |  |  |  | Passing Lane Alt - Climbing Lane Analysis: End of 2C to W of CTH P | 9,735 | 23,535 | 33,270 | 71\% |  |
|  |  | $898+80$ | 903+50 | CTH T | 470 | NP |  |  |  |  |  |  | Hybrid Alt - CTH UU to CTH G (4-Lane) <br> Hybrid Alt 2C - CTH G to Climbing Lane Start |  |  |  |  |  |  | -- | --- | --- | -- |
|  |  | 903+50 | 927+75 | CTH T | 2,425 | NP |  |  |  |  |  |  | 11,065 | 18,885 | 29,950 | 63\% |  |
|  |  | 971+15 | 1000+90 | CTH A | 2,975 | NP |  |  |  |  |  |  | Hybrid Alt - Climbing Lane Analysis: End of $2 C$ to $W$ of $C T H P$ | 9,735 | 23,535 | 33,270 | 71\% |  |

## WIS 23 Two-Lane Highway Analysis: No-Passing Zone Summary

October 2, 2017
Westbound No-Passing Zone Calcs

| Sideroads or Landmarks |  | Lengths by Stations |  |  | Measured from Google Aerials and Street View (Nov 2016) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Distances (ft) |  |  | Passing \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | End | $\begin{gathered} \text { STA } \\ \text { (start) } \end{gathered}$ | $\begin{aligned} & \hline \text { STA } \\ & \text { (end) } \\ & \hline \end{aligned}$ | Total (ft) | Length 1 (ft) <br> Easternmost |  | Length 2 (ft) |  | Length 3 ( ft ) |  | Length 4 (ft) |  | Length 5 (ft) |  | Length 6 (ft) |  | Length 7(ft) |  | Length 8 (ft) |  | Passing | $\begin{gathered} \text { No } \\ \text { Passing } \\ \hline \end{gathered}$ | Total |  |
| CTH UU | Tower Rd | 203+50 | 308+40 | 10,490 | 860 | Pass | 1,280 | NP | 3,060 | Pass | 2,830 | Pass | 2,460 | NP |  |  |  |  |  |  | 6,750 | 3,740 | 10,490 | 36\% |
| Tower Rd | 7 Hills Rd | 308+40 | $415+00$ | 10,660 | 2,210 | NP | 1,670 | Pass | 1,340 | NP | 5,440 | Pass |  |  |  |  |  |  |  |  | 7,110 | 3,550 | 10,660 | 33\% |
| 7 Hills Rd | W (s) | $415+00$ | $468+00$ | 5,300 | 3,160 | Pass | 2,140 | NP |  |  |  |  |  |  |  |  |  |  |  |  | 3,160 | 2,140 | 5,300 | 40\% |
| W (s) | w ( N ) | $468+00$ | 494+25 | 2,625 | 1,300 | NP | 1,325 | NP |  |  |  |  |  |  |  |  |  |  |  |  | , | 2,625 | 2,625 | 100\% |
| w ( N ) | Log Tavern | 494+25 | 535+10 | 4,085 | 200 | NP | 2,280 | Pass | 1,605 | nP |  |  |  |  |  |  |  |  |  |  | 2,280 | 1,805 | 4,085 | 44\% |
| Log Tavern | Pit | 535+10 | 580+00 | 4,490 | 1,680 | NP | 1,440 | Pass | 1,370 | NP |  |  |  |  |  |  |  |  |  |  | 1,440 | 3,050 | 4,490 | 68\% |
| Log Tavern | 2 Bend | 535+10 | 550+50 | 1,540 | 1,540 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 1,540 | 1,540 | 100\% |
| 2 B end | 2 Bstart | 550+50 | 618+00 | 6,750 | 290 | Pass | 750 | NP | 330 | NP | 1,680 | Pass | 750 | NP | 1,370 | NP | 1,440 | Pass | 140 | NP | 3,410 | 3,340 | 6,750 | 49\% |
| 2 B start | Triple T | 618+00 | 633+50 | 1,550 | 940 | NP | 610 | Pass |  |  |  |  |  |  |  |  |  |  |  |  | 610 | 940 | 1,550 | 61\% |
| Pit | Banner | 580+00 | 607+60 | 2,760 | 750 | NP | 1,680 | Pass | 330 | NP |  |  |  |  |  |  |  |  |  |  | 1,680 | 1,080 | 2,760 | 39\% |
| Banner | Triple T | 607+60 | 633+50 | 2,590 | 750 | NP | 900 | Pass | 940 | NP |  |  |  |  |  |  |  |  |  |  | 900 | 1,690 | 2,590 | 65\% |
| Triple T | Hillview | 633+50 | 662+60 | 2,910 | 1,500 | Pass | 1,410 | NP |  |  |  |  |  |  |  |  |  |  |  |  | 1,500 | 1,410 | 2,910 | 48\% |
| Hillview | CTH G | 662+60 | 718+50 | 5,590 | 2,270 | Pass | 3,120 | NP | 200 | Pass |  |  |  |  |  |  |  |  |  |  | 2,470 | 3,120 | 5,590 | 56\% |
| CTH G | Division Rd | 718+50 | 745+50 | 2,700 | 2,530 | NP | 170 | Pass |  |  |  |  |  |  |  |  |  |  |  |  | 170 | 2,530 | 2,700 | 94\% |
| Division Rd | Стн U | $745+50$ | 804+50 | 5,900 | 990 | NP | 1,310 | Pass | 3,600 | nP |  |  |  |  |  |  |  |  |  |  | 1,310 | 4,590 | 5,900 | 78\% |
| CTH U | Spring Valley Dr | 804+50 | $861+25$ | 5,675 | 5,525 | Pass | 150 | NP |  |  |  |  |  |  |  |  |  |  |  |  | 5,525 | 150 | 5,675 | 3\% |
| CTH U | 2 D end | 804+50 | 848+65 | 4,415 | 4,265 | Pass | 150 | NP |  |  |  |  |  |  |  |  |  |  |  |  | 4,265 | 150 | 4,415 | 3\% |
| 2 D end | 2 Dstart | 848+65 | 907+65 | 5,900 | 1,260 | Pass | 1,120 | NP | 2,135 | Pass | 1,385 | NP |  |  |  |  |  |  |  |  | 3,395 | 2,505 | 5,900 | 42\% |
| 2 s start | CTH T ( N ) | 907+65 | 914+90 | 725 | 725 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 725 | 725 | 100\% |
| Spring Valley Dr | Scenic View Dr | 861+25 | 888+80 | 2,755 | 1,120 | NP | 1,635 | Pass |  |  |  |  |  |  |  |  |  |  |  |  | 1,635 | 1,120 | 2,755 | 41\% |
| Scenic View Dr | CTH T ( N ) | 888+80 | 914+90 | 2,610 | 500 | Pass | 2,110 | NP |  |  |  |  |  |  |  |  |  |  |  |  | 500 | 2,110 | 2,610 | 81\% |
| CTH T ( N ) | Sugarbush Rd | 914+90 | 970+10 | 5,520 | 5,520 | Pass |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5,520 | 0 | 5,520 | 0\% |
| Sugarbush Rd | CTH A | 970+10 | 988+00 | 1,790 | 1,790 | Pass |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1,790 | 0 | 1,790 | 0\% |
| CTH A | CL end (Ridge) | 988+00 | 1058+00 | 7,000 | 340 | Pass | 1,550 | NP | 5,110 | Pass |  |  |  |  |  |  |  |  |  |  | 5,450 | 1,550 | 7,000 | 22\% |
| CL end | CTH S | 1058+00 | 1086+00 | 2,800 | 2,320 | NP | 480 | Pass |  |  |  |  |  |  |  |  |  |  |  |  | 480 | 2,320 | 2,800 | 83\% |
| CTH S | CL start (Twinkle) | 1086+00 | $1115+00$ | 2,900 | 2,900 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 2,900 | 2,900 | 100\% |
| Twinkle | W of CTH P | $1115+00$ | $1126+50$ | 1,150 | 1,150 | NP |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 1,150 | 1,150 | 100\% |
|  |  |  |  |  |  |  |  |  |  |  | No-Passing Zone Calculations for HCS Analysis |  | No-Build - CTH G to CTH UUNo-Build - Climbing Lane End to CTH GNo-Build - Climbing Lane Analysis: Twinkle to Ridge |  |  |  |  |  |  |  | 27,290 | 24,210 | 51,500 | 47\% |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 21,900 | 12,050 | 33,950 | 35\% |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 480 | 5,220 | 5,700 | 92\% |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | Passing Lane Alt $2 B$ - CTH G to CTH UU <br> Passing Lane Alt 2D-Climbing Lane End to Start of 2B |  |  |  |  |  |  |  | 27,290 | 24,210 | 51,500 | 47\% |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 26,480 | 17,520 | 44,000 | 40\% |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | Passing Lane Alt - Climbing Lane Analysis: Twinkle to Ridge |  |  |  |  |  |  |  | 480 | 5,220 | 5,700 | 92\% |
|  |  |  |  |  |  |  |  |  |  |  |  |  | --- | --- | --- | --- |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | Hybrid Alt 2D-Climbing Lane End to CTH G | --- | --- | --- | --- |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | Hybrid Alt - Climbing Lane Analysis: Twinkle to Ridge | 480 | 5,220 | 5,700 | 92\% |  |

## WIS 23 Two-Lane Highway Analysis: No-Passing Zone Summary (With Left-turn Lanes)

October 2, 2017
Westbound No-Passing Zone Calcs


## ATTACHMENT F

 PROJECTED INTERSECTION VOLUMESWIS 23/CTH UU Intersection Forecast Volumes
April 9, 2018


## 2040 No Build: PM Peak

Intersection volumes from WisDOT forecast (4-6-2018)


## 2040 Passing Lane Alt: AM Peak

Intersection volumes factored up based on WIS 23 mainline trends


## 2040 Passing Lane Alt: PM Peak

Intersection volumes factored up based on WIS 23 mainline trends


| Location | 2040 AADT |  | Growth |  |
| :---: | :---: | :---: | :---: | :---: |
|  | No-Build | Passing <br> Lane |  |  |
| Site <br> 201147 | CTH UU to <br> Tower | 8,300 | 8,500 | $2.4 \%$ |
|  |  |  |  |  |

Note: Site east of CTH K not used due to access changes as part of passing lane alternative.

WIS 23/CTH W (N) Intersection Forecast Volumes
April 9, 2018



2040 Passing Lane Alt: PM Peak


| Location |  | 2040 AADT |  | Growth Factor |
| :---: | :---: | :---: | :---: | :---: |
|  |  | No-Build | Passing |  |
| $\begin{gathered} \text { Site } \\ 200222 \end{gathered}$ | $\begin{gathered} \hline \mathrm{W}(\mathrm{~S}) \text { to } \\ \mathrm{W}(\mathrm{~N}) \\ \hline \end{gathered}$ | 7,800 | 8,000 | 2.6\% |
| $\begin{gathered} \hline \text { Site } \\ 200224 \\ \hline \end{gathered}$ | W (N) to Hillview | 7,100 | 7,300 | 2.8\% |
|  |  |  | Average | 2.7\% |

WIS 23/CTH G Intersection Forecast Volumes
April 9, 2018

2040 No Build: AM Peak
Intersection volumes from WisDOT forecast (4-6-2018)


## 2040 No Build: PM Peak

Intersection volumes from WisDOT forecast (4-6-2018)

## 2040 Passing Lane Alt: AM Peak

Intersection volumes factored up based on WIS 23 mainline trends


## 2040 Passing Lane Alt: PM Peak

Intersection volumes factored up based on WIS 23 mainline trends


| Location |  | 2040 AADT |  | Growth Factor |
| :---: | :---: | :---: | :---: | :---: |
|  |  | No-Build | Passing |  |
| $\begin{gathered} \hline \text { Site } \\ 201153 \end{gathered}$ | Hillview to | 6,900 | 7,100 | 2.9\% |
| $\begin{gathered} \hline \text { Site } \\ 590118 \end{gathered}$ | CTH G to CTH T (N) | 6,800 | 7,000 | 2.9\% |
|  |  |  | Average | 2.9\% |

WIS 23/CTH W - J-Turn Volume development (4-Lane On-Alignment and Hybrid) April 9, 2018

AM PEAK HOUR

4-lane On-Alignment Alternative Volumes (2040)
Intersection volumes from WisDOT forecast (4-6-2018)


4-lane On-Alignment and Hybrid Reduction Factor Development

| U-Turn Heavy Truck\% | $7.7 \%$ |  |
| ---: | :---: | :--- |
| Critical Headway | 4.55 | s |
| Follow Up Headway | 2.68 | s |
| CTH W to west U-Turn | 1,300 | ft |
| WB U-Turn storage | 450 | ft |


| U-Turn Heavy Truck\% | $0.0 \%$ |  |
| ---: | :---: | :--- | :--- |
| Critical Headway | 4.40 | s |
| Follow Up Headway | 2.60 | s |
| Loehr Rd to east U-Turn | 1,150 | ft |
| EB U-Turn storage | 450 | ft |
| Note: EB to WB U-turn includes |  |  |
| CTH W/Hinn NBL \& NBT in truck \% calc. |  |  |

CTH W/Hinn NBL \& NBT in truck \% calc.


WIS 23/CTH W - J-Turn Volume development (4-Lane On-Alignment and Hybrid) April 9, 2018

PM PEAK HOUR
4-lane On-Alignment Alternative Volumes (2040)
Intersection volumes from WisDOT forecast (4-6-2018)


U-Turn Heavy Truck\% 14.3\% Critical Headway 4.69
Follow Up Headway 2.74
CTH $W$ to west U-Turn $1,300 \mathrm{ft}$
WB U-Turn storage 450 ft

U-Turn Heavy Truck\% 17.2\%
Critical Headway 4.74
Follow Up Headway 2.77 s
Loehr Rd to east U-Turn 1,150 ft
EB U-Turn storage 450 ft
Note: EB to WB U-turn includes
CTH W/Hinn NBL \& NBT in truck \% calc.


WIS 23/CTH UU Interchange Volumes: 4-Lane On-Alignment and Hybrid Alternatives April 9, 2018

2040 4-Lane On-Alignment: AM Peak Intersection volumes from WisDOT forecast (4-6-2018)


2040 4-Lane On-Alignment: PM Peak Intersection volumes from WisDOT forecast (4-6-2018)


| Location |  | 2040 AADT |  | Factor |
| :---: | :---: | :---: | :---: | :---: |
|  | 4-Lane | Hybrid |  |  |
| Site <br> 200219 | West of <br> CTH UU | 16,700 | 15,600 | $93.4 \%$ |
| Site <br> 201147 | East of <br> CTH UU | 11,900 | 11,000 | $92.4 \%$ |
|  |  |  |  |  |

2040 Hybrid: AM Peak
Int volumes factored down based on WIS 23 mainline trends


WIS 23/CTH G Interchange Volumes: 4-Lane On-Alignment and Hybrid Alternatives April 9, 2018

2040 4-Lane On-Alignment: AM Peak Intersection volumes from WisDOT forecast (4-6-2018)

2040 4-Lane On-Alignment: PM Peak Intersection volumes from WisDOT forecast (4-6-2018)


| Location |  | 2040 AADT |  | Factor |
| :---: | :---: | :---: | :---: | :---: |
|  | 4-Lane | Hybrid |  |  |
| Site <br> 201153 | West of <br> CTH G | 9,900 | 8,800 | $88.9 \%$ |
| Site <br> 590118 | East of <br> CTH G | 9,500 | 7,900 | $83.2 \%$ |
|  |  |  |  |  |

2040 Hybrid: AM Peak
Int volumes factored down based on WIS 23 mainline trends




















| CTH W North/Loehr Rd (PM) |  |  |
| :---: | :---: | :---: |
| Year | West J-Turn | East J-Turn |
| 2020 | 30 | 25 |
| 2030 | 33 | 26 |
| 2040 | 35 | 27 |

## West J-Turn has existing CTH W North/Loehr Rd SBT and SBL

East J-Turn has existing CTH W North/Loehr Rd NBT and NBL as well as CTH W South/Hinn Rd NBT, NBL, and EBL

ATTACHMENT G WISDOT BTO PEER REVIEW

| From: | Rouleau, Benjamin M - DOT |
| :---: | :---: |
| To: | Urban, Joseph M.; Lipke, Bryan - DOT; Michaelson, لill - DOT |
| Cc: | DOT WIS 23-Major 1440-13/15-00/01; Lynch, Tom; Petersen, Joan; Kobryn, Jennifer; DOT Traffic Analysis \& Modeling; Szymkowski, Rebecca - DOT |
| Subject: | RE: WIS 23 - 2-Lane Operations Results (Draft 3-26-2018) |
| Date: | Thursday, April 12, 2018 3:56:16 PM |
| Attachments: | image001.png |
|  | dt1887 4-lane 4-12-18 2nd review.docx |
|  | dt1887 Intersections 4-12-18 2nd review.docx |

Joe,

Sounds good on everything. See attached for final DT1887s.

On the J-Turns, Vicki and I have discussed this and it's a little bit unclear what speed (posted or design or something else) should actually be used for calculating the EDTT. But 60 and 65 (ceiling) seem fine.

Ben

From: Urban, Joseph M. [mailto:Joseph.Urban@strand.com]
Sent: Thursday, April 12, 2018 9:57 AM
To: Rouleau, Benjamin M - DOT [Benjamin.Rouleau@dot.wi.gov](mailto:Benjamin.Rouleau@dot.wi.gov); Lipke, Bryan - DOT
[Bryan.Lipke@dot.wi.gov](mailto:Bryan.Lipke@dot.wi.gov); Michaelson, Jill - DOT [Jill.Michaelson@dot.wi.gov](mailto:Jill.Michaelson@dot.wi.gov)
Cc: DOT WIS 23-Major 1440-13/15-00/01 [DOTWIS23-Major1440-13/15-00/01@dot.wi.gov](mailto:DOTWIS23-Major1440-13/15-00/01@dot.wi.gov); Lynch,
Tom [Tom.Lynch@strand.com](mailto:Tom.Lynch@strand.com); Petersen, Joan [Joan.Petersen@strand.com](mailto:Joan.Petersen@strand.com); Kobryn, Jennifer
[Jennifer.kobryn@strand.com](mailto:Jennifer.kobryn@strand.com); DOT Traffic Analysis \& Modeling
[DOTTrafficAnalysisModeling@dot.wi.gov](mailto:DOTTrafficAnalysisModeling@dot.wi.gov); Szymkowski, Rebecca - DOT
[Rebecca.Szymkowski@dot.wi.gov](mailto:Rebecca.Szymkowski@dot.wi.gov)
Subject: RE: WIS 23-2-Lane Operations Results (Draft 3-26-2018)

Thanks again for the quick turnaround on the comments Ben.

We've reviewed and have made a couple of revisions to the J-turn analysis files and results, mainly with the speeds associated with the Hybrid Alternative. Overall, the results are similar in terms of delay, travel time, and LOS. Please see the attached DT1887 responses for more discussion on the intersection revisions and for the 4-lane analysis at CTH G.

For the TWSC at the interchange ramp terminals, we propose making a note in the environmental document that roundabouts or TWSC could be considered (as design progresses).

Let me know if you want to discuss or if you have any questions. Thanks,

Joe

From: Rouleau, Benjamin M - DOT [Benjamin.Rouleau@dot.wi.gov](mailto:Benjamin.Rouleau@dot.wi.gov)
Sent: Wednesday, April 11, 2018 4:26 PM

To: Urban, Joseph M. [Joseph.Urban@strand.com](mailto:Joseph.Urban@strand.com); Lipke, Bryan - DOT [Bryan.Lipke@dot.wi.gov](mailto:Bryan.Lipke@dot.wi.gov);
Michaelson, Jill - DOT < Jill.Michaelson@dot.wi.gov>
Cc: DOT WIS 23-Major 1440-13/15-00/01 [DOTWIS23-Major1440-13/15-00/01@dot.wi.gov](mailto:DOTWIS23-Major1440-13/15-00/01@dot.wi.gov); Lynch, Tom [Tom.Lynch@strand.com](mailto:Tom.Lynch@strand.com); Petersen, Joan [Joan.Petersen@strand.com](mailto:Joan.Petersen@strand.com); Kobryn, Jennifer <」ennifer.Kobryn@strand.com>; DOT Traffic Analysis \& Modeling
[DOTTrafficAnalysisModeling@dot.wi.gov](mailto:DOTTrafficAnalysisModeling@dot.wi.gov); Szymkowski, Rebecca - DOT
[Rebecca.Szymkowski@dot.wi.gov](mailto:Rebecca.Szymkowski@dot.wi.gov)
Subject: RE: WIS 23-2-Lane Operations Results (Draft 3-26-2018)

Joe and Bryan,

See attached. Overall, the files are looking good - but I do have a few questions and comments.

Also, I'm not sure if I've brought this up before, but with the volumes included for them, I would imagine that TWSC would be more than sufficient for control at the interchange ramp terminals.

Thanks,

Ben

## Benjamin M. Rouleau, E. I.

Traffic Operations and Analysis Engineer
Wisconsin Department of Transportation
Bureau of Traffic Operations

```
4 8 2 2 ~ M a d i s o n ~ Y a r d s ~ W a y , ~ 5 t h ~ F l o o r ~ S o u t h ~
Madison, WI 53705
Office: 608.266.7717
Cell: 802.272.8782
Email: benjamin.rouleau@dot.wi.gov
```

From: Urban, Joseph M. [mailto:Joseph.Urban@strand.com]
Sent: Tuesday, April 10, 2018 1:01 PM
To: Rouleau, Benjamin M - DOT [Benjamin.Rouleau@dot.wi.gov](mailto:Benjamin.Rouleau@dot.wi.gov); Lipke, Bryan - DOT
[Bryan.Lipke@dot.wi.gov](mailto:Bryan.Lipke@dot.wi.gov); Michaelson, Jill - DOT [Jill.Michaelson@dot.wi.gov](mailto:Jill.Michaelson@dot.wi.gov)
Cc: DOT WIS 23-Major 1440-13/15-00/01 <DOTWIS23-Major1440-13/15-00/01@ dot.wi.gov>; Lynch, Tom [Tom.Lynch@strand.com](mailto:Tom.Lynch@strand.com); Petersen, Joan < Joan.Petersen@strand.com>; Kobryn, Jennifer [Jennifer.kobryn@strand.com](mailto:Jennifer.kobryn@strand.com); DOT Traffic Analysis \& Modeling
[DOTTrafficAnalysisModeling@dot.wi.gov](mailto:DOTTrafficAnalysisModeling@dot.wi.gov); Szymkowski, Rebecca - DOT
[Rebecca.Szymkowski@dot.wi.gov](mailto:Rebecca.Szymkowski@dot.wi.gov)
Subject: RE: WIS 23-2-Lane Operations Results (Draft 3-26-2018)

Thanks Ben for the quick review on the two-lane mainline files. I've addressed the comment on Page 17 of the memo that you noted below.

Strand has completed updates to the four-lane highway and intersection analyses as well. Attached are the following files:

- An update to the " 01 " file from the previous emails with revisions to the 4 -lane volume development worksheet.
- "2018-04-10 WIS 23 Traffic Modeling Tech Memo (Draft with Attachments).pdf" - draft tech memo still with highlighted changes and attachments. The intersection analysis section and Attachment F have been revised since the previous version.
- Zip files that contain draft 4-lane highway and draft intersection HCS files based on the 4/6/2018 forecasts. The intersection analysis files include the following for the 2040 AM and PM peak hours:
- No-Build and Passing Lane Alternatives: two-way stop controlled analysis at 3 intersections.
- Hybrid and 4-Lane Alternatives: single-lane roundabout analysis at interchange ramp terminals (4 total intersections). RCUT, or J-Turn, analysis at 1 intersection.
- General intersection two-way stop controlled analysis with varying turning movement volumes for a two-lane and four-lane scenario.
- "2018-04-10 Draft Operations Analysis Results.zip" - contains a summary of the mainline MOEs and a summary of the intersection MOEs.

I believe your review in November covered most of the same files. The only modeling difference may be that the RCUT analysis/results for the County W/Loehr Road J-Turn are updated to reflect the guidance in the HCM6. Some other improvements were made to the presentation of the materials in Attachment F of the memo and the corresponding MOE tables to better align with how information may be presented in the environmental document.

Let me know if you have any questions during your review or if you need anything else. Thanks!
Joe

From: Rouleau, Benjamin M - DOT [Benjamin.Rouleau@dot.wi.gov](mailto:Benjamin.Rouleau@dot.wi.gov)
Sent: Monday, April 9, 2018 4:29 PM
To: Urban, Joseph M. [Joseph.Urban@strand.com](mailto:Joseph.Urban@strand.com); Lipke, Bryan - DOT [Bryan.Lipke@dot.wi.gov](mailto:Bryan.Lipke@dot.wi.gov);
Michaelson, Jill - DOT < Jill.Michaelson@dot.wi.gov>
Cc: DOT WIS 23-Major 1440-13/15-00/01 [DOTWIS23-Major1440-13/15-00/01@dot.wi.gov](mailto:DOTWIS23-Major1440-13/15-00/01@dot.wi.gov); Lynch, Tom [Tom.Lynch@strand.com](mailto:Tom.Lynch@strand.com); Petersen, Joan [Joan.Petersen@strand.com](mailto:Joan.Petersen@strand.com); Kobryn, Jennifer <」ennifer.Kobryn@strand.com>; DOT Traffic Analysis \& Modeling [DOTTrafficAnalysisModeling@dot.wi.gov](mailto:DOTTrafficAnalysisModeling@dot.wi.gov); Szymkowski, Rebecca - DOT
[Rebecca.Szymkowski@dot.wi.gov](mailto:Rebecca.Szymkowski@dot.wi.gov)
Subject: RE: WIS 23-2-Lane Operations Results (Draft 3-26-2018)
Joe, Bryan, and Jill,

See attached for the DT1887 form. I have reviewed the files and everything appears to be in order. The HCM equations appear to bounce around a bit with these small changes, but I have checked into it some and don't see any red flags.

I did note that, in the memo, item \#7 on page 17 ends with an incomplete sentence. It looks like this was also the case in the $3 / 26$ memo - sorry for having overlooked that previously.

Let me know when the other files are ready for review.

If there are any questions, just let me know.

Ben

Ben Rouleau
Traffic Operations and Analysis Engineer WisDOT Bureau of Traffic Operations
608.266.7717

From: Urban, Joseph M. [mailto:Joseph.Urban@strand.com]
Sent: Monday, April 09, 2018 10:19 AM
To: Rouleau, Benjamin M - DOT [Benjamin.Rouleau@dot.wi.gov](mailto:Benjamin.Rouleau@dot.wi.gov); DOT Traffic Analysis \& Modeling [DOTTrafficAnalysisModeling@dot.wi.gov](mailto:DOTTrafficAnalysisModeling@dot.wi.gov); Szymkowski, Rebecca - DOT
[Rebecca.Szymkowski@dot.wi.gov](mailto:Rebecca.Szymkowski@dot.wi.gov)
Cc: Lipke, Bryan - DOT [Bryan.Lipke@dot.wi.gov](mailto:Bryan.Lipke@dot.wi.gov); Michaelson, Jill - DOT
< ill.Michaelson@dot.wi.gov>; DOT WIS 23-Major 1440-13/15-00/01 [DOTWIS23-Major1440-13/1500/01@dot.wi.gov](mailto:DOTWIS23-Major1440-13/1500/01@dot.wi.gov); Lynch, Tom [Tom.Lynch@strand.com](mailto:Tom.Lynch@strand.com); Petersen, Joan [Joan.Petersen@strand.com](mailto:Joan.Petersen@strand.com); Kobryn, Jennifer < Jennifer.kobryn@strand.com>
Subject: RE: WIS 23-2-Lane Operations Results (Draft 3-26-2018)

Hi Ben,

Strand has completed updates to the WIS 23 two-lane mainline operations analysis based on the revised TDM-only forecasts from 4/6/2018. Please see below a description of the attached files, which are similar to the $3 / 26$ submittal.

- "01-Traffic Volumes - $\mathbf{2 0 1 8}$ April 6th Forecasts_App A" - Volume development sheets for each alternative.
- "02 - _Segment Forecasts (4-6-2018) - NERTDM only" - The NERTDM-only segment forecast reports extracted from Appendix A of the forecast document, provided by TFS to Strand on 4/6/2018.
- "03 - _Two-Lane Analysis Checklist 4-08-2018" - Revised two-lane mainline input checklist with the 4/6/2018 traffic volumes.
- "04a and 04b" Files - Draft operations results for the two-lane analysis. The "04a" file is a summary that shows the worst-case segment in each direction. The "04b" file shows a more detailed breakdown of the results from each individual HCS file.
- "05 - WIS $\mathbf{2 3}$ Two-Lane HCS Files (04-08-2018 Final Draft).zip" - The two-lane HCS files revised to reflect the latest traffic forecasts.
- "06-2018-04-09 WIS 23 Traffic Modeling Tech Memo (Draft changes).pdf" - Similar memo from your last review on $3 / 26$ that includes highlighted changes in comparison to the 11/9/2017 version of the memo. References to the traffic forecast date and the mainline

AADT/DHV volumes have been revised. See the email below regarding some detail on the check related to the version of HCS. For this analysis Version 7.5 was used.

The intersection and 4-lane operations modeling is in progress based on the AM and PM intersection forecasts received yesterday. I'd expect to be submitting the analysis files tomorrow for your review.

Let me know if you have any questions or if you need anything else. Thanks!

Joe

From: Urban, Joseph M.
Sent: Tuesday, April 3, 2018 10:31 AM
To: Lipke, Bryan - DOT [Bryan.Lipke@dot.wi.gov](mailto:Bryan.Lipke@dot.wi.gov); Michaelson, Jill - DOT
[jill.Michaelson@dot.wi.gov](mailto:jill.Michaelson@dot.wi.gov)
Cc: DOT WIS 23-Major 1440-13/15-00/01 [DOTWIS23-Major1440-13/15-00/01@dot.wi.gov](mailto:DOTWIS23-Major1440-13/15-00/01@dot.wi.gov); Lynch, Tom [Tom.Lynch@strand.com](mailto:Tom.Lynch@strand.com); Petersen, Joan [Joan.Petersen@strand.com](mailto:Joan.Petersen@strand.com); Kobryn, Jennifer [Jennifer.Kobryn@strand.com](mailto:Jennifer.Kobryn@strand.com)
Subject: RE: WIS 23-2-Lane Operations Results (Draft 3-26-2018)

Hi Bryan and Jill,

Strand has updated the two-lane operations analysis files to reflect the most recent version of HCS (version 7.5) that BTO used in their review. We've confirmed that there are no changes in operations compared to the previously submitted analysis files, which were completed in HCS version 7.3.

Attached are the HCS version 7.5 two-lane analysis files and revised checklist for your records. Let me know if you have any questions, otherwise these files could be passed on to BTO if needed to close out the two-lane peer review.

Thanks,

Joe

From: Rouleau, Benjamin M - DOT [Benjamin.Rouleau@dot.wi.gov](mailto:Benjamin.Rouleau@dot.wi.gov)
Sent: Tuesday, March 27, 2018 3:43 PM
To: Lipke, Bryan - DOT [Bryan.Lipke@dot.wi.gov](mailto:Bryan.Lipke@dot.wi.gov); DOT Traffic Analysis \& Modeling [DOTTrafficAnalysisModeling@dot.wi.gov](mailto:DOTTrafficAnalysisModeling@dot.wi.gov); Szymkowski, Rebecca - DOT
[Rebecca.Szymkowski@dot.wi.gov](mailto:Rebecca.Szymkowski@dot.wi.gov)
Cc: DOT WIS 23-Major 1440-13/15-00/01 [DOTWIS23-Major1440-13/15-00/01@dot.wi.gov](mailto:DOTWIS23-Major1440-13/15-00/01@dot.wi.gov); Lynch, Tom [Tom.Lynch@strand.com](mailto:Tom.Lynch@strand.com); Petersen, Joan [Joan.Petersen@strand.com](mailto:Joan.Petersen@strand.com); Kobryn, Jennifer [Jennifer.Kobryn@strand.com](mailto:Jennifer.Kobryn@strand.com); Urban, Joseph M. [Joseph.Urban@strand.com](mailto:Joseph.Urban@strand.com); Michaelson, Jill DOT < Jill.Michaelson@dot.wi.gov>
Subject: RE: WIS 23-2-Lane Operations Results (Draft 3-26-2018)

Bryan,

See attached for the DT1887. I didn't find any issues with the analysis. However, a couple things to note:

- Page 3 of the tech memo notes that the most recent version of HCS is 7.3 as of March 19, 2018. However, version 7.5 was released on $2 / 28 / 18$, I believe. This is the version that I used to review the model. I didn't come across any differences in results due to the different versions, but this should be updated.
- The "Two-Lane Analysis Checklist" file has Lu and Lde switched for Hybrid 2C: CTH G to CL EB. It is correct in Table 6 of the tech memo and, most importantly, in the HCS files. This error appears to have been present in previous iterations of this checklist table.

If you or Strand have any questions, please let me know.

Thanks,

Ben

## Benjamin M. Rouleau, E. I.

Traffic Operations and Analysis Engineer
Wisconsin Department of Transportation Bureau of Traffic Operations
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From: Lipke, Bryan - DOT
Sent: Monday, March 26, 2018 4:33 PM
To: DOT Traffic Analysis \& Modeling [DOTTrafficAnalysisModeling@dot.wi.gov](mailto:DOTTrafficAnalysisModeling@dot.wi.gov); Szymkowski, Rebecca - DOT [Rebecca.Szymkowski@dot.wi.gov](mailto:Rebecca.Szymkowski@dot.wi.gov); Rouleau, Benjamin M - DOT [Benjamin.Rouleau@dot.wi.gov](mailto:Benjamin.Rouleau@dot.wi.gov)
Cc: DOT WIS 23-Major 1440-13/15-00/01 [DOTWIS23-Major1440-13/15-00/01@dot.wi.gov](mailto:DOTWIS23-Major1440-13/15-00/01@dot.wi.gov); Lynch, Tom [Tom.Lynch@strand.com](mailto:Tom.Lynch@strand.com); Petersen, Joan [Joan.Petersen@strand.com](mailto:Joan.Petersen@strand.com); Kobryn, Jennifer < Jennifer.Kobryn@strand.com>; Urban, Joseph M. < Joseph.Urban@strand.com>; Michaelson, Jill DOT < Jill.Michaelson@dot.wi.gov>
Subject: FW: WIS 23-2-Lane Operations Results (Draft 3-26-2018)

Ben and Rebecca,

Transmitting Strands updated run of WIS 23 Traffic Operations based off the new traffic forecast information. Please keep me in the loop but work directly with Joe Urban if the questions or followup by phone or email can expedite BTO/Traffic Analysis Groups review. Again, this is the mainline only and we will reengage you for review of the side-road analysis soon when developed. Thank you for your review.

Bryan Lipke, P.E.

Planning Project Manager
Wisconsin Department of Transportation
Northeast Region
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Cell Phone: (920) 360-9196
Bryan.Lipke@dot.wi.gov
wisconsindot.gov
If this is related to a records request, please email: dotdtsdnerecords@dot.wi.gov

From: Urban, Joseph M. [mailto:Joseph.Urban@strand.com]
Sent: Monday, March 26, 2018 4:18 PM
To: Lipke, Bryan - DOT [Bryan.Lipke@dot.wi.gov](mailto:Bryan.Lipke@dot.wi.gov); Michaelson, Jill - DOT
< Jill.Michaelson@dot.wi.gov>
Cc: DOT WIS 23-Major 1440-13/15-00/01 [DOTWIS23-Major1440-13/15-00/01@dot.wi.gov](mailto:DOTWIS23-Major1440-13/15-00/01@dot.wi.gov); Lynch, Tom [Tom.Lynch@strand.com](mailto:Tom.Lynch@strand.com); Petersen, Joan [Joan.Petersen@strand.com](mailto:Joan.Petersen@strand.com); Kobryn, Jennifer [Jennifer.Kobryn@strand.com](mailto:Jennifer.Kobryn@strand.com)
Subject: [WARNING: ATTACHMENT(S) MAY CONTAIN MALWARE]WIS 23-2-Lane Operations Results (Draft 3-26-2018)

Hi Bryan and Jill,

Strand has completed updates to the 2-lane mainline operations analysis for WIS 23 based on the forecast documentation provided by WisDOT TFS on 3/19/2018. The volumes used in the operations analysis were from Appendix A of the forecasting document, which are based only on the Northeast Region Travel Demand Model (NERTDM). I've attached several files for WisDOT BTO's reference and review, a description of each is below.

- "01 - Traffic Volumes - 2018 Mar 19th Forecasts_App A" - Volume development sheets that are updated for the No-Build, Passing Lane, and Hybrid alternatives. The 4-Lane worksheet will be updated once intersection traffic forecasts are received because service ramp volumes are included in the 4-lane analyses.
- "02 - App A_Segment Forecasts (TDM only).pdf" - The NERTDM-only segment forecast reports extracted from Appendix A of the 3/19/2018 forecast document.
- "03 - __Two-Lane Analysis Checklist 3-23-2018" - Two-lane analysis input checklist provided for the first BTO review that has been updated for traffic volumes.
- "04a and 04b" Files - Draft operations results for the two-lane analysis. The "04a" file is a summary that shows the worst-case segment in each direction. The "04b" file shows a more detailed breakdown of the results from each individual HCS file.
- "05 - WIS 23 Two-Lane HCS Files (03-26-2018 Draft).zip" - The updated draft two-lane HCS files based on the NERTDM-only segment forecasts from 3/19/2018.
- "06-2018-03-26 WIS 23 Traffic Modeling Tech Memo (Draft changes).pdf" - Draft updates to the traffic modeling tech memo based on the 3/16/2018 WisDOT FDM updates and the $3 / 19 / 2018$ traffic forecasts. Changes from the 11/9/2017 version of the memo are highlighted or struck out at this time. Please note that the last page and attachments to the memo are a
work in progress and will be updated once the intersection traffic forecasts are received and the intersection/4-lane operations analysis is completed.

Let me know if you have any questions prior to the transmittal. Thanks!

Joe


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Excellence in Engineering Since 1946.

Wisconsin Department of Transportation (WisDOT)
DT1887 8/2015


Wisconsin Department of Tra

Traffic Volumes, \% Trucks,
Peak Hour Factor (PHF)Conditionally
Acceptable Yes

PHF = 1 and PHF = 0.89 scenarios both reviewed for future conditions
(continued on reverse side)

| SUMMARY OF REVIEW (continued) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Item Reviewed | Overall Model Acceptability | Revision Required | Reviewer Comment(s) | Analyst Response(s) |
| Signal Parameters (including RTOR) | $\square \square \square$ Acceptable $\square \square \square$ Unacceptable <br> $\square \square \square$ Conditionally $\square \square \boxtimes$ N/A <br> Acceptable  | $\boxtimes \square \square$ No $\square \square \square$ Yes |  |  |
| Stop-Control/Roundabout Parameters | $\square \square \square$ Acceptable $\square \square \square$ Unacceptable <br> $\square \square \square$ Conditionally $\square \square \square$ N/A <br> Acceptable  | $\square \square \square$ No $\square \square \square$ Yes |  |  |
| Freeway/Highway Parameters | $\square \square \square$ Acceptable $\square \square \square$ Unacceptable <br> $\square \square \square$ Conditionally $\square \square \square$ N/A <br> Acceptable $\square \square \square$ |  |  |  |
| Measures of Effectiveness (MOEs) | $\square \square \square$ Acceptable $\square \square \square$ Unacceptable <br> $\square \square \square$  <br> Conditionally <br> Acceptable $\square \square \square$ N/A | $\begin{aligned} & \boxed{\square \square} \text { No } \\ & \square \square \square \mathrm{Yes} \end{aligned}$ |  |  |
| Other: | $\square \square \square$ Acceptable $\quad \square \square \square$ Unacceptable $\square \square \square$ Conditionally Acceptable | $\square \square \square$ No $\square \square \square$ Yes |  |  |
| Overall Model | $\boxtimes \square \square$ Acceptable $\quad \square \square \square$ Unacceptable <br> $\square \square \square$Conditionally <br> Acceptable | $\boxtimes \square \square$ No $\square \square \square$ Yes |  |  |

Wisconsin Department of Transportation (WisDOT)
DT1887 8/2015

|  |  |  | Date Reviewed (m/d/yyyy) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \hline \text { Project ID(s) } \\ & 1440-13-00 \end{aligned}$ | Region: <br> NE |  |  | $\begin{gathered} \hline 1^{\text {st }} \text { Review } \\ 4 / 11 / 2018 \end{gathered}$ | $\begin{aligned} & 2^{\text {nd }} \text { Review } \\ & 4 / 12 / 2018 \end{aligned}$ | $3{ }^{\text {rd }}$ Review |
| Project Name/Description <br> WIS 23, Fond du Lac to Plymouth | Highway(s) <br> WIS 23 |  | Reviewed By: WisDOT BTO |  |  |  |
| Name (First, MI, Last) Ben Rouleau |  | Name (First, MI, Last) Joe Urban |  | Name (First, MI, Last) Bryan Lipke |  |  |
| Organization/Firm WisDOT BTO |  | Organization/Firm <br> Strand Associates <br> (Area Code) Telephone Number (608) 251-4843) |  | Region/Bureau NE Region |  |  |
|  |  |  |  | (Area Code) Telephone Number (920) 492-5703 |  |  |
| Email Address benjamin.rouleau@dot.wi.gov |  | Email Address joseph.urban@strand.com |  | Email Address bryan.lipke@dot.wi.gov |  |  |
| TRAFFIC MODEL DESCRIPTION |  |  |  |  |  |  |
| Model Completion/Revision Date (m/d/yyyy) 4/11/2018 |  | $\begin{aligned} & \text { Analysis Year(s) } \\ & 2040 \end{aligned}$ | Analysis Scenario/Alternative Build |  |  |  |

Scope of Model (intersections, ramps, corridors, etc. being reviewed)
$>$
ó
ór
Scope Model (intersections, ramps, corridors,
家 WIS 23 from County UU (Fond du Lac) to County P (Sheboygan); CTH G WB merge, CTH G EB diverge, CTH UU WB merge, CTH UU EB diverge, east of CTH UU basic, east of CTH $G$ basic



The excel spreadsheet has been updated to address the difference in terrain. The rolling terrain occurs further east of the proposed CTH G interchange so a "level" analysis is probably appropriate here. No changes to HCS files are proposed, please confirm.
For truck percentages, the data has been broken down in weighted averages to be $17 \%$ from CTH UU to CTH G and 13\% from CTH G to CTH P. The more conservative $17 \%$ value of the two weighted average truck percentages is used in this analysis. No changes are proposed, please confirm.
(continued on reverse side)

| SUMMARY OF REVIEW (continued) |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Item Reviewed | Overall Model Acceptability | Revision <br> Required | Reviewer Comment(s) |

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Page 3 of 3

Wisconsin Department of Transportation (WisDOT)
DT1887 8/2015

(continued on reverse side)

| SUMMARY OF REVIEW (continued) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Item Reviewed | Overall Model Acceptability | Revision Required | Reviewer Comment(s) | Analyst Response(s) |
| Signal Parameters (including RTOR) | $\square \square \square$ Acceptable $\square \square \square$ Unacceptable <br> $\square \square \square$ Conditionally <br> Acceptable $\square \square \square$ N/A | $\begin{aligned} & \boxed{\nabla \square \square \text { No }} \\ & \square \square \square \text { Yes } \end{aligned}$ |  |  |
| Stop-Control/Roundabout Parameters | $\square \boxtimes \square$ Acceptable $\quad \square \square \square$ Unacceptable$\boxtimes \square \square$Conditionally <br> Acceptable$\square \square \square$ N/A | $\square \boxtimes \square$ No $\square \square \square \mathrm{Yes}$ | The base critical headway for the $J$-turn analyses is set to 4.3. Even though this value isn't used, it should be 4.4 (HCM6, 23-77). The changes are acceptable. | The base critical headway settings have been revised to 4.4 seconds for the U-turn movements at the crossover intersections. Strand confirmed that the control delay results remain the same. |
| Freeway/Highway Parameters |  | $\begin{aligned} & \boxtimes \boxtimes \square \text { No } \\ & \square \square \square \text { Yes } \end{aligned}$ | To confirm - the mainline through the J-turn will be posted at 65 MPH? This is set as the "Major Street Free-Flow Speed". <br> The changes are acceptable. | In the 4-Lane Alternative the mainline would be posted at 65 mph (with a freeflow speed of 70 mph ) and in the Hybrid Alternative the mainline would be posted at 55 mph (with a freeflow speed of 60 mph ). These posted speeds were confirmed by WisDOT NE Region staff on 3/28/2018. <br> - Upon further review, the Hybrid Alternative J-Turn analysis has been updated with the 60 mph free-flow speed (was previously set at 65 mph ). Results have been updated. <br> - With the 4-Lane Alternative, HCS does not allow a speed of 70 mph to be entered (software caps the speed at 65 mph ). The HCS output could be post-processed to represent 70 mph , but the difference in travel time between the primary intersection and U-turns should be minimal. No changes to 4-Lane output based on 70 mph freeflow speed is proposed, please confirm. |
|  | $\square \square \square$ Acceptable $\quad \square \square \square$ Unacceptable | $\boxtimes \boxtimes \square$ No |  |  |

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| Measures of Effectiveness (MOEs) |  | $\square \square \square \mathrm{Yes}$ | For the J-turn analyses, recommend presenting results by movement. <br> The changes are acceptable. | Results have been updated to show individual movements for the NBR + EB Uturn and the SBR + WB U-turn, along with the NB and SB approaches. The mainline left-turn movements are shown in the tables above. Please see revised MOE table provided with this review. |
| :---: | :---: | :---: | :---: | :---: |
| Other: | $\square \square \square$ Acceptable $\quad \square \square \square$ Unacceptable $\square \square \square$ Conditionally Acceptable | $\square \square \square$ No $\square \square \square$ Yes |  |  |
| Overall Model | $\square \boxtimes \square$ Acceptable $\quad \square \square \square$ Unacceptable $\boxtimes \square \square$ Conditionally Acceptable |  | Some things to check into on the J -Turn analyses. Otherwise, looking good. <br> The intersection models are acceptable. | JMU 4-12-2018: A few revisions have been made per the responses above. |

WIS 23 Highway Capacity Software Mainline Analysis
April 9, 2018

|  |  | County UU to County G |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2-Lane No Build |  | Passing Lane Alternatives |  |  |  |  |  | 4-Lane On-Alignment |  |
|  |  | Passing Lanes Without Left Turn Lanes | Passing Lanes With Left Turn Lanes |  | Hybrid |  |  |  |
|  |  | Eastbound | Westbound | Eastbound | Westbound | Eastbound | Westbound | Eastbound* ${ }^{\text {* }}$ | Westbound* | Eastbound* | Westbound* |
|  | HCS Average Speed (mph) 2017 |  |  | 47.8 | 47.7 | -- | -- | -- | -- | -- | -- | -- | -- |
|  | \% Following 2017 | 67.5\% | 67.7\% | -- | -- | -- | -- | -- | -- | -- | -- |
|  | LOS 2017 (Numeric) | 4.17 | 4.18 | -- | -- | -- | -- | -- | -- | -- | -- |
|  | LOS 2017 | D | D | -- | -- | -- | -- | -- | -- | -- | -- |
|  | HCS Average Speed (mph) 2040 | 48.0 | 47.9 | 48.8 | 48.8 | 48.4 | 48.4 | 60.0 | 60.0 | 70.0 | 70.0 |
| \% \% | \% Following 2040 | 66.3\% | 66.6\% | 53.1\% | 52.8\% | 54.8\% | 54.3\% | -- | -- | -- | -- |
|  | LOS 2040 (Numeric) | 4.09 | 4.11 | 3.21 | 3.19 | 3.32 | 3.29 | -- | -- | -- | -- |
|  | LOS 2040 | D | D | C | C | C | C | A | A | A | A |
|  | $\begin{array}{\|r\|} \hline \hline \text { Year LOS passes from C to D } \\ \text { First Year C to D (either direction) } \end{array}$ | 2017 | 2017 | 2060+ | 2060+ | 2060+ | 2060+ | -- | -- | -- | -- |
|  |  | 2017 |  | 2060+ |  | 2060+ |  | -- |  | -- |  |




|  | HCS Average Speed (mph) 2040 <br> \% Following 2040 <br> LOS 2040 (Numeric) LOS 2040 | 48.3 | 48.7 | 48.4 | 49.5 | 47.9 | 49.0 | 47.4 | 48.9 | 70.0 | 70.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 64.7\% | 66.4\% | 63.7\% | 54.0\% | 65.8\% | 55.9\% | 67.6\% | 58.9\% | -- | -- |
|  |  | 3.98 | 4.09 | 3.91 | 3.27 | 4.05 | 3.39 | 4.17 | 3.59 | -- | -- |
|  |  | C | D | C | C | D | C | D | C | A | A |
| Year LOS passes from C to D First Year C to D (either direction) |  | 2054 | 2017 | 2060+ | 2060+ | 2025 | 2060+ | 2020 | $2060+$ | -- | -- |
|  |  | 2017 |  | 2060+ |  | 2025 |  | 2020 |  | -- |  |

Alpha and Numeric Level of Service (LOS) Scale

| LOS | A | B | C | D | E | F |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% Following | $\leq 35 \%$ | $35-50 \%$ | $50-65 \%$ | $65-80 \%$ | $>80 \%$ | volume $/$ capacity $>1.0$ |
| Numeric LOS | $1.01-2.00$ | $2.01-3.00$ | $3.01-4.00$ | $4.01-5.00$ | $5.01-6.00$ | ( |
| Average Travel Speed (mph) | $>55$ | $>50-55$ | $>45-50$ | $>40-45$ | $\leq 40$ | volume/capacity $>1.0$ |


*4-Lane Freeway Analysis

*4-Lane Freeway Analysis

## Notes:

\# Description:
1 Observed speeds are based on National Performance Management Research Data Set (NPMRDS) data from June 27-29, 2017 (3 weekdays), coinciding with the week of traffic volume counts for the study 2 Highway Capacity Software (HCS) results are based on WisDOT traffic forecasts completed on April 6, 2018 (Appendix A) using HCS Version 7.
3 see "DHV for WIS 23 Evaluation" memo and "Traffic Modeling Methodology" memo for more information on HCS analysis inputs and assumptions.
4 4-Lane section freeflow speed assumed to be 5 mph above expected posted speeds. Modeling confirms no reduction in freeflow speed for 4 -lane sections.
5 Adjusted travel speeds for the 2 -lane sections of the 2040 No-Build and Build Alternatives are developed by using the relative difference predicted by HCS and applying it to the 2017 observed speed data. For
example, if a segment's 2040 alternative travel speed is predicted to be 1 mph faster than the segment's 2017 existing condition travel speed in HCS , the segment's adjusted travel speed for the 2040 alternative $=$ 58 mph (Observed Speed) +1 mph (Difference Predicted by HCS) $=59 \mathrm{mph}$ (Adjusted Travel Speed). See Page 2 for all HCS difference calculations.

| Travel Time Differences (s) County UU to County G |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Eastbound (Flat Peak Hour Pattern) |  |  |  |  |  |
| 2017 | No-Build | PLnoL | PLwL | Hybrid | 4-Lane |
| 608 | 606 | 598 | 602 | 588 | 504 |
| Diff vs 2017 | -2 | -10 | -6 | -20 | -104 |
| Diff vs 2040 | No-Build | -8 | -4 | -18 | -102 |
| Westbound (Flat Peak Hour Pattern) |  |  |  |  |  |
| 2017 | No-Build | PLnoL | PLwL | Hybrid | 4-Lane |
| 608 | 606 | 597 | 601 | 588 | 504 |
| Diff vs 2017 | -2 | -11 | -7 | -20 | -104 |
| Diff vs 2040 | No-Build | -9 | -5 | -18 | -102 |

## Travel Time Differences (s)

County G to County P
Eastbound (Flat Peak Hour Pattern)
Eastbound (Flat Peak Hour Pattern)

| 2017 | No-Build | PL no L | PL w L | Hybrid | 4 -Lane |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 497 | 493 | 492 | 497 | 500 | 411 |
| Diff vs 2017 | -3 | -4 | 0 | 3 | -85 |
|  | Diff vs 2040 | No-Build | -1 | 3 | 7 |


| 2017 | No-Build | PL noL | PLwL | Hybrid | 4-La |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 497 | 493 | 486 | 491 | 491 | 411 |
| Diff vs 2017 | -3 | -11 | -6 | -5 | -85 |
| Diff vs 2040 | No-Build | -7 | -3 | -2 | -82 |

Travel Time Summary (s) vs. 2040 No-Build


|  | County UU to County G |  |  |  |  |  |  |  |  |  | Notes and Assumptions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Passing Lane Alternatives |  |  |  |  |  |  |  | 4-Lane On-Alignment |  |  |
|  | 2-Lane No Build |  | Passing Lanes Without Left Turn Lanes |  | Passing Lanes With Left Turn Lanes |  | Hybrid |  |  |  |  |
|  | Eastbound | Westbound | Eastbound | Westbound | Eastbound | Westbound | Eastbound* | Westbound* | Eastbound* | Westbound* |  |
| HCS Average Speed (mph) 2017 | 47.8 | 47.7 | -- | -- | -- | -- | -- | -- | -- | -- | Modeled 2017 existing conditions HCS travel speed |
| Observed Travel Speed (mph) 2017 | 58.0 | 58.0 | -- | -- | -- | -- | -- | -- | -- | -- |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| HCS Average Speed (mph) 2040 | 48.0 | 47.9 | 48.8 | 48.8 | 48.4 | 48.4 | 60.0 | 60.0 | 70.0 | 70.0 | Modeled 2040 HCS travel speed |
| HCS DIFFERENCE (2040-2017) | 0.2 | 0.2 | 1.0 | 1.1 | 0.6 | 0.7 | -- | -- | -- | -- | Difference between 2040 HCS travel speed and 2017 HCS travel speed |
| Adjusted Travel Speed (mph) 2040 | 58.2 | 58.2 | 59.0 | 59.1 | 58.6 | 58.7 | 60.0 | 60.0 | 70.0 | 70.0 |  |



Notes:
\# Description:
1 Observed speeds are based on National Performance Management Research Data Set (NPMRDS) data from June 27-29, 2017 ( 3 weekdays), coinciding with the week of traffic volume counts for the study.
2 Highway Capacity Software (HCS) results are based on WisDOT traffic forecasts completed on April 6, 2018 (Appendix A) using HCS Version 7.
3 See "DHV for WIS 23 Evaluation" memo and "Traffic Modeling Methodology" memo for more information on HCS analysis inputs and assumptions.
4 4-Lane section freeflow speed assumed to be 5 mph above expected posted speeds. Modeling confirms no reduction in freeflow speed for 4 -lane sections.
5 Adjusted travel speeds for the 2 -lane sections of the 2040 No-Build and Build Alternatives are developed by using the relative difference predicted by HCS and applying it to the 2017 observed speed data. For example, if a segment's 2040 alternative travel speed is predicted to be 1 mph faster than the segment's 2017 existing condition travel speed in HCS, the segment's adjusted travel speed for the 2040 alternative $=58 \mathrm{mph}$ (Observed Speed) +1 mph (Difference Predicted by HCS) $=59 \mathrm{mph}$ (Adjusted Travel Speed).

WIS 23 Intersection Operations: No-Build and Passing Lane Alternatives
April 12, 2018
Page 1 of 2

| No Build Side Street LOS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | 2040 AM PEAK |  |  |  |  |  |  |  | 2040 PM PEAK |  |  |  |  |  |  |  |
|  | NBL/TH |  | NBR |  | SBL/TH |  | SBR |  | NBL/TH |  | NBR |  | SBL/TH |  | SBR |  |
|  | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS |
| County UU | 24.5 | C | 10.4 | B | 22.1 | C | 12.4 | B | 39.1 | E | 12.7 | B | 27.9 | D | 11.6 | B |
| County W/Loehr | 16.7 | C | 10.1 | B | 17.2 | C | 10.7 | B | 20.5 | C | 10.9 | B | 21.3 | C | 10.8 | B |
| County G | 17.6 | C | 10.4 | B | 16.9 | C | 10.3 | B | 22.0 | C | 10.6 | B | 20.6 | C | 10.5 | B |


| Passing Lane Alternative without Left-Turn Lanes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | 2040 AM PEAK |  |  |  |  |  |  |  | 2040 PM PEAK |  |  |  |  |  |  |  |
|  | NBL/TH |  | NBR |  | SBL/TH |  | SBR |  | NBL/TH |  | NBR |  | SBL/TH |  | SBR |  |
|  | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS |
| County UU | 25.4 | D | 10.4 | B | 22.7 | C | 12.6 | B | 41.8 | E | 12.8 | B | 29.0 | D | 11.7 | B |
| County W/Loehr | 17.0 | C | 10.1 | B | 17.7 | C | 10.7 | B | 21.1 | C | 11.0 | B | 22.1 | C | 10.9 | B |
| County G | 18.1 | C | 10.5 | B | 17.3 | C | 10.4 | B | 22.9 | C | 10.7 | B | 21.3 | C | 10.6 | B |


| Passing Lane Alternative with Left-Turn Lanes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | 2040 AM PEAK |  |  |  |  |  |  |  | 2040 PM PEAK |  |  |  |  |  |  |  |
|  | NBL/TH |  | NBR |  | SBL/TH |  | SBR |  | NBL/TH |  | NBR |  | SBL/TH |  | SBR |  |
|  | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS |
| County UU | 17.3 | C | 10.4 | B | 16.0 | C | 12.6 | B | 21.2 | C | 12.8 | B | 18.5 | C | 11.7 | B |
| County W/Loehr | 13.8 | B | 10.1 | B | 14.1 | B | 10.7 | B | 16.0 | C | 11.0 | B | 15.9 | C | 10.9 | B |
| County G | 14.5 | B | 10.5 | B | 14.1 | B | 10.4 | B | 16.4 | C | 10.7 | B | 15.8 | C | 10.6 | B |

NBL = Northbound Left, NBR = Northbound Right
SBL = Southbound Left, SBR = Southbound Right
TH = Through, LOS = Level of Service
Notes: No-Build operations are based on April 6, 2018 traffic forecasts (App. A of traffic forecasting memo, NERTDM only). Passing Lane operations are based on volumes factored up from No-Build forecast. See Traffic Modeling Methodology Memo attachments for more detail on the inputs used for the intersection operations analysis.

| Intersection | Alternative | Hybrid and 4-Lane Alternatives: County UU |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2040 AM PEAK |  |  |  |  |  |  |  | 2040 PM PEAK |  |  |  |  |  |  |  |
|  |  | EB Approach |  | WB Approach |  | NB Approach |  | SB Approach |  | EB Approach |  | WB Approach |  | NB Approach |  | SB Approach |  |
|  |  | Delay (s) | LOS | Delay (s) | Los | Delay (s) | Los | Delay (s) | LOS | Delay (s) | Los | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS |
| County UU WB | Hybrid | --- | --- | 3.2 | A | 3.4 | A | 3.2 | A | --- | --- | 3.5 | A | 4.1 | A | 3.8 | A |
| Roundabout | 4-Lane | --- | --- | 3.2 | A | 3.4 | A | 3.3 | A | --- | --- | 3.5 | A | 4.1 | A | 3.9 | A |
| County UU EB | Hybrid | 3.5 | A | -- | --- | 3.4 | A | 3.1 | A | 3.4 | A | --- | --- | 4.2 | A | 3.7 | A |
| Roundabout | 4-Lane | 3.5 | A | --- | --- | 3.4 | A | 3.1 | A | 3.4 | A | --- | --- | 4.3 | A | 3.8 | A |


| Intersection | Alternative | Hybrid and 4-Lane Alternatives: County G |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2040 AM PEAK |  |  |  |  |  |  |  | 2040 PM PEAK |  |  |  |  |  |  |  |
|  |  | EB Approach |  | WB Approach |  | NB Approach |  | SB Approach |  | EB Approach |  | WB Approach |  | NB Approach |  | SB Approach |  |
|  |  | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | Los | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS |
| County G WB | Hybrid | --- | --- | 3.5 | A | 3.7 | A | 3.4 | A | --- | --- | 3.5 | A | 3.8 | A | 3.6 | A |
| Roundabout | 4-Lane | --- | --- | 3.5 | A | 3.7 | A | 3.5 | A | --- | --- | 3.5 | A | 3.9 | A | 3.7 | A |
| County G EB | Hybrid | 3.7 | A | --- | --- | 3.6 | A | 3.1 | A | 3.7 | A | --- | --- | 3.8 | A | 3.4 | A |
| Roundabout | 4-Lane | 3.7 | A | --- | --- | 3.7 | A | 3.2 | A | 3.8 | A | --- | --- | 3.9 | A | 3.5 | A |


| Intersection | Alternative | Hybrid and 4-Lane Alternatives: County W/Loehr Road J-Turn (Primary Intersection Control Delay) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2040 AM PEAK |  |  |  |  |  |  |  | 2040 PM PEAK |  |  |  |  |  |  |  |
|  |  | EBL |  | WBL |  | NBR |  | SBR |  | EBL |  | WBL |  | NBR |  | SBR |  |
|  |  | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS |
| County W/Loehr | Hybrid | 8.8 | A | 0.0 | A | 9.8 | A | 10.4 | B | 8.9 | A | 0.0 | A | 10.1 | B | 10.6 | B |
| Intersection | 4-Lane | 9.0 | A | 0.0 | A | 10.0 | A | 10.7 | B | 9.2 | A | 0.0 | A | 10.3 | B | 11.0 | B |


| Intersection | Alternative | Hybrid and 4-Lane Alternatives: County W/Loehr Road J-Turn (Crossover Intersection Control Delay) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2040 AM PEAK |  |  |  |  |  |  |  | 2040 PM PEAK |  |  |  |  |  |  |  |
|  |  | EBT |  | WB to EB U-turn |  | WBT |  | EB to WB U-turn |  | EBT |  | WB to EB U-turn |  | WBT |  | EB to WB U-turn |  |
|  |  | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS | Delay (s) | LOS |
| County W/Loehr West Crossover | Hybrid | 0.0 | A | 9.5 | A | --- | --- | --- | --- | 0.0 | A | 10.4 | B | --- | --- | --- | --- |
|  | 4-Lane | 0.0 | A | 9.7 | A | --- | --- | --- | --- | 0.0 | A | 10.8 | B | --- | --- | --- | --- |
| County W/Loehr East Crossover | Hybrid | --- | --- | --- | --- | 0.0 | A | 9.2 | A | --- | --- | --- | --- | 0.0 | A | 9.9 | A |
|  | 4-Lane | --- | --- | --- | --- | 0.0 | A | 9.4 | A | --- | --- | --- | --- | 0.0 | A | 10.2 | B |


| Intersection | Alternative | Hybrid and 4-Lane Alternatives: County W/Loehr Road J-Turn (HCM6 Alternative Intersection Analysis Results) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2040 AM PEAK |  |  |  |  |  |  |  | 2040 PM PEAK |  |  |  |  |  |  |  |
|  |  | NBR + EB U-turn |  | SBR + WB U-turn |  | NB Approach |  | SB Approach |  | NBR + EB U-turn |  | SBR + WB U-turn |  | NB Approach |  | SB Approach |  |
|  |  | ETT (s) | LOS | ETT (s) | LOS | ETT (s) | LOS | ETT (s) | LOS | ETT (s) | LOS | ETT (s) | LOS | ETT (s) | LOS | ETT (s) | LOS |
| County W/Loehr | Hybrid | 45.1 | D | 49.4 | D | 36.0 | D | 20.9 | c | 46.1 | D | 50.5 | D | 36.8 | D | 23.5 | c |
| Intersection | 4-Lane | 43.5 | D | 47.7 | D | 34.6 | c | 20.6 | c | 44.7 | D | 49.0 | D | 35.9 | D | 23.1 | c |

[^6]Notes: 4-Lane Alternative operations are based on April 6,2018 traffic forecasts (App. A of traffic forecasting memo, NERTDM only). Hybrid Alternative operations are based on volumes
factored down from 4-Lane Alternative forecast. The LOS scale for Alternative Intersections is different from unsignalized intersections and is based on Exhbibit 23 -13 of the HCM6. See Traffic Modeling Methodology Memo attachments for more detail on the inputs used for the intersection operations analysis.


[^0]:    ${ }^{1} 2010$ OMB Bulletin No 10-02
    TWL:plh $\backslash \mathrm{S}: \backslash$ MAD $\backslash 1000$--1099 $1089 \backslash 817 \backslash$ Wrd $\backslash$ Memos and Reports $\backslash$ DHV Memo\2018-05-11 Final WIS 23 DHV Tech Memo.docx $\backslash 051218$

[^1]:    ${ }^{2}$ Data was not available for these 2016 dates: $3 / 13,4 / 5,4 / 6,5 / 27,6 / 11-6 / 24,9 / 30,9 / 31,10 / 1,11 / 6-2016$ was a leap year.
    ${ }^{3}$ Data was not available for these 2016 dates: $1 / 1,4 / 6,6 / 7,9 / 1,12 / 7-2016$ was a leap year.
    TWL:plh $\backslash \mathrm{S}:$ IMAD $\backslash 1000$--1099 $1089 \backslash 817 \backslash$ Wrd 4 Memos and Reports $\$ DHV Memol2018-05-11 Final WIS 23 DHV Tech Memo.docx 1051218

[^2]:    ${ }^{4}$ FDM 11-5-3.7.1.1: http://wisconsindot.gov/Pages/doing-bus/eng-consultants/cnslt-rsrces/rdwy/fdm.aspx, accessed March 26, 2018
    ${ }^{5}$ Highway Capacity Manual (Transportation Research board, 6th Edition, 2016)
    

[^3]:    ${ }^{1}$ FDM source: http://wisconsindot.gov/Pages/doing-bus/eng-consultants/cnslt-rsrces/rdwy/fdm.aspx, accessed March 26, 2018
    ${ }^{2}$ Highway Capacity Manual (Transportation Research board, 6th Edition, 2016)
    TWL:plh $\backslash \mathrm{S}: \backslash \mathrm{MAD} \backslash 1000--1099 \backslash 1089 \backslash 817 \backslash \mathrm{Wrd} \backslash$ Memos and Reports $\backslash H C S$ Modeling Methodology 12018 -05-11 WIS 23 Traffic Modeling Tech Memo (Final).docx 0051218

[^4]:    ${ }^{3} 2010$ OMB Bulletin No 10-02
    TWL:plh\S:\MAD $\backslash 1000-1099 \backslash 1089 \backslash 817 \backslash$ Wrd $\backslash$ Memos and Reports\HCS Modeling Methodology\2018-05-11 WIS 23 Traffic Modeling Tech Memo (Final).docx 1051218

[^5]:    ${ }^{4}$ For the No-Build Alternative between County UU and County G, the net change in 3 less access points along the corridor results in one less access point per mile. There is no change in access points per mile between County G and County P. Testing performed in HCS with the 2040 No-Build Alternative between County UU and County G showed no change in numeric LOS along the corridor with the slightly lower access point density value.

[^6]:    LOS $=$ Level of Service, ETT $=$ Experienced Travel Time, EB $=$ Eastbound, WB $=$ Westbound, $\mathrm{NB}=$ Northbound, SB $=$ Southbound

