## Project and Analyst Information:

| Project ID: | 6180-30-00 |
| ---: | :--- |
| Project Type: | State Highway |
| Location: | STH 21 and Sand |
|  | Town of Omro |
|  | Winnebago |
|  | NE Region |
| Analyst: | Camie Ferrier |
| Agency: | Westwood Infr |
| Date: | March 31, 202 |
| ackground Information: |  |


| Project Need: | Safety |
| ---: | :--- |
| Project <br> Objective(s): | The project objective is to improve the safety at the intersection of STH 21 and Sand Pit Road. |
| Additional | The intersection of STH 21 and Sand Pit Road is included in a resurfacing project of STH 21, which <br> Information: <br> begins south of Structure B-70-0051 within the City of Omro and continues to approximately Leonard <br> Point Road. |
| The existing form of traffic control is a minor road stop on Sand Pit Road while STH 21 has free flow <br> traffic. The intersection geometry involves EB and WB both having a designated right turn lane while <br> the left turn and through movements share a lane. NB and SB both have a single lane approach. The <br> speed limit is 55 mph on STH 21 and 45 mph on Sand Pit Road. |  |

## Existing Crash Information:

## Observed Crash History:

Years: 2015-2019

| Crash Type | Fatal | Injury A | Injury B | Injury C | KABC | PDO | Total |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sideswipe |  |  |  | 1 | 1 | 1 | 2 |
| STH 21 Left Turn |  |  |  | 1 | 1 |  | 1 |
| Run off Road |  |  | 1 |  | 1 |  | 1 |
| STH 21 Rear End <br> while turning left |  |  | 4 | 3 | 7 | 2 | 9 |
| Total | 0 | 0 | 5 | 5 | 10 | 3 | 13 |

Injury A - Suspected Serious Injury
Injury B - Suspected Minor Injury
Injury C - Possible Injury
KABC - Fatal (K) and Injury A, B and C
PDO - Property Damage Only

## Crash Trends:

Left turning vehicles on STH 21 appear to be a factor in 13 of the 15 crashes. STH 21 through traffic rear ends traffic that is planning to turn left and left turning traffic from STH 21 fails to yield to oncoming traffic.

Contributing Factors:
Currently, left turn lanes do not exist on STH 21. Another factor may be difficulty selecting adequate gaps when crossing or turning left.

## Additional Modes of Transportation:

| Mode | Need? <br> Yes/No | Nearby Generators and Existing Facilities | Volume |  |
| :--- | :--- | :--- | :--- | :--- |
|  |  | \# |  | Unit |
| PED/BIKE | Yes | None | N/A |  |
| OSOW | Yes | None |  | vph |

(add more rows as needed)
Other Information: STH 21 in the area of this project is recommended to be part of the Oshkosh MPO Regional Bicycle \& Pedestrian Network as shown in the Appleton (Fox Cities) Transportation Management Area \& Oshkosh Metropolitan Planning Organization Bicycle and Pedestrian Plan - 2014.

STH 21 is an OSOW truck route and High Clearance Route. Minimum 20 foot vertical clearance required for new vertical elements such as sign structures, sign bridges, signals and lighting.

## Summary Tables:

## Descriptions:

| Alt. | Traffic Control | Description of Alternative |
| :---: | :--- | :--- |
| 1 | Minor Road Stop Control with <br> Slotted Left turns on Major Road | Maintain two-way stop control, with Sand Pit Road being stop controlled. <br> Install dedicated left turn lanes on STH 21. |
| 2 | Roundabout | Install a roundabout at the intersection of STH 21 and Sand Pit Road. |

Costs and Impacts:

| Alt. | Traffic Control | Construction <br> Cost | Real Estate Impacts |  |  | Environmental Impacts |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | \# Build | \# Acres | Cost | Impact Type | \# Acres |
|  | Minor Road Stop <br> Control with <br> Slotted Left turns <br> on Major Road |  | N/A | 0.07 | $\$ 1,400$ | Wetland | 0 |
| 2 | Roundabout | $\$ 2,000,000$ | N/A | 0.731 | $\$ 34,000$ | Wetland | 0 |

Safety Performance:

| Alt. | Traffic Control | Analysis Period | KABC | PDO | Total |
| :---: | :--- | :---: | :---: | :---: | :---: |
| - | Existing Conditions | $2014-2019$ | 11 | 4 | 15 |
| - | Future No-Build | $2027-2036$ | 4.918 | 11.153 | 16.071 |
| 1 | Minor Road Stop Control with <br> Slotted Left turns on Major Road | $2027-2036$ | 2.557 | 5.800 | 8.357 |
| 2 | Roundabout | $2027-2036$ | 2.965 | 18.645 | 21.610 |

Safety performance results are from the Safety Certification Document, dated 8-6-2020, signed 9-14-2020. Analysis method: Interactive Highway Safety Design Model

Recommendation:
Alternative:
Influencing
Factors:

## Existing \& Future No-Build Conditions:

Practical Feasibility:

| Public Opinion: | Concerns with safety have been expressed by local officials. A public involvement meeting is <br> scheduled to occur in 2021. |
| ---: | :--- |
| Business Impacts: | None |
| ROW Impacts: | None |
| Utility Impacts: | None |
| Cost Estimate: | \$0 |
| Additional Info: | None |

Safety Analysis:
Left turning vehicles on STH 21 appear to be a factor in 13 of the 15 crashes. STH 21 through traffic rear ends traffic that is planning to turn left and left turning traffic from STH 21 fails to yield to oncoming traffic.

Currently, left turn lanes do not exist on STH 21. Another factor may be difficulty selecting adequate gaps when crossing or turning left.

| Conflict Points: | EB and WB left turns conflicting with opposing through traffic. <br> NB and SB left turns conflicting with EB and WB traffic. |
| ---: | :--- |
| Vulnerable Users: | N/A |
| Additional Info: | N/A |

## Safety Performance Measures:

|  | Analysis Period | KABC | PDO | Total |
| :--- | :---: | :---: | :---: | :---: |
| Existing Conditions | $2014-2019$ | 11 | 4 | 15 |
| Future No-Build | $2027-2036$ | 4.918 | 11.153 | 16.071 |

## Operational Analysis:

Utilizing traffic counts from October 21, 2019, traffic signal warrants were evaluated for the intersection of STH 21 and Sand pit Road. The signal warrant analysis showed that traffic signals were not warranted at the intersection, therefore a traffic signal alternative was eliminated from consideration.
There are field entrances located on the north leg of Sand Pit Road at approximately 170' north of the intersection. The southbound queue of $165^{\prime}$ in 2047 approaches the first field entrance. There is a commercial driveway on the south leg of Sand Pit Road at approximately 185 ' south of the intersection. The northbound queue does not impact this driveway.

| Additional Capacity: | None |
| ---: | :--- |
| Railroad Impacts: | None |
| Additional Info: | In 2047, the southbound leg experiences a LOS of $F$ in the am and pm peak hours and the <br> northbound leg experiences a LOS of E in the pm peak hour. |

Operational Performance Measures:

| Year: 2027 | Existing Conditions |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L/T | - | R | L/T | - | R | - | All | - | - | All | - |
| \# Lanes | 1 |  | 1 | 1 |  | 1 |  | 1 |  |  | 1 |  |
| LOS | A |  |  | A |  |  |  | C |  |  | E |  |
| Delay (s) | 7.9 |  |  | 8.8 |  |  |  | 20.2 |  |  | 37.8 |  |
| v/c | 0.00 |  |  | 0.01 |  |  |  | 0.10 |  |  | 0.60 |  |
| Queue (ft.) | 0 |  |  | 0 |  |  |  | 7.5 |  |  | 87.5 |  |
| Storage (ft.) |  |  |  |  |  |  |  |  |  |  |  |  |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L/T | - | R | L/T | - | R | - | All | - | - | All | - |
| \# Lanes | 1 |  | 1 | 1 |  | 1 |  | 1 |  |  | 1 |  |
| LOS | A |  |  | A |  |  |  | D |  |  | E |  |
| Delay (s) | 9.0 |  |  | 8.4 |  |  |  | 29.5 |  |  | 37.1 |  |
| v/c | 0.02 |  |  | 0.01 |  |  |  | 0.28 |  |  | 0.36 |  |
| Queue (ft.) | 2.5 |  |  | 0 |  |  |  | 27.5 |  |  | 37.5 |  |
| Storage (ft.) |  |  |  |  |  |  |  |  |  |  |  |  |
| Additional Information |  |  |  |  |  |  |  |  |  |  |  |  |


| Year: 2047 | Future No-Build Conditions (Design Year) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L/T | - | R | L/T | - | R | - | All | - | - | All | - |
| \# Lanes | 1 |  | 1 | 1 |  | 1 |  | 1 |  |  | 1 |  |
| LOS | A |  |  | A |  |  |  | C |  |  | F |  |
| Delay (s) | 7.9 |  |  | 8.9 |  |  |  | 22.9 |  |  | 69.0 |  |
| v/c | 0.00 |  |  | 0.01 |  |  |  | 0.14 |  |  | 0.84 |  |
| Queue (ft.) | 0 |  |  | 0 |  |  |  | 12.5 |  |  | 165 |  |
| Storage (ft.) |  |  |  |  |  |  |  |  |  |  |  |  |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L/T | - | R | L/T | - | R | - | All | - | - | All | - |
| \# Lanes | 1 |  | 1 | 1 |  | 1 |  | 1 |  |  | 1 |  |
| LOS | A |  |  | A |  |  |  | E |  |  | F |  |
| Delay (s) | 9.2 |  |  | 8.5 |  |  |  | 40.8 |  |  | 56.9 |  |
| v/c | 0.03 |  |  | 0.01 |  |  |  | 0.44 |  |  | 0.56 |  |
| Queue (ft.) | 2.5 |  |  | 0 |  |  |  | 50 |  |  | 70 |  |
| Storage (ft.) |  |  |  |  |  |  |  |  |  |  |  |  |
| Additional Information |  |  |  |  |  |  |  |  |  |  |  |  |

## Alt. 1: Minor Road Stop Control with Slotted Left turns on Major Road:

Practical Feasibility:

| Public Opinion: | A public involvement meeting is scheduled in 2021. |
| ---: | :--- |
| Business Impacts: | None |
| ROW Impacts: | 0.07 Acres $(\$ 1,400)$ |
| Utility Impacts: | Unknown |
| Cost Estimate: | $\$ 1,630,000$ |
| Additional Info: | None |

## Safety Analysis:

| Crash Trend(s) being <br> Improved with Alt.: | The addition of slotted left turn lanes on STH 21 would address crashes related to left turning <br> vehicles and rear end crashes. |
| ---: | :--- |
| Geometric Concerns: | Due to the addition of left turn lanes, sideroad cross traffic will have additional travel length <br> to cross STH 21 or turn left onto STH 21. |
| Additional Info: | None |

Safety Performance Measures:

|  | Analysis Period | KABC | PDO | Total |
| :--- | :---: | :---: | :---: | :---: |
| Existing Conditions | $2014-2019$ | 11 | 4 | 15 |
| Future No-Build | $2027-2036$ | 4.918 | 11.153 | 16.071 |
| Alt. 1: Minor Road Stop Control <br> with Slotted Left turns on Major <br> Road: | $2027-2036$ | 2.557 | 5.800 | 8.357 |

Operational Analysis:

| Warrant Analysis: | N/A |
| ---: | :--- |
| Queue Impacts: | There are field entrances located on the north leg of Sand Pit Road at approximately 170' <br> north of the intersection. The southbound queue of 165' in 2047 approaches the first field <br> entrance. There is a commercial driveway on the south leg of Sand Pit Road at approximately <br> $185^{\prime}$ south of the intersection. The northbound queue does not impact this driveway. |
| Additional Capacity: | None |
| Railroad Impacts: | None |
| Additional Info: | In 2047, the southbound leg experiences a LOS of F in the am and pm peak hours and the <br> northbound leg experiences a LOS of E in the pm peak hour. |

Operational Performance Measures:

| Year: 2027 | Alt. 1: Minor Road Stop Control with Slotted Left turns on Major Road |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L | T | R | L | T | R | - | All | - | - | All | - |
| \# Lanes | 1 | 1 | 1 | 1 | 1 | 1 |  | 1 |  |  | 1 |  |
| LOS | A |  |  | A |  |  |  | C |  |  | E |  |
| Delay (s) | 7.9 |  |  | 8.8 |  |  |  | 20.1 |  |  | 37.6 |  |
| v/c | 0.00 |  |  | 0.01 |  |  |  | 0.10 |  |  | 0.60 |  |
| Queue (ft.) | 0 |  |  | 0 |  |  |  | 7.5 |  |  | 87.5 |  |
| Storage (ft.) | 300 |  |  | 300 |  |  |  |  |  |  |  |  |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L | T | R | L | T | R | - | All | - | - | All | - |
| \# Lanes | 1 | 1 | 1 | 1 | 1 | 1 |  | 1 |  |  | 1 |  |
| LOS | A |  |  | A |  |  |  | D |  |  | E |  |
| Delay (s) | 9.0 |  |  | 8.4 |  |  |  | 29.1 |  |  | 36.6 |  |
| v/c | 0.02 |  |  | 0.01 |  |  |  | 0.28 |  |  | 0.36 |  |
| Queue (ft.) | 2.5 |  |  | 0.0 |  |  |  | 27.5 |  |  | 37.5 |  |
| Storage (ft.) | 300 |  |  | 300 |  |  |  |  |  |  |  |  |
| Additional Information |  |  |  |  |  |  |  |  |  |  |  |  |


| Year: 2047 | Alt. 1: Minor Road Stop Control with Slotted Left turns on Major Road |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L | T | R | L | T | R | - | All | - | - | All | - |
| \# Lanes | 1 | 1 | 1 | 1 | 1 | 1 |  | 1 |  |  | 1 |  |
| LOS | A |  |  | A |  |  |  | C |  |  | F |  |
| Delay (s) | 7.9 |  |  | 8.9 |  |  |  | 22.8 |  |  | 68.3 |  |
| v/c | 0.00 |  |  | 0.01 |  |  |  | 0.14 |  |  | 0.84 |  |
| Queue (ft.) | 0 |  |  | 0 |  |  |  | 12.5 |  |  | 165 |  |
| Storage (ft.) | 300 |  |  | 300 |  |  |  |  |  |  |  |  |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L | T | R | L | T | R | - | All | - | - | All | - |
| \# Lanes | 1 | 1 | 1 | 1 | 1 | 1 |  | 1 |  |  | 1 |  |
| LOS | A |  |  | A |  |  |  | E |  |  | F |  |
| Delay (s) | 9.2 |  |  | 8.5 |  |  |  | 39.8 |  |  | 55.2 |  |
| v/c | 0.03 |  |  | 0.01 |  |  |  | 0.43 |  |  | 0.55 |  |
| Queue (ft.) | 2.5 |  |  | 0 |  |  |  | 50 |  |  | 67.5 |  |
| Storage (ft.) | 300 |  |  | 300 |  |  |  |  |  |  |  |  |
| Additional Information |  |  |  |  |  |  |  |  |  |  |  |  |

Alt. 2: Roundabout:
Practical Feasibility:

| Public Opinion: | A public involvement meeting is scheduled in 2021. |
| ---: | :--- |
| Business Impacts: | Roundabout is designed to accommodate OSOW vehicles. There are no impacts to <br> businesses. |
| ROW Impacts: | 0.731 Acres, $\$ 34,000$ |
| Utility Impacts: | Unknown |
| Cost Estimate: | $\$ 2,000,000$ |
| Additional Info: | None |

## Safety Analysis:

| Crash Trend(s) being <br> Improved with Alt.: | The installation of a roundabout at the intersection of STH 21 and Sand Pit Road would <br> address right-angle crashes and left turning crashes at the intersection. |
| ---: | :--- |
| Geometric Concerns: | None |
| Additional Info: | None |

## Safety Performance Measures:

|  | Analysis Period | KABC | PDO | Total |
| :--- | :---: | :---: | :---: | :---: |
| Existing Conditions | $2014-2019$ | 11 | 4 | 15 |
| Future No-Build | $2027-2036$ | 4.918 | 11.153 | 16.071 |
| Alt. 2: Roundabout: | $2027-2036$ | 2.965 | 18.645 | 21.610 |

## Operational Analysis:

| Warrant Analysis: | N/A |
| ---: | :--- |
| Queue Impacts: | There are field entrances located on the north leg of Sand Pit Road at approximately 170' <br> north of the intersection. There is a commercial driveway on the south leg of Sand Pit Road at <br> approximately 185' south of the intersection. The southbound and northbound queues do <br> not impact these driveways. |
| Additional Capacity: | All legs operate at a LOS of A in 2047 for the AM and PM peak hours. This alternative has <br> additional capacity compared to alternative 1. |
| Railroad Impacts: | None |
| Additional Info: | All legs operate at a LOS of A in 2047 for the AM and PM peak hours. |

Operational Performance Measures:

| Year: 2027 | Alt. 2: Roundabout |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | - | All | - | - | All | - | - | All | - | - | All | - |
| \# Lanes |  | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |
| LOS |  | A |  |  | A |  |  | A |  |  | A |  |
| Delay (s) |  | 9.3 |  |  | 4.7 |  |  | 5.7 |  |  | 5.0 |  |
| v/c |  | 0.536 |  |  | 0.231 |  |  | 0.038 |  |  | 0.153 |  |
| Queue (ft.) |  | 93.1 |  |  | 28.6 |  |  | 3.5 |  |  | 16.1 |  |
| Storage (ft.) |  |  |  |  |  |  |  |  |  |  |  |  |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | - | All | - | - | All | - | - | All | - | - | All | - |
| \# Lanes |  | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |
| LOS |  | A |  |  | A |  |  | A |  |  | A |  |
| Delay (s) |  | 6.7 |  |  | 8.8 |  |  | 5.2 |  |  | 5.6 |  |
| v/c |  | 0.399 |  |  | 0.536 |  |  | 0.071 |  |  | 0.083 |  |
| Queue (ft.) |  | 60.2 |  |  | 101.0 |  |  | 6.8 |  |  | 7.9 |  |
| Storage (ft.) |  |  |  |  |  |  |  |  |  |  |  |  |
| Additional Information |  |  |  |  |  |  |  |  |  |  |  |  |


| Year: 2047 | Alt. 2: Roundabout |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | - | All | - | - | All | - | - | All | - | - | All | - |
| \# Lanes |  | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |
| LOS |  | B |  |  | A |  |  | A |  |  | A |  |
| Delay (s) |  | 10.6 |  |  | 4.9 |  |  | 6.1 |  |  | 5.6 |  |
| v/c |  | 0.587 |  |  | 0.248 |  |  | 0.050 |  |  | 0.201 |  |
| Queue (ft.) |  | 105.7 |  |  | 31.2 |  |  | 4.5 |  |  | 21.9 |  |
| Storage (ft.) |  |  |  |  |  |  |  |  |  |  |  |  |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | - | All | - | - | All | - | - | All | - | - | All | - |
| \# Lanes |  | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |
| LOS |  | A |  |  | A |  |  | A |  |  | A |  |
| Delay (s) |  | 7.3 |  |  | 9.8 |  |  | 5.6 |  |  | 6.0 |  |
| v/c |  | 0.432 |  |  | 0.585 |  |  | 0.098 |  |  | 0.111 |  |
| Queue (ft.) |  | 67.4 |  |  | 117.8 |  |  | 9.3 |  |  | 10.5 |  |
| Storage (ft.) |  |  |  |  |  |  |  |  |  |  |  |  |
| Additional Information |  |  |  |  |  |  |  |  |  |  |  |  |

## Attachments:

(Provide attachments outline in FDM 11-25-3 Attachment 3.7 as appropriate)

1. Project Location Map
2. Aerial Photo
3. Traffic Data
4. Crash Diagram
5. Exhibits
a. Existing
b. Alternative 1 - Left Turn Lane
c. Alternative 2 - Roundabout
6. Safety Certification Document
7. Signal Warrants
8. Capacity Analysis
a. HCS
b. SIDRA 9


6180-30-00
STH 21
STH 116 - Leonard Point Rd Winnebago County

Intersection STH 21 \& Sand Pit Rd



WisDOT Bureau of Planning \& Economic Development

Design Hour Turning Movement Data

Projected PM Design Hour Traffic Volumes
$\int$ Indicates roundabout
Design Hour: 3:30-4:30pm
Forecast Completed: 10/26/2020

## Project Description

Project ID(s): 6180-30-00
Route(s): STH 21
Region/COUNTY(IES): NE/Winnebago
Location: @ Sand Pit Rd






Date: August 6, 2020

To: WisDOT NE Region Planning Chief: Brian Brock
Bureau of Traffic Operations - Traffic Engineering and Safety Section (BTOSafetyEngineering@dot.wi.gov)

From: Scott Nelson
WisDOT NE Region

Subject: SAFETY CERTIFICATION DOCUMENT
Project I.D. (design) 6180-30-00
STH 21 from STH 116 - Leonard Point Road
Winnebago County

Having considered the safety performance of the existing corridor and any proposed improvements, we believe this document reflects the intent of the policy and guidelines described in section 11-38 of the Wisconsin Facilities Development Manual.

Concurrence:

| $\frac{\text { Kevin M. Scopoline }}{\text { Bureau of Traffic Operations }}$Traffic Engineering and Safety Section |  |
| :--- | :--- |
| Date |  |

Approval:

> Bran S. Bund

9/14/2020
Date

## SAFETY CERTIFICATION DOCUMENT

Analyst: Scott A. Nelson

| Design ID: | $6180-30-00$ |
| ---: | :--- |
| Highway: | STH 21 |
| Project Title: | Omro - Oshkosh, STH 116 - Leonard Pt Rd |
| Improvement Concept Code: | RSRF10 |

Improvement Concept Code: RSRF10

## 1. Did the project have Sites of Promise from the system screening?

Yes $\boxtimes \quad$ No $\square$
Comments:

PDP ID 4284 - STH 116 to Webster - Crash Rate Flag 2.11, KAB Crash Rate Flag 2.09
PDP ID 4289 - CTH FF to Sand Pit Road - KAB Crash Rate Flag 1.46
PDP ID 4290 - Sand Pit Road to Leonard Point Road - Crash Rate Flag 1.18, KAB Crash Rate Flag 1.79
IX_70_02975 - STH 21 \& STH 116 - Total Crash LOSS 4, PSI 3.97, KABC LOSS 4, PSI 0.84
IX_70_02977 - STH 21 \& Madison Ave - Total Crash LOSS 4, PSI 2.39
IX_70_02978 - STH 21 \& Monroe St - KABC LOSS 4, PSI 0.45
IX_70_02980 - STH 21 \& Quincy - KABC LOSS 4, PSI 1.16
IX_70_03026 - STH 21 \& McKinley Ave - KABC LOSS 4, PSI 0.45
IX_70_03024 - STH 21 Beckwith Ave - KABC LOSS 4, PSI 0.45
IX_70_03034 - STH 21 \& Alder Ave \& Goldenrod Dr - Total Crash LOSS 4, PSI 4.27, KABC LOSS 4, PSI 1.43
IX_70_02902 - STH 21 \& Rivermoor Rd - Total Crash LOSS 4, PSI 2.84
IX_70_02649 - STH 21 \& CTH FF/Reighmoor Rd - Total Crash LOSS 4, PSI 3.21, KABC LOSS 4, PSI 3.76
IX_70_02660 - STH 21 \& Sand Pit Rd - Total Crash LOSS 4, PSI 9.04, KABC LOSS 4, PSI 4.10
2. Did relevant crashes remain after the initial Crash Vetting Process?

Yes $\boxtimes \quad$ No $\square$
Comments:
PDP ID 4284 - STH 116 to Webster (Segment Identified) - Of the ten crashes in this segment, five crashes remained after vetting. Four WB rear end crashes at the Jefferson St intersection and one at driveway. A TWLTL was evaluated for feasibility by PDS preliminary engineering and it was determined to not be a feasible alternative.

PDP ID 4289 - CTH FF to Sand Pit Road (Segment Identified) - Of the twenty-two crashes in this segment, twelve crashes remain after vetting. Only one segment crash occurred near Potratz Hill, but no safety mitigation strategies are recommended base on this one isolated crash. The remaining crashes will be addressed in the intersection safety flag for the CTH FF/Reighmoor intersection.

PDP ID 4290 - Sand Pit Road to Leonard Point Road (Segment Identified) - Of the thirty-seven crashes in this segment, fourteen remaining after vetting. Nine of these crashes occurred at the Sand Pit Road intersection and will be addressed in the intersection safety flag below. The remaining five crashes involve drifting left of center along this segment. The improvement project will include centerline rumble stripes which should help address this crash trend.

IX_70_02975 - STH 21 \& STH 116 (Intersection Identified) - Of the eight crashes at this intersection, five remain after vetting. Four WB rear end crashes at the Jefferson St intersection and one at a driveway. A TWLTL was evaluated for feasibility by PDS preliminary engineering and it was determined to not be a feasible alternative.

IX_70_02977 - STH 21 \& Madison Ave (Intersection Identified) - One of the seven crashes remain after vetting. The crash involved a WB vehicle yielded to a pedestrian crossing North to South on the East side of the intersection. Another WB tried bypassing WB on right and struck the pedestrian. The crash could be classified as driver error by bypassing the yielding vehicle in front. No safety mitigation strategies are recommended based on this one crash.

IX_70_02978 - STH 21 \& Monroe St (Intersection Identified) - Of the four crashes at this intersection three remained after vetting. Two WB rear ends of left turns onto Monroe and one WB rear end turning into Kwik Trip. A TWLTL was evaluated for feasibility by PDS preliminary engineering and it was determined to not be a feasible alternative. No other safety mitigation strategies are recommended.

IX_70_02980 - STH 21 \& Quincy (Intersection Identified) - Of the three crashes at this intersection, one remained after vetting and it occurred at a driveway near the Quincy St. intersection. A WB rear end of left turning traffic into a driveway near Quincy Ave. No safety mitigation strategies are recommended based on this one crash.

IX_70_03026 - STH 21 \& McKinley Ave (Intersection Identified) - Of the four crashes at this intersection, three remain after vetting. Three WB rear end crashes have occurred with left turns onto McKinley Ave. A TWLTL was evaluated for feasibility by PDS preliminary engineering and it was determined to not be a feasible alternative. No other safety mitigation strategies are recommended.

IX_70_03024 - STH 21 Beckwith Ave (Intersection Identified) - Of the four crashes at this intersection, no crashes remain after vetting. No safety mitigation strategies are recommended.

IX_70_03034 - STH 21 \& Alder Ave \& Goldenrod Dr (Intersection Identified) - Of the ten crashes at this intersection, three remained after vetting. Two EB rear end crashes while turning onto Goldenrod and on WB rear end crash while turning onto Alder Ave. A TWLTL was evaluated for feasibility by PDS preliminary engineering and it was determined to not be a feasible alternative. No other safety mitigation strategies are recommended.

IX_70_02902 - STH 21 \& Rivermoor Rd (Intersection Identified) - Of the four crashes at this intersection, no crashes remain after vetting. No safety mitigation strategies are recommended.

IX_70_02649 - STH 21 \& CTH FF/Reighmoor Rd (Intersection Identified) - Of the eleven crashes at this intersection, nine crashes remain after vetting. Six of the nine crashes involved left turning crashes from Hwy 21. One NB left failed to yield to a SB motorist. One SB failed to yield to WB. The remaining crash was not intersection related but the driver drifted off the roadway to the right. Two safety mitigation strategies are recommended to move forward with the CGA process. The first alternative is to add install positive offset left turn lanes on STH 21. The second alternative is to install a roundabout at the intersection.

IX_70_02660 - STH 21 \& Sand Pit Rd (Intersection Identified) - Of the eleven crashes at this intersection, eleven crashes remain after vetting. Ten of the eleven crashes involve a left turning vehicle from Highway 21. The specific crash types with the left turns are identified on the collision diagram in Appendix A. The remaining crash was a NB failure to yield to an EB. Two safety mitigation strategies are recommended to move forward with the CGA process. The first alternative is to add install positive offset left turn lanes on STH 21. The second alternative is to install a roundabout at the intersection.
3. Were possible safety mitigation alternatives identified in the CGA Process? Yes $\boxtimes \quad$ No $\square$

Comments:
IX_70_02649 - STH 21 \& CTH FF/Reighmoor Rd - Two safety mitigation strategies are recommended to move forward with the CGA process. The first alternative is to add install positive offset left turn lanes on STH 21. The second alternative is to install a roundabout at the intersection. Each alternative will target the six mainline left turn crashes that have occurred. Additionally, the two right-angle crashes can be targeted by the roundabout alternative.

IX_70_02660 - STH 21 \& Sand Pit Rd - Two safety mitigation strategies are recommended to move forward with the CGA process. The first alternative is to add install positive offset left turn lanes on STH 21. The second alternative is to install a roundabout at the intersection. Each alternative will target the ten mainline left turning crashes that have occurred. Additionally, the right-angle crash will be targeted by the roundabout alternative.
4. Were safety mitigation alternatives analyzed in this project?

Yes $\boxtimes \quad$ No $\square$

### 4.1. Provide narrative of existing geometric conditions and describe any geometric features that contributed to the type or severity of the crashes.

IX_70_02649 - STH 21 \& CTH FF/Reighmoor Rd - The current lane configuration at this intersection consists of a right turn lane and a shared through/left turn lane on STH 21. The absence of the left turn lane has contributed to one fatal crash, two suspect minor injury crashes, two possible injury crashes, and one property damage only crash. Based on mainline and sideroad volumes, picking an adequate gap is also challenging on the sideroad which has contributed to some of the other crashes. The remaining crashes resulted in two suspected minor
injuries, and one possible injury crash.
IX_70_02660 - STH 21 \& Sand Pit Rd - The current lane configuration at this intersection consists of a right turn lane and a shared through/left turn lane on STH 21. The absence of the left turn lane has contributed to five suspected minor injuries, three possible injuries, and two property damage only crashes. The remaining rightangle crash resulted in property damage only.

### 4.2. Provide narrative of crash history, crash trends, and contributing factors that were targeted in the safety mitigation alternatives.

IX_70_02649 - STH 21 \& CTH FF/Reighmoor Rd - Of the eleven crashes at this intersection, nine crashes remain after vetting. Six of the nine crashes involved left turning crashes from Hwy 21. One NB left failed to yield to a SB motorist. One SB failed to yield to WB. The remaining crash was not intersection related but the driver drifted off the roadway to the right. The current lane configuration at this intersection consists of a right turn lane and a shared through/left turn lane on STH 21. The absence of the left turn lane has contributed to one fatal crash, two suspect minor injury crashes, two possible injury crashes, and one property damage only crash. The remaining crashes resulted in two suspected minor injuries and one property damage only crash. The left turn lane alternative will target the left turn crashes. The roundabout alternative will target the left turn crashes and rightangle crashes.

IX_70_02660 - STH 21 \& Sand Pit Rd - Of the eleven crashes at this intersection, eleven crashes remain after vetting. Ten of the eleven crashes involve a left turning vehicle from Highway 21. One NB motorist failed to yield to a EB motorist. The current lane configuration at this intersection consists of a right turn lane and a shared through/left turn lane on STH 21. The absence of the left turn lane has contributed to five suspected minor injuries, three possible injuries, and two property damage only crashes. The remaining right-angle crash resulted in property damage only. The left turn lane alternative will target the left turn crashes. The roundabout alternative will target the left turn crashes and right-angle crashes.

### 4.3. Provide narrative and the name for each safety mitigation alternative analyzed in SMCP

STH 21 \& CTH FF/Reighmoor Rd
Concrete Repair \& Overlay - Base case with no geometric improvements.
STH 21 Left Turn Lanes - Add EB and WB left turn lanes on STH 21. Final geometry for EB and WB approaches will consist of a left turn lane, a through lane, and a right turn lane.

Single lane roundabout - Construct a single lane roundabout at the CTH FF/Reighmoor Rd intersection.

STH 21 \& Sand Pit Road
Concrete Repair \& Overlay - Base case with no geometric improvements.
STH 21 Left Turn Lanes - Add EB and WB left turn lanes on STH 21. Final geometry for EB and WB approaches will consist of a left turn lane, a through lane, and a right turn lane.

Single lane roundabout - Construct a single lane roundabout at the Sand Pit Rd intersection.

Analysis Location: STH 21 \& CTH FF/Reighmoor Rd Analysis Method: 2a

|  | Base | Alt. A | Alt. B | Add/Remove <br> columns |
| :--- | :---: | :---: | :---: | :---: |
| Alternative Name | Concrete <br>  <br> Overlay | STH 21 Left <br> Turn Lanes | Roundabout |  |
| Fatal \& Injury | 5.806 | 3.019 | 2.360 |  |
| Property Damage | 13.169 | 6.848 | 15.651 |  |
| Total | 18.975 | 9.867 | 18.011 |  |
| Benefits | - | $\$ 1,653,033.89$ | $\$ 2,744,853.97$ |  |
| Net Cost | $\$ 0$ | $\$ 660,000$ | $\$ 780,000$ |  |
| B/C |  | $\mathbf{2 . 5 0 4 6}$ | $\mathbf{3 . 5 1 9 0}$ |  |

Comments:
Both the left turn lane and roundabout alternative have B/C greater than 1.0 using IHSDM with Wisconsin calibration, crash distribution, model, and economic analysis model data sets. No external CMF's were applied.

Analysis Location: STH 21 \& Sand Pit Road
Analysis Method: 2a

|  | Base | Alt. A | Alt. B | Add/Remove <br> columns |
| :--- | :---: | :---: | :---: | :---: |
| Alternative Name | Concrete <br>  <br> Overlay | STH 21 Left <br> Turn Lanes | Roundabout |  |
| Fatal \& Injury | 4.918 | 2.557 | 2.965 |  |
| Property Damage | 11.153 | 5.800 | 18.645 |  |
| Total | 16.071 | 8.357 | 21.610 |  |
| Benefits | - | $\$ 1,400,196.68$ | $\$ 2,108,056.68$ |  |
| Net Cost | $\$ 0$ | $\$ 550,000$ | $\$ 730,000$ |  |
| B/C |  | $\mathbf{2 . 5 4 5 8}$ | $\mathbf{2 . 8 8 7 8}$ |  |

Comments:
Both the left turn lane and roundabout alternative have B/C greater than 1.0 using IHSDM with Wisconsin calibration, crash distribution, model, and economic analysis model data sets. No external CMF's were applied.
4.5. Provide narrative of reasonable and acceptable safety mitigation alternatives for consideration in the project improvement process

STH 21 \& CTH FF/Reighmoor Rd
Alt. A - STH 21 Left Turn Lanes - The addition of left turn lanes on STH 21 approaching CTH FF/Reighmoor Road should be considered as a feasible alternative for consideration through the NEPA process.

Alt. B - Single lane roundabout - A single lane roundabout at the intersection of STH 21 \& CTH FF/Reighmoor Rd should be considered as a feasible alternative for consideration through the NEPA process.

STH 21 \& Sand Pit Road
Alt. A - STH 21 Left Turn Lanes - The addition of left turn lanes on STH 21 approaching Sand Pit Road should be considered as a feasible alternative for consideration through the NEPA process.

Alt. B - Single Lane Roundabout - A single lane roundabout at the intersection of STH 21 \& Sand Pit Rd should be considered as a feasible alternative for consideration through the NEPA process.

## ATTACHMENTS

Include all attachments in the final SCD and submit as a PDF
A. Project Information
a. Project Location/Overview Map
b. Crash Diagram(s)
B. Sites of Promise Documentation
a. Meta-Manager spreadsheet
b. Intersection Network Screening spreadsheet
C. Crash Vetting Documentation
a. WisTransPortal crash data spreadsheet with vetting comments
D. Contributing Geometric Analysis Documentation
a. Safety Certification Worksheet
E. Safety Mitigation Certification Documentation
a. Layout/Schematic for each alternative
b. Cost estimate for each alternative
c. IHSDM Crash Prediction Evaluation Report for each alternative
d. IHSDM Economic Analysis Report
e. Highway Safety Benefit Cost Analysis Tool results

# ATTACHMENT A 

## Project Information

Project Location/Overview Map

# Safety Certification Mapping (SCM) Tool 

Design ID
6180-30-00
Project Title
OMRO - OSHKOSH
SCM Comment

Meta Manager Version: 2019-10
Meta Manager Crash Years: 2014-2018
SCM Crash Years: 2014-2018

Construction ID(s)

Project Description
STH 116 - LEONARD POINT ROAD

Sites of Promise

| Corridor \# | Highway | Start County | End County | Start RP | End RP |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | WIS 21 EB | WINNEBAGO | WINNEBAGO | 021E162T000 | 021E170K000 |
| $4284: \overline{\mathrm{KAB}, \text { Crash Rate }}$ |  |  |  |  |  |
| 4289: KAB |  |  |  |  |  |
| $4290: \mathrm{KAB}$, Crash Rate |  |  |  |  |  |



Corridor \# 1: WIS 21 EB - 021E162T000-021E170K000

| Meta Manager Version: 2019-10 |  |  | Crash Years: 2014-2018 |  | SCM Crash Years: 2014-2018 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PDP ID | Crash | KAB | Int Crash | Int KAB | K | A | B | C | O | TOTAL |
| 4284 | 2.1088 | 2.0873 |  |  |  |  | 2 | 1 | 7 | 10 |
| 4285 |  |  |  |  |  |  |  |  | 5 | 5 |
| 4286 |  |  |  |  |  |  | 9 | 5 | 22 | 36 |
| 4287 |  |  |  |  |  | 1 | 3 | 2 | 12 | 18 |
| 4288 |  |  |  |  |  |  | 6 | 3 | 13 | 22 |
| 4289 |  | 1.4584 |  |  | 1 | 1 | 7 | 7 | 6 | 22 |
| 4290 | 1.1763 | 1.7913 |  |  | 1 |  | 13 | 6 | 17 | 37 |
| TOTAL |  |  |  |  | 2 | 2 | 40 | 24 | 82 |  |

Manner of Collision

| PDP ID | NO COLLISION | REAR END | SS OPP | SS SAME | OTHER | TOTAL |
| :--- | :--- | :---: | :--- | :---: | :---: | :---: |
| 4284 |  | 9 |  |  | 1 | 10 |
| 4285 | 1 | 2 |  | 1 | 1 | 5 |
| 4286 | 9 | 20 | 1 |  | 6 | 36 |
| 4287 | 3 | 7 | 1 |  | 7 | 18 |
| 4288 | 12 | 7 |  | 1 | 2 | 22 |
| 4289 | 8 | 8 |  |  | 6 | 22 |
| 4290 | 10 | 17 | 2 | 1 | 7 | 37 |

# ATTACHMENT A 

## Project Information

Crash Diagram(s)



# ATTACHMENT B 

# Sites of Promise Documentation 

Meta-Manager Spreadsheet

# ATTACHMENT B 

## Sites of Promise Documentation

Intersection Network Screening Spreadsheet



| Intersection Network Screening <br> Updated: 132020 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Safety Certification Worksheet Information |  |  |  |  |  | Data Needed for SPFs |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | SPF Results |  |  |  |  |  |
|  |  |  |  |  |  | TOTAL Crashes (values for entire analysis | KABC Crashes(values for entire analysis |  |  |
|  | $\stackrel{\text { crorat }}{\text { coss }}_{\text {coss }}^{\text {corat }}$ | $\underset{\substack{\text { PSI } \\ \text { (Tratal }}}{\square}$ | $\begin{aligned} & \text { (Kase } \\ & \text { Kass } \end{aligned}$ | $\stackrel{\text { PSI }}{\substack{\text { KRBCOC }}}$ | Flagged Locatiol (Yortho) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Region | Countr ${ }^{-}$ | Area <br> Typ - | $\begin{gathered} \text { Ramp } \\ \text { Termil } \end{gathered}$ | Number of Lf | Control Typ - | Median Typ . | Number of tar | $\begin{aligned} & \text { Major } \\ & \text { AAD } \\ & \hline \end{aligned}$ |  | Inside <br> Ramn <br> AAI ${ }^{-}$ | Outside <br> Ramn <br> AAD | Off Ramp On Ramp AAD $\square$ AAD - |  | Number of Ram! | Total <br> AAI | $\begin{array}{\|c\|c\|} \hline \text { Years of } & \text { Crash Datal } \\ \left\lvert\, \begin{array}{c\|} \text { Crash } \mathrm{I} \\ \hline \end{array}\right. & \text { Rang } \\ \hline \end{array}$ |  | Observed (Tore | Predicted (ToTA | Expected (TOTA | $\begin{gathered} \text { Observed } \\ \text { CKAEE } \end{gathered}$ |  |  |
| 25458 \|X_70_0295\% STH 21\& Arboretu | L0S5 2 | -1.76 | L05S2 | -0.09 | No | NE | Winnebago | URBAN | FALSE | 4 | TWSC | JNDIVIVEL |  | 12418 | 433 | - | , | - |  |  | ${ }^{12851}$ |  | 2014-2018 | 5 | 7.27 | 5.51 | ${ }^{2}$ | 2.15 | 2.06 |
| $254591 \times$-70-02966 USH $45 \%$ WBent | Loss 3 | 0.54 | LOSS 2 | -0.33 | No | NE | Winnebago | UREAN | FALSE | 4 | TWSC | JNDIVIIDE | 2 | 14576 | 433 | 0 | 0 | 0 | 0 | 0 | 15009 | 5 | 2014-2018 | 9 | 8.32 | 8.86 | 2 | 2.52 | 2.20 |
| $254501 \times$ 1-70_0297: STH 218 A Adams 4 | LOSS 2 | -0.36 | Loss2 | -0.95 | No | NE | Winnebago | RUPAL | FALSE | 4 | OTHER | JNDIVIIDE[ | 1 | 12166 | 374 | 0 | 0 | 0 | 0 | 0 | 12540 | 5 | 2014-2018 | 5 | 5.50 | 5.14 | 0 | 1.62 | 0.67 |
| $254611 \times$-70_02975 STH $21 \&$ STH 116 | LOSS 4 | 3.97 | LOSS 4 | 0.84 | Yes | NE | Wirnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIDE[ | 1 | 12166 | 1446 | 0 | 0 | 0 | 0 | 0 | 13612 | 5 | 2014-2018 | ${ }^{10}$ | 4.48 | 8.45 | 3 | 1.35 | 2.19 |
| 25462 1X-70_02977 STH 21\% Webster | Loss 3 | 1.07 | LOSS 2 | -0.39 | No | NE | Winnebago | RUPAL | FALSE | 3 | TWSC | JMDIVIIEE | 1 | 9196 | 914 | 0 | 0 | 0 | 0 | 0 | 10110 | 5 | 2014-2018 | 5 | 3.37 | 4.44 | 0 | 0.94 | 0.55 |
| $254631 \times 70$ - 02397 STH 218 Madison | LOSS 4 | 2.39 | LOSS 3 | 0.02 | Yes | NE | Wirnebago | RUPAL | FALSE | 3 | TWSC | JMDIVIIDE[ | 1 | 9196 | 914 | 0 | 0 | 0 | 0 | 0 | 10110 | 5 | 2014-2018 | 7 | 3.37 | 5.76 | 1 | 0.94 | 0.97 |
| $254641 \times$ 70_02976 STH 218 . Monroe | LOSS 3 | 0.62 | LOSS 4 | 0.45 | Yes | NE | Winnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIIEE | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | ${ }^{4}$ | 3.02 | 3.64 | 2 | 0.72 | 1.17 |
| $254651 \times$-70_02988 STH 21\& Quincy | LOSS 3 | 0.62 | LOSS 4 | 1.16 | Yes | NE | Wirnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIVE[ | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | 4 | 3.02 | 3.64 | 4 | 0.72 | 1.88 |
| 2546611 -70 02988 STH 211 Jackson | LOSS 3 | 1.25 | LOSS 3 | 0.10 | No | NE | Winnebago | RURAL | FALSE | 3 | TWSC | JNDIVIDEC | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | 5 | 3.02 | 4.28 | 1 | 0.72 | 0.82 |
| 25467 1X 70 -02988 STH 218 Van Bur | LOSS 2 | $-0.65$ | LOSS 2 | $-0.25$ | No | NE | Wirnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIIDE[ | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | 2 | 3.02 | 2.37 | 0 | 0.72 | 0.46 |
| $254681 \times 70$-7029385 STH 218 Harrison | LOSS 2 | -2.68 | LOSS 2 | -0.79 | No | NE | Winnebago | RUPAL | FALSE | 4 | TWSC | JNDIVIVEE | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | 1 | 4.86 | 2.18 | 0 | 1.43 | 0.63 |
| $254691 \times 70$ - 703014 USH $45 \&$ Stanley | LOSS 2 | $-0.87$ | LOSS 2 | -0.79 | No | NE | Winnebago | UREAN | FALSE | 3 | TWSC | JNDIVIVE[ | 2 | 14576 | 433 | 0 | 0 | 0 | 0 | 0 | 15009 | 5 | 2014-2018 | 4 | 5.15 | 4.28 | 0 | 1.54 | 0.75 |
| $254701 \times 70$-703018 STH 218. Maplewb | LOSS 2 | $-0.65$ | LOSS 3 | 0.10 | No | NE | Wirnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIVEE | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | 2 | 3.02 | 2.37 | 1 | 0.72 | 0.82 |
| $25471 \times 1 \times$ 70-03022 STH 21\& Hollister | LOSS 2 | -1.77 | LOSS 2 | -0.13 | No | NE | Wirnebago | UREAN | FALSE | 3 | TWSC | JNDIVIIDE[ | 2 | 12418 | 433 | 0 | 0 | 0 | 0 | 0 | 12851 | 5 | 2014-2018 | 2 | 4.44 | 2.67 | 1 | 1.27 | 1.15 |
| $254721 \times$-7000302: STH 218 Lincoln, | LOSS 2 | -0.65 | LOSS 2 | -0.25 | No | NE | Winnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIIEE | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | 2 | 3.02 | 2.37 | 0 | 0.72 | 0.46 |
| $254731 \times 70$-03022 STH 21\& Beckwith | LOSS 3 | 0.62 | LOSS 4 | 0.45 | Yes | NE | Winnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIIDE[ | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | 4 | 3.02 | 3.64 | 2 | 0.72 | 1.17 |
| $25474 \mid \times 70$-0302E STH 218 McKirle | LOSS 3 | 0.62 | LOSS 4 | 0.45 | Yes | NE | Winnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIIDE[ | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | ${ }^{4}$ | 3.02 | 3.64 | ${ }^{2}$ | 0.72 | 1.17 |
| $254751 \times 1 \times$-70 O3022 STH 21\& Omreau | LOSS 2 | -0.65 | LOSS 3 | 0.10 | No | NE | Winnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIIEE | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | 2 | 3.02 | 2.37 | 1 | 0.72 |  |
| $254761 \times$ P70 O3022 STH 21\& Goldenro | Missing DatM | ssing Data | lissing Datd | ssing Dati | Missing Data | NE | Wirnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIVE[ | 1 | 10384 | , | 0 | 0 | 0 | 0 | 0 | 10384 | 5 | 2014-2018 | 1 1 | dissing Dalu | dissing D | - 0 | dissing Dalu | /lissing Dat. |
| 25477 1X 70-03033 STH 218 Industria | LOSS 2 | $-1.12$ | LOSS 3 | 0.43 | No | NE | Wirnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIIEE | 1 | 10384 | 914 | 0 | 0 | 0 | 0 | 0 | 11298 | 5 | 2014-2018 | 2 | 3.66 |  | - 2 |  |  |
| 25478 \|x-70_03033 STH 21\& Alder A. | LOS5 4 | 4.27 | LOS5 4 | 1.43 | Yes | NE | Winnebago | RUPAL | FALSE | 4 | TWSC | JNDIVIIDE[ | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | ${ }^{11}$ | 4.86 | 9.13 | 4 | 1.43 | ${ }^{2} 86$ |
| 25479 1X-70_0304: STH 21\& Erooke 5 | LOSS 3 | 0.10 | LOSS 2 | $-0.79$ | No | NE | Winnebago | RUPAL | FALSE | 4 | TWSC | JNDIVIIDE[ | 1 | 10384 | 374 | 0 | 0 | 0 | 0 | 0 | 10758 | 5 | 2014-2018 | 5 | 4.86 | 4.96 | 0 | 1.43 | 0.63 |
| 25480 1X 70-03055: USH 45 \& Hobbs $A$ | LOSS 3 | 1.76 | LOSS 4 | 0.81 | Yes | NE | Wirnebago | UREAN | FALSE | 3 | TWSC | Ralised | 2 | 14576 | 433 | 0 | 0 | 0 | 0 | 0 | 15009 | 5 | 2014-2018 | 7 | 4.60 | 6.36 | 3 | 1.23 | 2.04 |
| $254811 \times 70$-03066 USH $45 \&$ STH 21 | LOSS 3 | 5.36 | LOSS 2 | -0.19 | No | NE | Winnebago | UREAN | FALSE | 3 | SIINAL | RAISED |  | 12418 | 8010 | 0 | 0 | 0 | 0 | 0 | 20428 | 5 | 2014-2018 | 22 | 15.62 | 20.98 | 4 | 4.29 | 4.11 |
| $254821 \times$ 70-03066 USH 45 \& Plymout | LOSS 1 | -2.53 | LOSS 2 | -0.41 | No | NE | Winnebago | URBAN | FALSE | 3 | TWSC | JNDIVIVE[ | 2 | 10146 | 433 | 0 | 0 | 0 | 0 | 0 | 10579 | 5 | 2014-2018 | 0 | 3.68 | 1.15 | 0 | 1.00 | 0.60 |
| $254831 \times$-70 03077 USH 458 \& Sherida | LOSS 2 | -3.08 | LOSS 2 | -0.40 | No | NE | Winnebago | UREAN | FALSE | 4 | TWSC | JNDIVIVE[ | 2 | 10146 | 433 | 0 | 0 | 0 | 0 | 0 | 10579 | 5 | 2014-2018 | 2 | 6.13 | 3.05 | 1 | 1.76 | 1.36 |
| $254881 \times$ \| 70 -03071USH $45 \&$ Crane 5 | LOSS 2 | -1.15 | LOSS2 | 0.00 | No | NE | Winnebago | URBAN | FALSE | 3 | TWSC | JNDIVIIDE[ | 2 | 10146 | 433 | 0 | 0 | 0 |  | 0 | 10579 | 5 | 2014-2018 | 2 | 3.68 | 2.52 | 1 | 1.00 | 1.00 |
| $254851 \times$ \| 70 -03072 USH 458 \& Dlive St | LOSS 2 | -1.84 | LOSS 2 | -0.41 | No | NE | Winnebago | UREAN | FALSE | 3 | TWSC | JNDIVIVE[ | 2 | 10146 | 433 | 0 | 0 | 0 | 0 | 0 | 10579 | 5 | 2014-2018 | 1 | 3.68 | 1.84 | 0 | 1.00 | 0.60 |
| $254861 \times$-70-03077 USH 458 \& Mitchell | LOSS 2 | -1.15 | LOSS 2 | -0.41 | No | NE | Winnebago | URBAN | FALSE | 3 | TWSC | JNDIVIIDE[ | 2 | 10146 | 433 | 0 | 0 | 0 | 0 | 0 | 10579 | 5 | 2014-2018 | 2 | 3.68 | 2.52 | 0 | 1.00 | 0.60 |
| 25487 1X-70_03072 USH $458 . E$ Elmwoo | Loss 3 | 2.21 | LOSS 4 | 2.19 | Yes | NE | Winnebago | UREAN | FALSE | 4 | TWSC | JNDIVIIDE[ | 2 | 11350 | 2544 | 0 | 0 | 0 | 0 | 0 | 13894 | 5 | 2014-2018 | 16 | 13.45 | 15.66 |  | 3.95 | 6.14 |
| 25488 1X 70 -03072 USH 45 \& Walnut: | LOSS 2 | -2.19 | LOSS 2 | -0.50 | No | NE | Wirnebago | URBAN | FALSE | 3 | TWSC | JNDIVIIDE[ | 2 | 11350 | 433 | 0 | 0 | 0 | 0 | 0 | 11783 | 5 | 2014-2018 | 1 | 4.08 | 1.90 | 0 | 1.14 | 0.64 |
| $254891 \times$ P70 03076 USH 458 \& Cedar 5 | LOSS 2 | -0.77 | LOSS 3 | 0.37 | No | NE | Wirnebago | UREAN | FALSE | 3 | TWSC | JNDIVIIEE |  | ${ }^{11350}$ | 433 | 0 | 0 | 0 | 0 | 0 | 11783 | 5 | 2014-2018 | 3 | 4.08 | 3.31 | 2 | 1.14 | 1.52 |
| $254901 \times 1 \times 70$-0307, USH $45 \times$ Beech | LOSS 2 | -2.85 | LOSS 2 | -1.10 | No | NE | Winnebago | URBAN | FALSE | 4 | TWSC | JNDIVIVEE | 2 | 11350 | 433 | 0 | 0 | 0 | 0 | 0 | 11783 | 5 | 2014-2018 | 3 | 6.74 | 3.88 | 0 | 1.97 | 0.87 |
| $254911 \times .70$ O3077 USH 458 L Liberty S | LOSS 2 | -2.19 | LOSS 2 | $-0.06$ | No | NE | Wirnebago | UREAN | FALSE | 3 | TWSC | JNDIVIIDE[ | 2 | 11350 | 433 | 0 | 0 | 0 | 0 | 0 | 11783 | 5 | 2014-2018 | 1 | 4.08 | 1.90 | 1 | 1.14 | 1.08 |
| $254921 \times 1 \times 70$ O3077 USSH $45 \&$ Westerr | LOSS 2 | -0.77 | LOSS 2 | $-0.50$ | No | NE | Winnebago | URBAN | FALSE | 3 | TWSC | JNDIVIVEL | 2 | ${ }^{11350}$ | 433 | 0 | 0 | 0 | 0 | 0 | ${ }^{11783}$ | 5 | 2014-2018 | 3 | 4.08 | 3.31 | 0 | 1.14 | 0.64 |
| $254931 \times$-70_0308C USH $45 \&$ STH 76 | LOS5 4 | 54.20 | LOSS 4 | 18.72 | Yes | NE | Winnebago | UREAN | FALSE | 4 | RAB | RAISED | 2 | 18786 | 11905 | 0 | 0 | 0 | 0 | 0 | 30691 | 5 | 2014-2018 | ${ }^{112}$ | 55.04 | 109.24 | 36 | 10.00 | 28.72 |
| $254941 \times$ \| 70 O_0308\% STH 116 \& Webste | LOSS 4 | 1.55 | LOSS 3 | 0.12 | Yes | NE | Winnebago | RUPAL | FALSE | 3 | TWSC | JNDIVIIDE[ | 1 | 5000 | 914 | 0 | 0 | 0 | 0 | 0 | 5914 | 5 | 2014-2018 | 5 | 2.25 | 3.80 | 1 | 0.63 | 0.75 |
| $254951 \times 1 \times 70$ O3088: USH 45 \& Ontario | LOSS 2 | -2.19 | LOSS 2 | -0.50 | No | NE | Winnebago | UREAN | FALSE | 3 | TWSC | JNDIVIVE[ | 2 | 11350 | 433 | 0 | 0 | 0 | 0 | 0 | 11783 | 5 | 2014-2018 | 1 | 4.08 | 1.90 | 0 | 1.14 | 0.64 |
| $254961 \times$ IX 70 O3088 USH 45 \& Wiscons | LOS5 3 | 8.83 | LOSS 3 | 0.86 | No | NE | Winnebago | URBAN | FALSE | 4 | SIGNAL | JNDIVIIDE[ | 2 | 11350 | 4579 | 0 | 0 | 0 | 0 | 0 | 15929 | 5 | 2014-2018 | ${ }^{36}$ | 25.87 | 34.69 | 9 | 7.74 | 8.61 |
| $254971 \times$-70 03008 STH 116 \& Cedar | LOSS 2 | -0.44 | LOSS 2 | -0.11 | No | NE | Winnebago | FURAL | FALSE | 3 | TWSC | JNDIVIVEL | 1 | 5000 | 374 | 0 | 0 | 0 | 0 | 0 | 5374 | 5 | 2014-2018 | 20 | ${ }^{1.86}$ | 1.42 | 0 | 0.45 | 0.33 |
| $254981 \times 1 \times 70$ 0309: STH 218 STH 116 | LOSS 4 | 5.60 | LOSS3 | 0.54 | Yes | NE | Winnebago | RURAL | FALSE |  | SIIGNAL | PCR | 1 | 12166 | 374 | 0 | 0 |  | 0 |  | 12540 | 5 | 2014-2018 | 20 | 12.51 | 18.11 | 4 | 2.94 | 3.48 |
| $254991 \times 7003096$ STH 116 \& Dak St | LOSS4 | 1.11 | L05S2 | -0.04 | Yes | NE | Winnebago | RURAL | FALSE |  | TWSC | JNDIVIDEL |  | 2136 | 374 |  |  |  |  |  | 2510 |  | 2014-2018 | 4 | 1.06 | 2.17 |  | 0.26 | 0.22 |

# ATTACHMENT C Crash Vetting Documentation 

WisTransPortal crash data spreadsheet with vetting comments



## ATTACHMENT D

# Contributing <br> Geometric Analysis Documentation 

Safety Certification Worksheet

## Safety Certification Worksheet

| Analyst: Nelson, Scott A | Design ID: 6180-30-00 |
| :---: | :---: |
| Agency: WisDOT DTSD NE Region | Highway: WIS 21 EB |
| Date of Analysis: 2020-04-08 | Project Title: OMRO-OSHKOSH |
| Meta Manager Version: 2019-10 | Project Description: STH 116-LEONARD POINT ROAD |
| Meta Manager Crash Years: 2014-2018 | Worksheet ID: 2716 |


| System Screening - Sites of Promise |  |  |  |  |  |  | Crash Vetting - Sites of Promise | Contributing Geo | ometric Analysis |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| See FDM 11-38-10.2 for guidance |  |  |  |  |  |  | See FDM 11-38-10.3 for guidance | See FDM 11-38-10.4 for guidance |  |
| Segments: Meta-Manager |  |  |  |  |  |  |  |  |  |
| PDP ID | From RP | RP Description | To RP | Length (PDP_Mile) | Crash Rate Flag (RATEFLAG) (Insert value if $\geq 1.0$ ) | KAB Crash Rate Flag (MMGR_KAB_CRSH_RT) (Insert value if $\geq 1.00$ ) | Summarize the contributing factors for ALL crashes in the flagged segment. | Which geometric features contribute to the type and severity of the crashes? | Possible Countermeasures for Safety Mitigation Process |
| 4284 | 021E162T000 | STH 116 WB | 021E162T006 | 0.06 | 2.1088 | 2.0873 | 5 of 10 crashes remain after vetting. All five crashes are intersection specific. Four WB rear ends of left turning traffic. No left turn lane exists. One NB fail to yield to WB with visibility obstructed by a parked vehicle at the Jefferson intersection. | WB rear end crashes were impacted by having no left turn lane to turn south on STH 116/Jefferson St. or driveways. These four crashes resulted in one type $B$ suspected minor injury, one type C possible injury and two property damage only crashes. The right angle failure to yield crash had no geometric features influencing the crash. The crash resulted in a property damage only crash. | Developing a left turn lane on STH 21 WB at Jefferson or TWLTL could help address the two rear end crashes. This was determined to not be a feasible alternative. |
| 4285 | 021 162T006 | WEbSTER AVE | 021 162T017 | 0.11 |  |  |  |  |  |
| 4286 | 021 162T017 | MADISON AVE | 021E162T110 | 0.93 |  |  |  |  |  |
| 4287 | 021E162T110 | INDUSTRIAL DR | 021 1666000 | 1.06 |  |  |  |  |  |
| 4288 | 021 1166 000 | RIVERMOOR RD | $021 E 168000$ | 1.57 |  |  |  |  |  |
| 4289 | 021E168 000 | CTH FF | 021E169 000 | 1.02 |  | 1.4584 | 12 of the 22 crashes remain after vetting. Eight of the 12 crashes remaining crashes occurred at CTH FF intersection and are described in the intersections section below. Of the four remaining crashes in this segment, one occurred at Potratz Hill where WB vehicle was rear ended, one drifted left of centerline, and the remaining two were at Sand Pit Road. | For the ten crashes at CTH FF and Sand Pit Road, see the intersections section below. Of the two remaining crashes one drifted left of center and one was a WB rear end crash at Potratz Hill. These two crashes resulted in one type A suspected serious injury and one type B suspected minor injury. | Recommendations at CTH FF \& Sand Pit are listed in the inersections section below. Given only one crash at Potratz Hill, no safety mitigation recommended at this intersection. The project is expected to include centerline rumble strips to address the crash that drifted left of center. |
| 4290 | 021E169 000 | SAND PIT RD | 021E170K000 | 1.35 | 1.1763 | 1.7913 | 14 of 37 crashes remain after vetting. Nine of the remaining crashes occurred at the inersection of Sand Pit Road and the details are discussed in the intersections section below. The five remaining crashes all involve vehicles that drifted left of centerline | For the nine crashes at Sand Pit Road, see the intersections section below. For the five drifting left of center crashes, no geometric features seem to influence these crashes other than no centerline rumble strips are present. These five crashes resulted in one fatal crash, one suspected minor injury, and three property damage only crashes. | Recommendations at CTH FF \& Sand Pit are listed in the inersections section below. Centerline rumble stripes are expected to be included in the project to address these left of center crashes. |
| \|ntersections: Intersection Network Screening |  |  |  |  |  |  |  |  |  |
| INT_ID |  | ction Name X_NAME) | $\begin{aligned} & \text { LOSS } \\ & \text { (TOTAL) } \end{aligned}$ | PSI <br> (TOTAL) | $\begin{gathered} \text { LOSS } \\ \text { (KABC) } \end{gathered}$ | $\begin{gathered} \text { PSI } \\ \text { (KABC) } \end{gathered}$ | Summarize the contributing factors for ALL crashes in the flagged intersection. | Which geometric features contribute to the type and severity of the crashes? | Possible Countermeasures for Safety Mitigation Process |

FDM 11-38 Attachment 10.2 Safety Certification Worksheet

| \|X_70_02975 | STH 21 \& STH 116 | LOSS 4 | 3.97 | LOSS 4 | 0.84 | 5 of 8 crashes remain after vetting. Four WB rear ends of left turning traffic. No left turn lane exists. One NB fail to yield to WB with visibility obstructed by a parked vehicle. | WB rear end crashes were impacted by having no left turn lane to turn south on STH 116/Jefferson St. or driveways. These four crashes resulted in one type B suspected minor injury, one type C possible injury and two property damage only crashes. The right angle failure to yield crash had no geometric features influencing the crash. The crash resulted in a property damage only crash. | Developing a left turn lane on STH 21 WB at Jefferson or TWLTL could help address the two rear end crashes. This was determined to not be a feasible alternative. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \|X_70_02976 | STH 21 \& Webster Ave S | Loss 3 | 1.07 | Loss 2 | -0.39 |  |  |  |
| \|X_70_02977 | STH 21 \& Madison Ave | LOSS 4 | 2.39 | LOSS 3 | 0.02 | 1 of 7 crashes remain after vetting. A WB vehicle yielded to a pedestrian crossing North to South on the East side of the inersection. Another WB tried bypassing WB on right and struck the pedestrian. | Mainly a driver error by passing vehicle resulting in type B suspected minor injury. The width of the crossing is long with two travel lanes and two parking lanes. | Narrowing the STH 21 or creating bump-outs at the Madison Street intersection may have reduced the likehood of this collision. This was determined to not be a feasible alternative. |
| \|X_70_02978 | STH $21 \&$ Monroe St | LOSS 3 | 0.62 | LOSS 4 | 0.45 | 3 of 4 crashes remain after vetting. Two WB rear ends of left turns onto Monroe and one WB rear end turing into Kwik Trip. | WB rear end crashes were impacted by having no left turn lane to turn south on STH 116 to Monroe St. or driveways. These three crashes resulted in one type B suspected minor injury, and two property damage only crashes. | Developing a left turn lane on STH 21 WB at Monroe or TWLTL could help address the two rear end crashes. This was determined to not be a feasible alternative. |
| \|X_70_02980 | STH 21 \& Quincy Ave | LOSS 3 | 0.62 | LOSS 4 | 1.16 | 1 of 3 crashes remain after vetting. A WB rear end of left turning traffic into a driveway near Quincy Ave. | WB rear end crash was impacted by having no left turn lane. The crash resulted in a type C possible injury. | Developing a left turn lane on STH 21 WB at Quincy Ave. or TWLTL could help address the two rear end crashes. This was determined to not be a feasible alternative. |
| \|X_70_02981 | STH 21 \& Jackson Ave | Loss 3 | 1.25 | Loss 3 | 0.10 |  |  |  |
| 1X_70_02982 | STH $21 \& \mathrm{Van}$ Buren Ave | Loss 2 | -0.65 | Loss 2 | -0.25 |  |  |  |
| 1X_70_02985 | STH 21 \& Harrison Ave \& Maplewood Rd | Loss 2 | -2.68 | Loss 2 | -0.79 |  |  |  |
| \|X_70_03018 | STH 21 \& Maplewood Rd | Loss 2 | -0.65 | Loss 3 | 0.10 |  |  |  |
| \|X_70_03027 | STH 21 \& Omreau Ave | Loss 2 | -0.65 | Loss 3 | 0.10 |  |  |  |
| \|X_70_03026 | STH 21 \& McKinley Ave | LOSS 3 | 0.62 | LOSS 4 | 0.45 | 3 of 4 crashes remain after vetting. Three WB rear end crashes with left turns onto McKinley Ave. | The three WB rear end crashes were impacted by having no left turn lanes. The three crashes resulted in on type C possible injury and two property damage only crashes. | Developing a left turn lane on STH 21 at McKinley Ave. or TWLTL could help address the three rear end crashes. This was determined to not be a feasible alternative. |
| IX_70_03024 | STH 21 \& Beckwith Ave | Loss 3 | 0.62 | LOSS 4 | 0.45 | 0 of 4 crashes remain after vetting. | None | None |
| \|X_70_03023 | STH 21 \& Lincoln Ave | Loss 2 | -0.65 | Loss 2 | -0.25 |  |  |  |
| \|X_70_03028 | STH 21 \& Goldenrod Ave | Loss 2 | -1.43 | Loss 2 | -0.31 |  |  |  |
| \|X_70_03030 | STH 21 \& Industrial Dr | Loss 2 | -1.12 | Loss 3 | 0.43 |  |  |  |
| \|X_70_03034 | STH 21 \& Alder Ave \& Goldenrod Dr | LOSS 4 | 4.27 | LOSS 4 | 1.43 | 3 of ten crashes remain after vetting. Two EB rear end crashes while turning onto Goldenrod and on WB rear end crash while turning onto Alder Ave. | The three rear end crashes of left turning vehicles were impacted by having no left turn lanes. The three crashes resulted in property damage only. | Developing a left turn lane on STH 21 EB \& WB at Alder/Goldenrod or TWLTL could help address the three rear end crashes. This was determined to not be a feasible alternative. |
| 1X 70_03043 | STH 21 \& Brooke Dr \& Schwab Ave | Loss 3 | 0.10 | Loss 2 | -0.79 |  |  |  |
| \|X_70_02902 | STH 21 \& Rivermoor Rd (2) | Loss 4 | 2.84 | Loss 3 | 0.06 | 0 of 4 crashes remain after vetting. | None | None |
| 1X_70_02757 | STH $21 \&$ E Scott St | Loss 3 | 0.38 | Loss 3 | 0.14 |  |  |  |
| \|X_70_02649 | STH $21 \&$ CTH FF \& Reighmoor Rd | LOSS 4 | 3.21 | LOSS 4 | 3.76 | 9 of the 11 crashes remain after vetting. Six of the 9 involved left turning crashes from Hwy 21. One NB left failed to yield to a SB motorist. One SB failed to yield to WB. The remaining crash was not intersection related but the driver drifted off the roadway to the right. | The mainline left turning crashes are impacted by having no left turn lanes. NB failing to yield ot SB due to looking at crossing traffic. SB and WB crash due to picking an inadequate gap. The drift to the right due to inattentive driving. The nine crases resulted in one fatality, three type $B$ suspected minor injuries, four type $C$ possible injuries, and one property damage only. | Safety mitigation for these crashes could inlcude a roundabout, left turn lanes on STH 21 EB \& WB, and longitudinal shoulder rumble strips. |
| \|X_70_02655 | STH 21 \& Marquart Ln \& Potratz Hill Rd | Loss 3 | 0.24 | Loss 3 | 0.48 |  |  |  |
| \|X_70_02660 | STH 21 \& Sand Pit Rd | LOSS 4 | 9.04 | LOSS 4 | 4.10 | 11 of 11 crashes remain after vetting. Ten of the 11 crashes involve a left turning vehicle from Highway 21. The remaining crash was a NB failure to yield to an EB. | The mainline left turning crashes are impacted by having no left turn lanes. NB failing to yield to EB due to picking an inadequate gap. These crashes resulted in five type B suspected minor injuries, three type C possible injuries, and three property damage only crashes. | Safety mitigation for these crashes could inlcude a roundabout, left turn lanes on STH 21 EB \& WB, and longitudinal shoulder rumble strips. |

## ATTACHMENT E

## Safety Mitigation Certification Documentation

Layout/Schematic for each alternative and Cost Estimate for each alternative

Project ID: 6180-30-00
$\begin{array}{ll}\text { Title }: \text { Omro-Oshkosh } \\ \text { Region } & \text { : NORTHEAST }\end{array}$

Route : STH 021
Sub Title: STH 116 - Leonard Point
County : Winnebago

Improvement Type proposed RSRF10
MetaManager 9/2019
Year 1 ADT varies 10,590

## Year 20 ADT varies 10,590

HMA - would be 4MT58-28S based on FDM: 14-10 Attachment 10.3 WisDOT HMA Mixture Selection Process.

Existing roadway conditions:

- 25 MPH roadway
- 12-ft thru lanes with 9-ft parking lanes or 6-ft urban shoulders

Proposed TWLTL conditions:

- 25 MPH roadway
- 12-ft through lanes
- 16-ft TWLTL
- 6-ft Bike Lanes

The options presented were to compare an overlay of STH 21 to adding a TWLTL, however a TWLTL will not fit in the current roadway area. Widening the road to accommodate this option would require a massive real estate acquisition of downtown Omro. As such, no alternative will be presented for this section of roadway.

Project ID: 6180-30-00
STH 21
Created: 6/2/2020
Omro - Oshkosh
STH 116 - Leonard Point Rd
Winnebago County
STH 21 \& CTH FF/Reighmoor Rd Intersection
The intersection of STH 21 and CTH FF has an intersection safety flag. Two alternatives have been suggested to mitigate the crashes occurring they are slotted left turn lanes on STH 21 and a single lane roundabout. A construction cost estimate including estimated real estate costs have been created for the two alternatives and a do-nothing alternative cost estimate.


Existing roadway conditions and assumptions for project:

- STH 21 is on the community's plan for wider shoulders for bike accommodations
- $1 \frac{1}{4}$-Inch Base Aggregate Dense unit weight $=2$ Tons/ CY
- $3 / 4$-Inch Base Aggregate Dense unit weight $=2.1$ Tons/CY
- Fill expansion factor: 1.33
- STH 21 is a concrete roadway with no HMA overlay
- As-built 6184-03-71
- Traffic forecasting:
- Year 1 AADT: 11,090
- Year 20 AADT: 11,090
- The proposed Improvement Type is RSRF10
*NOTE - if this Do nothing alternative. is selected for the preferred alternative the CTH FF work would most likely stop at the radius and not extend down the road. Due to the nature of IHSDM and this process all alternatives need to have the same limits. All design assumptions need to be revisited in final design.


## Do Nothing Alternative (Option 1):

No Geometric modifications.
Limits on STH 21: 0+75 - STA 19+90. Mainline length 1915-ft.
Assumptions:

- $10 \%$ of the concrete will need to be repaired or replaced.
- 2-inch HMA of 4LT58-28S based on FDM: 14-10 Attachment 10.3 WisDOT HMA Mixture Selection Process.
- 5 -ft shoulders (widen from 3 -ft due to bike comp plan)
- No new BAD is needed for shoulders due to HMA widening. Using Shaping Shoulders to shape gravel section of shoulder. - Anticipated to be used project wide - therefore higher quantity for pices.

Limits on CTH FF: CTH FF from STA $22+58-32+44$. Sideroad lengths: $1020-\mathrm{ft}$
Assumptions:

- 2-inch HMA of 4LT58-28S based on FDM: 14-10 Attachment 10.3 WisDOT HMA Mixture Selection Process.
- Mill 2-inches -It is assumed this would be the only milling on the project.
- No new BAD for shoulders

Estimated cost:

| Item Number | Item Name | Unit | Quantity | Unit Price | Item Cost |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 305.0500 | Shaping Shoulders | STA | 18.8 | $\$ 50.00$ | $\$ 940$ |
| 416.1710 | Concrete Pavement Repair | SY | 315 | $\$ 80.00$ | $\$ 25,200$ |
| 416.1720 | Concrete Pavement <br> Replacement | SY | 315 | $\$ 90.00$ | $\$ 28,350$ |
| 455.0605 | Tack Coat | Gal | 510 | $\$ 5.00$ | $\$ 2,550$ |
| 204.0120 | Removing Asphaltic <br> Surface Milling | SY | 2,500 | $\$ 6.00$ | $\$ 15,000$ |
| 460.5224 | HMA Pavement 4LT 58-28S | Tons | 1,125 | $\$ 70.00$ | $\$ 78,750$ |
| 646.1020 | Marking Line Epoxy 4-Inch | LF | 2,775 | $\$ 1.00$ | $\$ 2,775$ |
| 646.1040 | Marking Line Grooved <br> Epoxy 4-inch | LF | 3,750 | $\$ 2.00$ | $\$ 7,500$ |
|  |  |  |  | Total | $\$ 161,665$ |
|  |  |  |  | Rounded | $\$ 170,000$ |

Items that are not included in the estimate:

- Traffic control items
- Mobilization
- Field office
- Incentive Items

These items are not included because they are depended on the entire project. To speculate the percentage of these items for this specific location would be very challenging and most-likely not accurate.

## Option 2 - Slotted Left Turn Lane

This option will add a slotted left turn lane with a 6 -ft positive offset along STH 21 . Based off traffic forecast, the left turn lane will be 300-ft. it will be assumed that the final pavement design along STH 21 will be 2inches of HMA over 9 -inches of concrete over 6 inches of base aggregate with 5 - ft shoulders. Outside of the intersection reconstruction limits, a 2 -inch mill and overlay will be applied to CTH FF road between $22+58-32+44$. It is assumed that all the concrete will be hand work on this project.

Limits on STH 21: 0+75 - STA 19+90. Mainline length 1915-ft.
Assumptions:

- 6-ft positive offset of left turn lanes
- 300-ft left turn lanes
- Pavement Structure: 2-inches HMA over 9-inches concrete over 6-inches of $1 \frac{1}{4}$-Inch BAD
- 2-inch HMA of 4LT58-28S based on FDM: 14-10 Attachment 10.3 WisDOT HMA Mixture Selection Process.
- 5-ft shoulders (widen from 3-ft due to bike comp plan) with 5-ft gravel shoulders

Limits on CTH FF: CTH FF from STA $22+58-32+44$. Sideroad lengths: $1020-\mathrm{ft}$
Assumptions:

- 5-inch HMA of 4LT58-28S based on FDM: 14-10 Attachment 10.3 WisDOT HMA Mixture Selection Process.
- Mill 2-inches
- No new BAD for shoulders

Estimated cost:

| Item Number | Item Name | Unit | Quantity | Unit Price | Item Cost |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 204.0100 | Removing Pavement | SY | 6,300 | $\$ 20.00$ | $\$ 126,000$ |
| 205.0100 | Excavation Common | CY | 5,000 | $\$ 12.00$ | $\$ 120,000$ |


| 208.0100 | Borrow | CY | 1200 | \$12.00 | \$14,400 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 305.0110 | Base Aggregate Dense $3 / 4$ Inch | Tons | 400 | \$22.00 | \$8,800 |
| 305.0120 | Base Aggregate Dense 1 114Inch | Tons | 3,125 | \$18.00 | \$56,250 |
| 415.0090 | Concrete Pavement 9-Inch | SY | 6,300 | \$55.00 | \$346,500 |
| 455.0605 | Tack Coat | Gal | 70 | \$5.00 | \$350 |
| 460.5224 | HMA Pavement 4MT 4828 S | Ton | 1,125 | \$70.00 | \$78,750 |
| 522.1018 | Apron Endwalls for Culvert Pipe Reinforced Concrete 18-Inch | Each | 2 | \$600 | \$1,200 |
| 601.0411 | Concrete Curb \& Gutter 30-Inch Type D | LF | 800 | \$30.00 | \$24,000 |
| 602.0410 | Concrete Sidewalk 5-Inch | SF | 2,400 | \$10.00 | \$24,000 |
| 608.0318 | Storm Sewer Culvert Pipe Reinforced Concrete Class III 18-Inch | LF | 60 | \$100 | \$6,000 |
| 611.1004 | Catch Basin 4-ft Diameter | Each | 2 | \$2,000 | \$4,000 |
| 625.0500 | Salvaged Topsoil | SY | 400 | \$4.00 | \$1,600 |
| 628.2004 | Erosion Mat Class I Type B | SY | 400 | \$1.50 | \$600 |
| 629.0210 | Fertilizer Type B | CWT | . 1 | \$250.00 | \$25 |
| 630.0120 | Seeding Mixture No. 20 | LBS | 10 | \$25.00 | \$250 |
| 646.1020 | Marking Line Epoxy 4-Inch | LF | 2,775 | \$1.00 | \$2,775 |
| 646.1040 | Marking Line Grooved Epoxy 4-inch | LF | 3,750 | \$2.00 | \$11,250 |
|  | FEE R/W (1 parcel) | Acres | . 2 | \$50,000 | \$10,000 |
|  | TLE R/W (1 parcel) | Acres | . 05 | \$10,000 | \$500 |
|  |  |  |  | Total | \$823,000 |
|  |  |  |  | Rounded | \$830,000 |

Items that are not included in the estimate:

- Traffic control items
- Mobilization
- Field office
- Incentive Items

These items are not included because they are depended on the entire project. To speculate the percentage of these items for this specific location would be very challenging and most-likely not accurate.

## Option 3 - Single Lane Roundabout

This option will reconstruct the intersection to a single lane roundabout. In final design the exact configuration will be completed.


Limits on STH 21: 0+75 - STA 19+90. Mainline length 1915-ft.
Assumptions:

- STA 4+77-16+09 will be reconstructed
- STA 0+75 - STA 19+90 -2-inch HMA of 4LT58-28S based on FDM: 14-10 Attachment 10.3 WisDOT HMA Mixture Selection Process.
- 5-ft paved shoulders, 5 -ft Gravel at full thickness
- Did not provide grading for Multi-use path
- Lighting lump sum was created by: poles, arms, pull box, Transformer Base, Luminaire LED lights, and Lighting Control Cabinet

Limits on CTH FF: CTH FF from STA 22+58-32+44. Sideroad lengths: 1020-ft
Assumptions:

- STA 22+58-32+44 be reconstructed
- Depth of HMA, 4LT58-28S based off recent As-built
- 3-ft gravel Shoulders

Estimated Costs: See above for some comments. - How come HMA was brought down to 65, less quantity than project above - I would suggest staying at 70 ?

| Item <br> Number | Item Name | Unit | Quantity | Unit Price | Item Cost |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 205.0100 | Excavation Common | CY | 10,000 | \$12.00 | \$120,000 |
| 305.0110 | Base Aggregate Dense $3 / 4$ Inch | Tons | 400 | \$22.00 | \$8,800 |
| 305.0120 | Base Aggregate Dense 1 ¼ -Inch | Tons | 3,700 | \$18.00 | \$66,600 |
| 415.0090 | Concrete Pavement 9-Inch | SY | 4,500 | \$55.00 | \$247,500 |
| 416.0512 | Concrete Truck Apron 12Inch | SY | 457 | \$60.00 | 27,420 |
| 460.5244 | HMA Pavement 4LT 58-28S | Tons | 750 | \$70.00 | \$52,500 |
| 522.1018 | Apron Endwalls for Culvert Pipe Reinforced Concrete 18-Inch | Each | 8 | \$600 | \$4,800 |
| 608.0318 | Storm Sewer Culvert Pipe Reinforced Concrete Class III 18-Inch | LF | 120 | \$100 | \$12,000 |
| 601.0411 | Concrete Curb \& Gutter 30-Inch Type D | LF | 4,562 | \$30.00 | \$136,860 |
| 602.0410 | Concrete Sidewalk 5-Inch (at splitter island crossings) | SF | 11,721 | \$10.00 | \$117,210 |
| 611.1004 | Catch Basin 4-ft Diameter | Each | 8 | \$2,000 | \$16,000 |
| 625.0500 | Salvaged Topsoil | SY | 5,000 | \$4.00 | \$20,000 |
| 628.2004 | Erosion Mat Class I Type B | SY | 5,000 | \$1.50 | \$7,500 |
| 629.0210 | Fertilizer Type B | CWT | . 5 | \$250.00 | \$125 |
| 630.0120 | Seeding Mixture No. 20 | LBS | 200 | \$25.00 | \$5,000 |
| 646.1020 | Marking Line Epoxy 4-Inch | LF | 2,775 | \$1.00 | \$2,775 |
| 646.1040 | Marking Line Grooved Epoxy 4-inch | LF | 3,750 | \$2.00 | \$7,500 |
| SPV. 0120.01 | Lighting Slump Sum | LS | 1 | \$65,000 | \$65,000 |
|  | FEE R/W (5 Parcels) | Acres | . 5 | \$50,000 | \$25,000 |
|  |  |  |  | Total | \$942,590 |
|  |  |  |  | Rounded | \$950,000 |

Items that are not included in the estimate:

- Traffic control items
- Mobilization
- Field office
- Incentive Items

These items are not included because they are depended on the entire project. To speculate the percentage of these items for this specific location would be very challenging and most-likely not accurate.

Project ID: 6180-30-00
STH 21
Created: 5/20/2020
Omro - Oshkosh
STH 116 - Leonard Point Rd
Winnebago County
STH 21 \& Sand Pit Rd Intersection

The intersection of STH 21 and Sand Pit Rd has an intersection safety flag. Two alternatives have been suggested to mitigate the crashes occurring they are slotted left turn lanes on STH 21 and a single lane roundabout. A construction cost estimate including estimated real estate costs have been created for the two alternatives and a do-nothing alternative cost estimate.


Existing roadway conditions and assumptions for project:

- STH 21 is on the community's plan for wider shoulders for bike accommodations
- $1 \frac{1}{4}$-Inch Base Aggregate Dense unit weight $=2$ Tons/ CY
- $3 / 4$-Inch Base Aggregate Dense unit weight = 2.1 Tons/CY
- Fill expansion factor: 1.33
- STH 21 is a concrete roadway with no HMA overlay
o As-built 6184-03-71
- Traffic forecasting:
- Year 1 AADT: 11,090
- Year 20 AADT: 11,090
- The proposed Improvement Type is RSRF10
*NOTE - if this Do nothing alternative. is selected for the preferred alternative the CTH FF work would most likely stop at the radius and not extend down the road. Due to the nature of IHSDM and this process all alternatives need to have the same limits. All design assumptions need to be revisited in final design.


## Do Nothing Alternative (Option 1):

No Geometric modifications.
Limits on STH 21: 54+32 - STA 73+11. Mainline length 1879-ft.
Assumptions:

- $10 \%$ of the concrete will need to be repaired or replaced.
- 2-inch HMA of 4LT58-28S based on FDM: 14-10 Attachment 10.3 WisDOT HMA Mixture Selection Process.
- 5 -ft shoulders (widen from 3 -ft due to bike comp plan)
- No new BAD is needed for shoulders due to HMA widening. Using Shaping Shoulders to shape gravel section of shoulder.

Limits on CTH FF: STA 0+00-10+20. Sideroad lengths: 1020-ft
Assumptions:

- 2-inch HMA of 4LT58-28S based on FDM: 14-10 Attachment 10.3 WisDOT HMA Mixture Selection Process.
- Mill 2-inches
- No new BAD for shoulders

Estimated cost:

| Item Number | Item Name | Unit | Quantity | Unit Price | Item Cost |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 305.0500 | Shaping Shoulders | STA | 18.8 | $\$ 50.00$ | $\$ 940$ |
| 416.1710 | Concrete Pavement Repair | SY | 315 | $\$ 80.00$ | $\$ 25,200$ |
| 416.1720 | Concrete Pavement <br> Replacement | SY | 315 | $\$ 90.00$ | $\$ 28,350$ |
| 455.0605 | Tack Coat | Gal | 510 | $\$ 5.00$ | $\$ 2,550$ |
| 204.0120 | Removing Asphaltic <br> Surface Milling | SY | 2500 | $\$ 6.00$ | $\$ 15,000$ |
| 460.5224 | HMA Pavement 4LT 58-28S | Tons | 1,125 | $\$ 70.00$ | $\$ 78,750$ |
| 646.1020 | Marking Line Epoxy 4-Inch | LF | 2,775 | $\$ 1.00$ | $\$ 2,775$ |
| 646.1040 | Marking Line Grooved <br> Epoxy 4-inch | LF | 3,750 | $\$ 2.00$ | $\$ 7,500$ |
|  |  |  |  | Total | $\$ 161,065$ |
|  |  |  |  | Rounded | $\$ 170,000$ |

Items that are not included in the estimate:

- Traffic control items
- Mobilization
- Field office
- Incentive Items

These items are not included because they are depended on the entire project. To speculate the percentage of these items for this specific location would be very challenging and most-likely not accurate.

Option 2 - Slotted Left Turn Lane


This option will add a slotted left turn lane with a 6 - ft positive offset along STH 21. Based off traffic forecast, the left turn lane will be 300 -ft. it will be assumed that the final pavement design along STH 21 will be 2 inches of HMA over 9 -inches of concrete over 6 inches of base aggregate with 5 - ft shoulders. Outside of the intersection reconstruction limits, a 2-inch mill and overlay will be applied to CTH FF road between $0+00-10+20$. It is assumed that all the concrete will be hand work on this project.

Limits on STH 21: 54+32 - STA 73+11. Mainline length 1879-ft.
Assumptions:

- 6-ft positive offset of left turn lanes
- 300 -ft left turn lanes
- Pavement Structure: 2 -inches HMA over 9 -inches concrete over 6 -inches of $1 \frac{1}{4}$-Inch BAD
- 2-inch HMA of 4LT58-28S based on FDM: 14-10 Attachment 10.3 WisDOT HMA Mixture Selection Process.
- 5 -ft shoulders (widen from 3 -ft due to bike comp plan) with 5 -ft Gravel shoulders
- Limits on CTH FF: STA 0+00-10+20. Sideroad lengths: 1020-ft

Assumptions:

- 5-inch HMA of 4LT58-28S based on FDM: 14-10 Attachment 10.3 WisDOT HMA Mixture Selection Process.
- 2-inch over lay limits
- Mill 2-inches
- No new BAD for shoulders

Estimated cost:

| Item Number | Item Name | Unit | Quantity | Unit Price | Item Cost |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 204.0100 | Removing Pavement | SY | 6,300 | \$20.00 | \$126,000 |
| 205.0100 | Excavation Common | CY | 500 | \$12.00 | \$6,000 |
| 208.0100 | Borrow | CY | 1200 | \$12.00 | \$14,400 |
| 305.0120 | Base Aggregate Dense $11 / 4$ Inch | Tons | 3,125 | \$18.00 | \$56,250 |
| 415.0090 | Concrete Pavement 9-Inch | SY | 6,300 | \$55.00 | \$346,500 |
| 455.0605 | Tack Coat | Gal | 70 | \$5.00 | \$350 |
| 460.5224 | HMA Pavement 4MT 48- 28 S | Ton | 1,125 | \$70.00 | \$78,750 |
| 522.1018 | Apron Endwalls for Culvert Pipe Reinforced Concrete 18-Inch | Each | 2 | \$600 | \$1,200 |
| 601.0411 | Concrete Curb \& Gutter 30-Inch Type D | LF | 800 | \$30.00 | \$24,000 |
| 602.0410 | Concrete Sidewalk 5-Inch (at splitter island crossings) | SF | 2,400 | \$10.00 | \$24,000 |
| 608.0318 | Storm Sewer Culvert Pipe Reinforced Concrete Class III 18-Inch | LF | 60 | \$100 | \$6,000 |
| 611.1004 | Catch Basin 4-ft Diameter | Each | 2 | \$2,000 | \$4,000 |
| 625.0500 | Salvaged Topsoil | SY | 400 | \$4.00 | \$1,600 |
| 628.2004 | Erosion Mat Class I Type B | SY | 400 | \$1.50 | \$600 |
| 629.0210 | Fertilizer Type B | CWT | . 1 | \$250.00 | \$25 |
| 630.0120 | Seeding Mixture No. 20 | LBS | 10 | \$25.00 | \$250 |
| 646.1020 | Marking Line Epoxy 4-Inch | LF | 2,775 | \$1.00 | \$2,775 |
| 646.1040 | Marking Line Grooved Epoxy 4-inch | LF | 3,750 | \$2.00 | \$7,500 |
|  | FEE R/W | Acres | . 2 | \$50,000 | \$10,000 |
|  | TLE R/W | Acres | . 05 | \$10,000 | \$500 |
|  |  |  |  | Total | \$710,700 |
|  |  |  |  | Rounded | \$720,000 |

Items that are not included in the estimate:

- Traffic control items
- Mobilization
- Field office
- Incentive Items

These items are not included because they are depended on the entire project. To speculate the percentage of these items for this specific location would be very challenging and most-likely not accurate.

## Option 3 - Single Lane Roundabout

This option will reconstruct the intersection to a single lane roundabout. In final design the exact configuration will be completed.


Limits on STH 21: 54+32 - STA 73+11. Mainline length 1879-ft. Assumptions:

- STA 58+32-69+68. will be reconstructed - based off previous As-built depths
- STA 54+32 - STA 73+11 -2-inch HMA of 4LT58-28S based on FDM: 14-10 Attachment 10.3 WisDOT HMA Mixture Selection Process.
- 5-ft paved shoulders, 5 -ft Gravel at full thickness
- Did not provide grading for Multi-use path
- Lighting lump sum was created by: poles, arms, pull box, Transformer Base, Luminaire LED lights, and Lighting Control Cabinet

Limits on CTH FF: STA $0+00-10+20$. Sideroad lengths: 1020-ft Assumptions:

- STA 22+58-32+44 be reconstructed
- Depth of HMA, 4LT58-28S based on previous as-built
- 3-ft gravel shoulders

| Item Number | Item Name | Unit | Quantity | Unit Price | Item Cost |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 205.0100 | Excavation Common | CY | 6,200 | \$12.00 | \$74,400 |
| 305.0110 | Base Aggregate Dense $3 / 4$ Inch | Tons | 400 | \$22.00 | \$8,800 |
| 305.0120 | Base Aggregate Dense 1 1⁄4 -Inch | Tons | 3,700 | \$18.00 | \$66,600 |
| 415.0090 | Concrete Pavement 9-Inch | SY | 4,500 | \$55.00 | \$247,500 |
| 416.0512 | Concrete Truck Apron 12Inch | SY | 457 | \$60.00 | 27,420 |
| 460.5244 | HMA Pavement 4LT 58-28S | Tons | 750 | \$70.00 | \$52,500 |
| 522.1018 | Apron Endwalls for Culvert Pipe Reinforced Concrete 18-Inch | Each | 8 | \$600 | \$4,800 |
| 608.0318 | Storm Sewer Culvert Pipe Reinforced Concrete Class III 18-Inch | LF | 120 | \$100 | \$12,000 |
| 601.0411 | Concrete Curb \& Gutter 30-Inch Type D | LF | 4,562 | \$30.00 | \$136,860 |
| 602.0410 | Concrete Sidewalk 5-Inch | SF | 11,721 | \$10.00 | \$117,210 |
| 611.1004 | Catch Basin 4-ft Diameter | Each | 8 | \$2,000 | \$16,000 |
| 625.0500 | Salvaged Topsoil | SY | 5,000 | \$4.00 | \$20,000 |
| 628.2004 | Erosion Mat Class I Type B | SY | 5,000 | \$1.50 | \$7,500 |
| 629.0210 | Fertilizer Type B | CWT | . 5 | \$250.00 | \$125 |
| 630.0120 | Seeding Mixture No. 20 | LBS | 200 | \$25.00 | \$5,000 |
| SPV.0120.01 | Lighting Slump Sum | LS | 1 | \$65,000 | \$65,000 |
|  | FEE R/W | Acres | . 5 | \$50,000 | \$25,000 |
|  |  |  |  | Total | \$886,715 |
|  |  |  |  | Rounded | \$900,000 |

Items that are not included in the estimate:

- Traffic control items
- Mobilization
- Field office
- Incentive Items

These items are not included because they are depended on the entire project. To speculate the percentage of these items for this specific location would be very challenging and most-likely not accurate.

## ATTACHMENT E

## Safety Mitigation Certification Documentation

IHSDM Crash Prediction Evaluation Report for each alternative

# Interactive Highway Safety Design Model 

# Crash Prediction Evaluation Report 

STH 21 \& CTH FF Overlay \& Concrete Repair Base Case

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## Report Overview

## Report Generated: Aug 6, 2020 9:10 AM

Report Template: System: Multi-Page, 508 Compliant [System] (sscpm4, Jan 20, 2020 2:20 PM)

Evaluation Date: Thu Aug 06 09:00:20 CDT 2020
IHSDM Version: v15.0.0 (Oct 31, 2019)
Site Set Crash Prediction Module: $v \mid$ ModuleInfo.moduleVersion| (|ModuleInfo.moduleDate|)

User Name: Scott Nelson
Organization Name: WisDOT NE Region
Phone: 920.366.2109
E-Mail: scott.nelson@dot.wi.gov

Project Title: 6180-30-00, STH 21 from STH 116 to Leonard Point
Project Comment: Created Wed Jul 01 13:40:49 CDT 2020
Project Unit System: U.S. Customary

Site Set: CTH FF Intersection Overlay \& Concrete Repair
Site Set Comment: Created Wed Jul 01 13:41:29 CDT 2020
Site Set Version: v3

Evaluation Title: CTH FF Predicted Crashes Overlay \& Concrete Repair
Evaluation Comment: Created Thu Aug 06 08:59:07 CDT 2020
Policy for Superelevation: AASHTO 2011 U.S. Customary
Calibration: WisDOT Calibration_v15-0
Crash Distribution: WisDOT Distributions_v15-0
Model/CMF: WisDOT Models_v15-0
Note: A Model Data Set other than the HSM (Highway Safety Manual) Configuration was selected for this Evaluation. If Crash Modification Factors (CMFs) were modified, then the results will not be in accordance with the HSM (see HSM Appendix to Part C, section A.1.3).
First Year of Analysis: 2027
Last Year of Analysis: 2036
Empirical-Bayes Analysis: None

## Disclaimer Regarding Crash Prediction Method

## IMPORTANT NOTICE ABOUT COMPARING RESULTS FROM HIGHWAY SAFETY MANUAL FIRST EDITION (2010) MODELS TO RESULTS FROM NEW MODELS DEVELOPED UNDER NCHRP PROJECTS 17-70 AND 17-58

Since the publication of the Highway Safety Manual - First Edition (HSM-1), in 2010 by the American Association of State

Highway and Transportation Officials (AASHTO), multiple research efforts have been undertaken through the National Cooperative Highway Research Program (NCHRP) to develop safety performance models for road segment and intersection facility types that were not initially reflected in the HSM-1, in order to expand the breadth and depth of the HSM in the future.

The IHSDM Crash Prediction Module (CPM) is intended as a faithful implementation of HSM Part C predictive methods. As NCHRP projects to develop new predictive methods for the HSM are completed, FHWA works to incorporate the new methods into IHSDM, sometimes in advance of publication in the HSM. The following new crash predictive methods have been accepted by NCHRP project panels and incorporated into IHSDM, while pending AASHTO's approval for incorporation into a future edition of the HSM:

- Roundabouts: completed in 2018 under NCHRP Project 17-70, the new methods will provide improved outcomes for the safety analysis of roundabouts.
- 6+ lane and one-way urban/suburban arterials (including models for segments and intersections): completed under NCHRP Project 17-58.

However, in the absence of local calibration factors (see HSM-1 Part C, Appendix A for guidance on calibration of the predictive models), it is neither appropriate nor advisable to directly compare the results from new models (from NCHRP Projects 17-58 and 17-70) to results from HSM-1 models, as the models were not calibrated to the same base state data sets, and consequently can produce unexpected results. If local calibration factors are available and applied to both new models and HSM- 1 models, then it may be appropriate to directly compare the results.[Note: Work being performed under NCHRP Project 17-72 (Update of Crash Modification Factors for the Highway Safety Manual) is expected to re-calibrate many of the old (HSM-1) and new (e.g., NCHRP 17-70) models to data from a single (or small number of) states, that would allow results from all models to be directly compared.]

The models produced for NCHRP Project 17-70 have independent value in terms of informing the design of a roundabout and assessing the effects of different design characteristics on the expected safety performance of a roundabout.

The HSM-1 interim method previously included in IHSDM for evaluating roundabouts on urban/suburban arterials (i.e., evaluating an existing intersection and then applying a Crash Modification Factor for replacing the existing intersection with a roundabout) has been deactivated in IHSDM, to minimize any confusion with the new roundabout methodology.

## Section Types

## Rural Two Lane Site Set CPM Evaluation

Site Type<br>Type: 4ST<br>Calibration Factor: 1

Table 1. Evaluation and Crash Data (CSD) (if applicable) Intersection Sites

| Site No. | Type | Highway | Site Description | Major AADT | Minor AADT | $\begin{array}{\|c\|} \hline \text { Number of } \\ \text { Approaches with Left- } \\ \text { Turn Lanes } \\ \hline \end{array}$ | Number of Approaches with Right-Turn Lanes Right-Turn Lane | Skew Angle 1 (deg) | $\begin{array}{\|c} \text { Skew Angle } \\ \text { ( } \text { (deg) } \end{array}$ | Presence of Lighting |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4ST | $\begin{aligned} & \mathrm{STH} 21 \& \mathrm{CTH} \\ & \mathrm{FF} \end{aligned}$ | Overlay \& Concrete Repair | $\begin{aligned} & \text { 2027-2036: } \\ & 11090 \end{aligned}$ | $2027: 2118 ; 2028: 2133 ; 2029: 2148 ; 2030: 2162 ; 2031: 2177 ;$ 2032: 2192; 2033: 2207; 2034: 2222; 2035: 2237; 2036; 2251 | 0 | 2 | 0.0000 | 0.0000 | no |

Table 2. Predicted Crash Frequencies and Rates by Site

| Site <br> No. | Type | Highway | Site Description | Total Predicted Crashes for Evaluation Period | Predicted Total Crash Frequency (crashes/yr) | Predicted FI <br> Crash <br> Frequency <br> (crashes/yr) | Predicted PDO Crash Frequency (crashes/yr) | Predicted Intersection Travel Crash Rate (crashes/million veh) | Intersection Crash Rate (crashes/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4ST | STH 21 \& CTH FF | Overlay \& Concrete Repair | 18.976 | 1.8975 | 0.5806 | 1.3169 | 0.39 | 1.8975 |
|  |  | Total | Total | 18.976 | 1.8975 | 0.5806 | 1.3169 | 0.39 | 1.8975 |

Table 3. Predicted Crash Frequencies by Year (4ST)

| Year | Total Crashes | FI Crashes | Percent FI (\%) | PDO Crashes | Percent PDO (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2027 | 1.86 | 0.57 | 30.600 | 1.29 | 69.400 |
| 2028 | 1.87 | 0.57 | 30.600 | 1.30 | 69.400 |
| 2029 | 1.88 | 0.57 | 30.600 | 1.30 | 69.400 |
| 2030 | 1.89 | 0.58 | 30.600 | 1.31 | 69.400 |
| 2031 | 1.89 | 0.58 | 30.600 | 1.31 | 69.400 |
| 2032 | 1.90 | 0.58 | 30.600 | 1.32 | 69.400 |
| 2033 | 1.91 | 0.58 | 30.600 | 1.32 | 69.400 |
| 2034 | 1.92 | 0.59 | 30.600 | 1.33 | 69.400 |
| 2035 | 1.93 | 0.59 | 30.600 | 1.34 | 69.400 |
| 2036 | 1.93 | 0.59 | 30.600 | 1.34 | 69.400 |
| Total | 18.98 | 5.81 | 30.600 | 13.17 | 69.400 |
| Average | 1.90 | 0.58 | 30.600 | 1.32 | 69.400 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

## Table 4. Predicted 4ST Crash Type Distribution

| Element Type | Crash Type | FI <br> Crashes | Percent <br> FI (\%) | PDO <br> Crashes | $\begin{aligned} & \text { Percent } \\ & \text { PDO (\%) } \end{aligned}$ | Total Crashes | Percent <br> Total (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Collision with Animal | 0.06 | 0.3 | 3.35 | 17.6 | 3.41 | 18.0 |
| Intersection | Collision with Bicycle | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Other Single-vehicle Collision | 1.19 | 6.2 | 2.84 | 15.0 | 4.03 | 21.2 |
| Intersection | Overturned | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Collision with Pedestrian | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Run Off Road | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Total Single Vehicle Crashes | 1.25 | 6.6 | 6.19 | 32.6 | 7.44 | 39.2 |
| Intersection | Angle Collision | 2.66 | 14.0 | 2.83 | 14.9 | 5.48 | 28.9 |
| Intersection | Head-on Collision | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Other Multiple-vehicle Collision | 0.22 | 1.1 | 0.28 | 1.5 | 0.49 | 2.6 |
| Intersection | Rear-end Collision | 1.25 | 6.6 | 2.28 | 12.0 | 3.53 | 18.6 |
| Intersection | Sideswipe | 0.44 | 2.3 | 1.59 | 8.4 | 2.03 | 10.7 |
| Intersection | Total Multiple Vehicle Crashes | 4.56 | 24.0 | 6.98 | 36.8 | 11.54 | 60.8 |
| Intersection | Total Intersection Crashes | 5.80 | 30.6 | 13.16 | 69.4 | 18.98 | 100.0 |
|  | Total Crashes | 5.80 | 30.6 | 13.16 | 69.4 | 18.98 | 100.0 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

# Interactive Highway Safety Design Model 

# Crash Prediction Evaluation Report 

STH 21 \& CTH FF Mainline Left Turn Lanes

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## Report Overview

## Report Generated: Aug 6, 2020 9:13 AM

Report Template: System: Multi-Page, 508 Compliant [System] (sscpm4, Jan 20, 2020 2:20 PM)

Evaluation Date: Thu Aug 06 09:01:13 CDT 2020
IHSDM Version: v15.0.0 (Oct 31, 2019)
Site Set Crash Prediction Module: $v \mid$ ModuleInfo.moduleVersion| (|ModuleInfo.moduleDate|)

User Name: Scott Nelson
Organization Name: WisDOT NE Region
Phone: 920.366.2109
E-Mail: scott.nelson@dot.wi.gov

Project Title: 6180-30-00, STH 21 from STH 116 to Leonard Point
Project Comment: Created Wed Jul 01 13:40:49 CDT 2020
Project Unit System: U.S. Customary

Site Set: CTH FF Intersection with STH 21 Left Turn Lanes
Site Set Comment: Copied from CTH FF Intersection Overlay \& Concrete Repair (v3)
Site Set Version: v4

Evaluation Title: CTH FF Predicted Crashes Left Turn Lanes
Evaluation Comment: Created Thu Aug 06 09:00:49 CDT 2020
Policy for Superelevation: AASHTO 2011 U.S. Customary
Calibration: WisDOT Calibration_v15-0
Crash Distribution: WisDOT Distributions_v15-0
Model/CMF: WisDOT Models_v15-0
Note: A Model Data Set other than the HSM (Highway Safety Manual) Configuration was selected for this Evaluation. If Crash Modification Factors (CMFs) were modified, then the results will not be in accordance with the HSM (see HSM Appendix to Part C, section A.1.3).
First Year of Analysis: 2027
Last Year of Analysis: 2036
Empirical-Bayes Analysis: None

## Disclaimer Regarding Crash Prediction Method

## IMPORTANT NOTICE ABOUT COMPARING RESULTS FROM HIGHWAY SAFETY MANUAL FIRST EDITION (2010) MODELS TO RESULTS FROM NEW MODELS DEVELOPED UNDER NCHRP PROJECTS 17-70 AND 17-58

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Highway and Transportation Officials (AASHTO), multiple research efforts have been undertaken through the National Cooperative Highway Research Program (NCHRP) to develop safety performance models for road segment and intersection facility types that were not initially reflected in the HSM-1, in order to expand the breadth and depth of the HSM in the future.

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- Roundabouts: completed in 2018 under NCHRP Project 17-70, the new methods will provide improved outcomes for the safety analysis of roundabouts.
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However, in the absence of local calibration factors (see HSM-1 Part C, Appendix A for guidance on calibration of the predictive models), it is neither appropriate nor advisable to directly compare the results from new models (from NCHRP Projects 17-58 and 17-70) to results from HSM-1 models, as the models were not calibrated to the same base state data sets, and consequently can produce unexpected results. If local calibration factors are available and applied to both new models and HSM- 1 models, then it may be appropriate to directly compare the results.[Note: Work being performed under NCHRP Project 17-72 (Update of Crash Modification Factors for the Highway Safety Manual) is expected to re-calibrate many of the old (HSM-1) and new (e.g., NCHRP 17-70) models to data from a single (or small number of) states, that would allow results from all models to be directly compared.]

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The HSM-1 interim method previously included in IHSDM for evaluating roundabouts on urban/suburban arterials (i.e., evaluating an existing intersection and then applying a Crash Modification Factor for replacing the existing intersection with a roundabout) has been deactivated in IHSDM, to minimize any confusion with the new roundabout methodology.

## Section Types

## Rural Two Lane Site Set CPM Evaluation

Site Type<br>Type: 4ST<br>Calibration Factor: 1

Table 1. Evaluation and Crash Data (CSD) (if applicable) Intersection Sites

| Site No. | Type | Highway | Site Description | Major AADT | Minor AADT | $\begin{array}{\|c\|} \hline \text { Number of } \\ \text { Approaches with Left- } \\ \text { Turn Lanes } \\ \hline \end{array}$ | Number of Approaches with Right-Turn Lanes Right-Turn Lane | Skew Angle 1 (deg) | $\begin{array}{\|c} \text { Skew Angle } \\ \text { ( } \text { (deg) } \end{array}$ | Presence of Lighting |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4ST | $\begin{aligned} & \mathrm{STH} 21 \& \mathrm{CTH} \\ & \mathrm{FF} \end{aligned}$ | Overlay \& Concrete Repair | $\begin{aligned} & \text { 2027-2036: } \\ & 11090 \end{aligned}$ | $2027: 2118 ; 2028: 2133 ; 2029: 2148 ; 2030: 2162 ; 2031: 2177 ;$ 2032: 2192; 2033: 2207; 2034: 2222; 2035: 2237; 2036; 2251 | 2 | 2 | 0.0000 | 0.0000 | no |

Table 2. Predicted Crash Frequencies and Rates by Site

| Site <br> No. | Type | Highway | Site Description | Total Predicted Crashes for Evaluation Period | Predicted Total Crash Frequency (crashes/yr) | Predicted FI <br> Crash <br> Frequency <br> (crashes/yr) | Predicted PDO Crash Frequency (crashes/yr) | Predicted Intersection Travel Crash Rate (crashes/million veh) | Intersection Crash Rate (crashes/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4ST | STH 21 \& CTH FF | Overlay \& Concrete Repair | 9.867 | 0.9867 | 0.3019 | 0.6848 | 0.20 | 0.9867 |
|  |  | Total | Total | 9.867 | 0.9867 | 0.3019 | 0.6848 | 0.20 | 0.9867 |

Table 3. Predicted Crash Frequencies by Year (4ST)

| Year | Total Crashes | FI Crashes | Percent FI (\%) | PDO Crashes | Percent PDO (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2027 | 0.97 | 0.30 | 30.600 | 0.67 | 69.400 |
| 2028 | 0.97 | 0.30 | 30.600 | 0.68 | 69.400 |
| 2029 | 0.98 | 0.30 | 30.600 | 0.68 | 69.400 |
| 2030 | 0.98 | 0.30 | 30.600 | 0.68 | 69.400 |
| 2031 | 0.98 | 0.30 | 30.600 | 0.68 | 69.400 |
| 2032 | 0.99 | 0.30 | 30.600 | 0.69 | 69.400 |
| 2033 | 0.99 | 0.30 | 30.600 | 0.69 | 69.400 |
| 2034 | 1.00 | 0.30 | 30.600 | 0.69 | 69.400 |
| 2035 | 1.00 | 0.31 | 30.600 | 0.69 | 69.400 |
| 2036 | 1.00 | 0.31 | 30.600 | 0.70 | 69.400 |
| Total | 9.87 | 3.02 | 30.600 | 6.85 | 69.400 |
| Average | 0.99 | 0.30 | 30.600 | 0.69 | 69.400 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

## Table 4. Predicted 4ST Crash Type Distribution

| Element Type | Crash Type | FI <br> Crashes | Percent <br> FI (\%) | PDO <br> Crashes | Percent <br> PDO (\%) | Total <br> Crashes | Percent <br> Total (\%) |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Intersection | Collision with Animal | 0.03 | 0.3 | 1.74 | 17.6 | 1.77 | 18.0 |
| Intersection | Collision with Bicycle | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Other Single-vehicle Collision | 0.62 | 6.2 | 1.48 | 15.0 | 2.10 | 21.2 |
| Intersection | Overturned | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Collision with Pedestrian | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Run Off Road | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Total Single Vehicle Crashes | 0.65 | 6.6 | 3.22 | 32.6 | 3.87 | 39.2 |
| Intersection | Angle Collision | 1.38 | 14.0 | 1.47 | 14.9 | 2.85 | 28.9 |
| Intersection | Head-on Collision | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Other Multiple-vehicle Collision | 0.11 | 1.1 | 0.14 | 1.5 | 0.26 | 2.6 |
| Intersection | Rear-end Collision | 0.65 | 6.6 | 1.19 | 12.0 | 1.83 | 18.6 |
| Intersection | Sideswipe | 0.23 | 2.3 | 0.83 | 8.4 | 1.06 | 10.7 |
| Intersection | Total Multiple Vehicle Crashes | 2.37 | 24.0 | 3.63 | 36.8 | 6.00 | 60.8 |
| Intersection | Total Intersection Crashes | 3.02 | 30.6 | 6.85 | 69.4 | 9.87 | 100.0 |
|  | 3.02 | 30.6 | 6.85 | 69.4 | 9.87 | 100.0 |  |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

Interactive Highway Safety Design Model

## Crash Prediction Evaluation Report

STH 21 \& CTH FF<br>Roundabout Alternative

## Disclaimer

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## Report Overview

## Report Generated: Aug 6, 2020 9:14 AM

Report Template: System: Multi-Page, 508 Compliant [System] (sscpm4, Jan 20, 2020 2:20 PM)

Evaluation Date: Thu Aug 06 09:01:52 CDT 2020
IHSDM Version: v15.0.0 (Oct 31, 2019)
Site Set Crash Prediction Module: $v \mid$ ModuleInfo.moduleVersion| (|ModuleInfo.moduleDate|)

User Name: Scott Nelson
Organization Name: WisDOT NE Region
Phone: 920.366.2109
E-Mail: scott.nelson@dot.wi.gov

Project Title: 6180-30-00, STH 21 from STH 116 to Leonard Point
Project Comment: Created Wed Jul 01 13:40:49 CDT 2020
Project Unit System: U.S. Customary

Site Set: CTH FF Intersection Single Lane Roundabout
Site Set Comment: Created Wed Jul 01 14:00:43 CDT 2020
Site Set Version: v2

Evaluation Title: CTH FF Crash Prediction Roundabout
Evaluation Comment: Created Thu Aug 06 09:01:29 CDT 2020
Policy for Superelevation: AASHTO 2011 U.S. Customary
Calibration: WisDOT Calibration_v15-0
Crash Distribution: WisDOT Distributions_v15-0
Model/CMF: WisDOT Models_v15-0
Note: A Model Data Set other than the HSM (Highway Safety Manual) Configuration was selected for this Evaluation. If Crash Modification Factors (CMFs) were modified, then the results will not be in accordance with the HSM (see HSM Appendix to Part C, section A.1.3).
First Year of Analysis: 2027
Last Year of Analysis: 2036
Empirical-Bayes Analysis: None

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## Section Types

## Roundabout Site Set CPM Evaluation

## Site Type

Type: Roundabout RTL 41R
Calibration Factor: RTL 41R $=1.0$

Table 1. Evaluation and Crash Data (CSD) (if applicable) Roundabout - Homogeneous Sites

| Site No. | Type | Roundabout | Area Type | Entering AADT |
| :---: | :---: | :---: | :---: | :--- |
|  | 1 | 41R-Roundabout with 4 legs and a single circulating lane | STH $21 \&$ CTH FF | Rural |

Table 2. Predicted Crash Frequencies and Rates by Site

| Site No. | Type | Roundabout | Site Description | Total Predicted Crashes for Evaluation Period | Predicted Total <br> Crash <br> Frequency (crashes/yr) | Predicted FI Crash Frequency (crashes/yr) | Predicted PDO <br> Crash <br> Frequency <br> (crashes/yr) | Predicted Intersection Travel Crash Rate (crashes/million veh) | Intersection Crash Rate (crashes/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 41R - Roundabout with 4 legs and a single circulating lane | STH 21 \& CTH FF |  | 18.011 | 1.8011 | 0.2360 | 1.5651 | 0.81 | 1.8011 |
|  |  | Total | Total | 18.011 | 1.8011 | 0.2360 | 1.5651 | 0.81 | 1.8011 |

Table 3. Predicted Crash Frequencies by Year (Roundabout RTL 41R)

| Year | Total Crashes | FI Crashes | Percent FI (\%) | PDO Crashes | Percent PDO (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2027 | 1.80 | 0.23 | 13.097 | 1.56 | 86.903 |
| 2028 | 1.80 | 0.24 | 13.098 | 1.56 | 86.901 |
| 2029 | 1.80 | 0.24 | 13.100 | 1.56 | 86.900 |
| 2030 | 1.80 | 0.24 | 13.101 | 1.56 | 86.898 |
| 2031 | 1.80 | 0.24 | 13.103 | 1.56 | 86.897 |
| 2032 | 1.80 | 0.24 | 13.104 | 1.56 | 86.895 |
| 2033 | 1.80 | 0.24 | 13.106 | 1.57 | 86.894 |
| 2034 | 1.80 | 0.24 | 13.107 | 1.57 | 86.893 |
| 2035 | 1.80 | 0.24 | 13.109 | 1.57 | 86.891 |
| 2036 | 1.80 | 0.24 | 13.110 | 1.57 | 86.890 |
| Total | 18.01 | 2.36 | 13.104 | 15.65 | 86.896 |
| Average | 1.80 | 0.24 | 13.104 | 1.56 | 86.896 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

Table 4. Predicted Roundabout RTL 41R Crash Severity

| Site No. | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating Injury <br> (B) Crashes (crashes) | Possible Injury <br> (C) Crashes <br> (crashes) | No Injury <br> (O) Crashes <br> (crashes) |
| ---: | :---: | ---: | ---: | ---: | ---: |
| 1 | 0.0178 | 0.1766 | 1.1362 | 1.0295 | 15.6510 |
| Total | 0.0178 | 0.1766 | 1.1362 | 1.0295 | 15.6510 |

Table 5. Predicted Roundabout RTL 41R Crash Type Distribution

| Element Type | Crash Type | FI <br> Crashes | Percent <br> FI (\%) | PDO <br> Crashes | Percent <br> PDO <br> $(\%)$ | Total <br> Crashes |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Potal (\%) |  |  |  |  |  |  |$|$| Percent |  |
| ---: | :--- |
| Intersection | Collision with Animal |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

# Interactive Highway Safety Design Model 

# Crash Prediction Evaluation Report 

STH 21 \& Sand Pit Road<br>Overlay \& Concrete Repair Base Case

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## Report Overview

## Report Generated: Aug 6, 2020 9:16 AM

Report Template: System: Multi-Page, 508 Compliant [System] (sscpm4, Jan 20, 2020 2:20 PM)

Evaluation Date: Thu Aug 06 09:02:36 CDT 2020
IHSDM Version: v15.0.0 (Oct 31, 2019)
Site Set Crash Prediction Module: $v \mid$ ModuleInfo.moduleVersion| (|ModuleInfo.moduleDate|)

User Name: Scott Nelson
Organization Name: WisDOT NE Region
Phone: 920.366.2109
E-Mail: scott.nelson@dot.wi.gov

Project Title: 6180-30-00, STH 21 from STH 116 to Leonard Point
Project Comment: Created Wed Jul 01 13:40:49 CDT 2020
Project Unit System: U.S. Customary

Site Set: Sand Pit Road Intersection Overlay \& Concrete Repair
Site Set Comment: Created Wed Jul 01 15:29:11 CDT 2020
Site Set Version: v2

Evaluation Title: Sand Pit Predicted Crashes Overlay and Concrete Repair
Evaluation Comment: Created Thu Aug 06 09:02:06 CDT 2020
Policy for Superelevation: AASHTO 2011 U.S. Customary
Calibration: WisDOT Calibration_v15-0
Crash Distribution: WisDOT Distributions_v15-0
Model/CMF: WisDOT Models_v15-0
Note: A Model Data Set other than the HSM (Highway Safety Manual) Configuration was selected for this Evaluation. If Crash Modification Factors (CMFs) were modified, then the results will not be in accordance with the HSM (see HSM Appendix to Part C, section A.1.3).
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Last Year of Analysis: 2036
Empirical-Bayes Analysis: None

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## Section Types

## Rural Two Lane Site Set CPM Evaluation

Site Type<br>Type: 4ST<br>Calibration Factor: 1

Table 1. Evaluation and Crash Data (CSD) (if applicable) Intersection Sites

| Site No. | Type | Highway | Site Description | Major AADT | Minor Aadt | Number of Approaches with Left-Turn Lanes | Number of Approaches with Right-Turn Lane | $\underset{1(\mathrm{deg})}{\text { Skew Angle }}$ | $\begin{array}{\|c} \text { Skew Angle } \\ 2 \text { (deg) } \end{array}$ | Presence of Lighting |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4ST | Sand Pit Road |  | $\begin{aligned} & \text { 2027-2036: } \\ & 14340 \end{aligned}$ | 2027: 1259; 2028: 1266; 2029: 1274; 2030: 1281; 2031: 1288; 2032: 1296; 2033: 1303; 2034: 1311; 2035: 1318; 2036: 1325 | 0 | 2 | 0.0000 | 0.0000 | no |

Table 2. Predicted Crash Frequencies and Rates by Site

| Site <br> No. | Type | Highway | Site Description | Total Predicted Crashes for Evaluation Period | Predicted Total Crash Frequency (crashes/yr) | Predicted FI Crash Frequency (crashes/yr) | Predicted PDO <br> Crash <br> Frequency <br> (crashes/yr) | Predicted Intersection Travel Crash Rate (crashes/million veh) | Intersection Crash Rate (crashes/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4ST | Sand Pit Road |  | 16.070 | 1.6071 | 0.4918 | 1.1153 | 0.28 | 1.6071 |
|  |  | Total | Total | 16.070 | 1.6071 | 0.4918 | 1.1153 | 0.28 | 1.6071 |

Table 3. Predicted Crash Frequencies by Year (4ST)

| Year | Total Crashes | FI Crashes | Percent FI (\%) | PDO Crashes | Percent PDO (\%) |
| :--- | ---: | ---: | ---: | ---: | ---: |
| 2027 | 1.58 | 0.48 | 30.600 | 1.10 | 69.400 |
| 2028 | 1.59 | 0.49 | 30.600 | 1.10 | 69.400 |
| 2029 | 1.59 | 0.49 | 30.600 | 1.11 | 69.400 |
| 2030 | 1.60 | 0.49 | 30.600 | 1.11 | 69.400 |
| 2031 | 1.60 | 0.49 | 30.600 | 1.11 | 69.400 |
| 2032 | 1.61 | 0.49 | 30.600 | 1.12 | 69.400 |
| 2033 | 1.61 | 0.49 | 30.600 | 1.12 | 69.400 |
| 2034 | 1.62 | 0.50 | 30.600 | 1.12 | 69.400 |
| 2035 | 1.63 | 0.50 | 30.600 | 1.13 | 69.400 |
| 2036 | 1.63 | 0.50 | 30.600 | 1.13 | 69.400 |
| Total | 16.07 | 4.92 | 30.600 | 11.15 | 69.400 |
| Average | 1.61 | 0.49 | 30.600 | 1.11 | 69.400 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

Table 4. Predicted 4ST Crash Type Distribution

| Element Type | Crash Type | FI <br> Crashes | Percent <br> FI (\%) | PDO <br> Crashes | Percent <br> PDO (\%) | Total <br> Crashes |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Percent |  |  |  |  |  |  |
| Total (\%) |  |  |  |  |  |  |$|$

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

# Interactive Highway Safety Design Model 

# Crash Prediction Evaluation Report STH 21 \& Sand Pit Road Mainline Left Turns Alternative 

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## Report Overview

## Report Generated: Aug 6, 2020 9:16 AM

Report Template: System: Multi-Page, 508 Compliant [System] (sscpm4, Jan 20, 2020 2:20 PM)

Evaluation Date: Thu Aug 06 09:03:12 CDT 2020
IHSDM Version: v15.0.0 (Oct 31, 2019)
Site Set Crash Prediction Module: $v \mid$ ModuleInfo.moduleVersion| (|ModuleInfo.moduleDate|)

User Name: Scott Nelson
Organization Name: WisDOT NE Region
Phone: 920.366.2109
E-Mail: scott.nelson@dot.wi.gov

Project Title: 6180-30-00, STH 21 from STH 116 to Leonard Point
Project Comment: Created Wed Jul 01 13:40:49 CDT 2020
Project Unit System: U.S. Customary

Site Set: Sand Pit Road Intersection STH 21 Left Turn Lanes
Site Set Comment: Copied from Sand Pit Road Intersection Overlay \& Concrete Repair (v2)
Site Set Version: v2

Evaluation Title: Sand Pit Predicted Crashes Left Turn Lanes
Evaluation Comment: Created Thu Aug 06 09:02:51 CDT 2020
Policy for Superelevation: AASHTO 2011 U.S. Customary
Calibration: WisDOT Calibration_v15-0
Crash Distribution: WisDOT Distributions_v15-0
Model/CMF: WisDOT Models_v15-0
Note: A Model Data Set other than the HSM (Highway Safety Manual) Configuration was selected for this Evaluation. If Crash Modification Factors (CMFs) were modified, then the results will not be in accordance with the HSM (see HSM Appendix to Part C, section A.1.3).
First Year of Analysis: 2027
Last Year of Analysis: 2036
Empirical-Bayes Analysis: None

## Disclaimer Regarding Crash Prediction Method

## IMPORTANT NOTICE ABOUT COMPARING RESULTS FROM HIGHWAY SAFETY MANUAL FIRST EDITION (2010) MODELS TO RESULTS FROM NEW MODELS DEVELOPED UNDER NCHRP PROJECTS 17-70 AND 17-58

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Highway and Transportation Officials (AASHTO), multiple research efforts have been undertaken through the National Cooperative Highway Research Program (NCHRP) to develop safety performance models for road segment and intersection facility types that were not initially reflected in the HSM-1, in order to expand the breadth and depth of the HSM in the future.

The IHSDM Crash Prediction Module (CPM) is intended as a faithful implementation of HSM Part C predictive methods. As NCHRP projects to develop new predictive methods for the HSM are completed, FHWA works to incorporate the new methods into IHSDM, sometimes in advance of publication in the HSM. The following new crash predictive methods have been accepted by NCHRP project panels and incorporated into IHSDM, while pending AASHTO's approval for incorporation into a future edition of the HSM:

- Roundabouts: completed in 2018 under NCHRP Project 17-70, the new methods will provide improved outcomes for the safety analysis of roundabouts.
- 6+ lane and one-way urban/suburban arterials (including models for segments and intersections): completed under NCHRP Project 17-58.

However, in the absence of local calibration factors (see HSM-1 Part C, Appendix A for guidance on calibration of the predictive models), it is neither appropriate nor advisable to directly compare the results from new models (from NCHRP Projects 17-58 and 17-70) to results from HSM-1 models, as the models were not calibrated to the same base state data sets, and consequently can produce unexpected results. If local calibration factors are available and applied to both new models and HSM- 1 models, then it may be appropriate to directly compare the results.[Note: Work being performed under NCHRP Project 17-72 (Update of Crash Modification Factors for the Highway Safety Manual) is expected to re-calibrate many of the old (HSM-1) and new (e.g., NCHRP 17-70) models to data from a single (or small number of) states, that would allow results from all models to be directly compared.]

The models produced for NCHRP Project 17-70 have independent value in terms of informing the design of a roundabout and assessing the effects of different design characteristics on the expected safety performance of a roundabout.

The HSM-1 interim method previously included in IHSDM for evaluating roundabouts on urban/suburban arterials (i.e., evaluating an existing intersection and then applying a Crash Modification Factor for replacing the existing intersection with a roundabout) has been deactivated in IHSDM, to minimize any confusion with the new roundabout methodology.

## Section Types

## Rural Two Lane Site Set CPM Evaluation

Site Type<br>Type: 4ST<br>Calibration Factor: 1

Table 1. Evaluation and Crash Data (CSD) (if applicable) Intersection Sites

| Site No. | Type | Highway | Site Description | Major AADT | Minor Aadt | Number of Approaches with Left-Turn Lanes | Number of Approaches with Right-Turn Lane | $\underset{1(\mathrm{deg})}{\text { Skew Angle }}$ | $\begin{array}{\|c} \text { Skew Angle } \\ 2 \text { (deg) } \end{array}$ | Presence of Lighting |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4ST | Sand Pit Road |  | $\begin{aligned} & \text { 2027-2036: } \\ & 14340 \end{aligned}$ | 2027: 1259; 2028: 1266; 2029: 1274; 2030: 1281; 2031: 1288; 2032: 1296; 2033: 1303; 2034: 1311; 2035: 1318; 2036: 1325 |  | 2 | 0.0000 | 0.0000 | no |

Table 2. Predicted Crash Frequencies and Rates by Site

| Site <br> No. | Type | Highway | Site Description | Total Predicted Crashes for Evaluation Period | Predicted Total Crash Frequency (crashes/yr) | Predicted FI Crash Frequency (crashes/yr) | Predicted PDO <br> Crash <br> Frequency (crashes/yr) | Predicted Intersection Travel Crash Rate (crashes/million veh) | Intersection Crash Rate (crashes/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4ST | Sand Pit Road |  | 8.357 | 0.8357 | 0.2557 | 0.5800 | 0.15 | 0.8357 |
|  |  | Total | Total | 8.357 | 0.8357 | 0.2557 | 0.5800 | 0.15 | 0.8357 |

Table 3. Predicted Crash Frequencies by Year (4ST)

| Year | Total Crashes | FI Crashes | Percent FI (\%) | PDO Crashes | Percent PDO (\%) |
| :--- | ---: | ---: | ---: | ---: | ---: |
| 2027 | 0.82 | 0.25 | 30.600 | 0.57 | 69.400 |
| 2028 | 0.82 | 0.25 | 30.600 | 0.57 | 69.400 |
| 2029 | 0.83 | 0.25 | 30.600 | 0.57 | 69.400 |
| 2030 | 0.83 | 0.25 | 30.600 | 0.58 | 69.400 |
| 2031 | 0.83 | 0.26 | 30.600 | 0.58 | 69.400 |
| 2032 | 0.84 | 0.26 | 30.600 | 0.58 | 69.400 |
| 2033 | 0.84 | 0.26 | 30.600 | 0.58 | 69.400 |
| 2034 | 0.84 | 0.26 | 30.600 | 0.58 | 69.400 |
| 2035 | 0.85 | 0.26 | 30.600 | 0.59 | 69.400 |
| 2036 | 0.85 | 0.26 | 30.600 | 0.59 | 69.400 |
| Total | 8.36 | 2.56 | 30.600 | 5.80 | 69.400 |
| Average | 0.84 | 0.26 | 30.600 | 0.58 | 69.400 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

Table 4. Predicted 4ST Crash Type Distribution

| Element Type | Crash Type | FI <br> Crashes | Percent <br> FI (\%) | PDO <br> Crashes | Percent <br> PDO (\%) | Total <br> Crashes |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Percent |  |  |  |  |  |  |
| Total (\%) |  |  |  |  |  |  |$|$

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

# Interactive Highway Safety Design Model 

# Crash Prediction Evaluation Report 

STH 21 \& Sand Pit Road Roundabout Alternative

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## Report Overview

## Report Generated: Aug 6, 2020 9:18 AM

Report Template: System: Multi-Page, 508 Compliant [System] (sscpm4, Jan 20, 2020 2:20 PM)

Evaluation Date: Thu Aug 06 09:03:53 CDT 2020
IHSDM Version: v15.0.0 (Oct 31, 2019)
Site Set Crash Prediction Module: $v \mid$ ModuleInfo.moduleVersion| (|ModuleInfo.moduleDate|)

User Name: Scott Nelson
Organization Name: WisDOT NE Region
Phone: 920.366.2109
E-Mail: scott.nelson@dot.wi.gov

Project Title: 6180-30-00, STH 21 from STH 116 to Leonard Point
Project Comment: Created Wed Jul 01 13:40:49 CDT 2020
Project Unit System: U.S. Customary

Site Set: Sand Pit Road Intersection Roundabout
Site Set Comment: Copied from Sand Pit Road Intersection STH 21 Left Turn Lanes (v2)
Site Set Version: v4

Evaluation Title: Sand Pit Predicted Crashes Roundabout
Evaluation Comment: Created Thu Aug 06 09:03:27 CDT 2020
Policy for Superelevation: AASHTO 2011 U.S. Customary
Calibration: WisDOT Calibration_v15-0
Crash Distribution: WisDOT Distributions_v15-0
Model/CMF: WisDOT Models_v15-0
Note: A Model Data Set other than the HSM (Highway Safety Manual) Configuration was selected for this Evaluation. If Crash Modification Factors (CMFs) were modified, then the results will not be in accordance with the HSM (see HSM Appendix to Part C, section A.1.3).
First Year of Analysis: 2027
Last Year of Analysis: 2036
Empirical-Bayes Analysis: None

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However, in the absence of local calibration factors (see HSM-1 Part C, Appendix A for guidance on calibration of the predictive models), it is neither appropriate nor advisable to directly compare the results from new models (from NCHRP Projects 17-58 and 17-70) to results from HSM-1 models, as the models were not calibrated to the same base state data sets, and consequently can produce unexpected results. If local calibration factors are available and applied to both new models and HSM- 1 models, then it may be appropriate to directly compare the results.[Note: Work being performed under NCHRP Project 17-72 (Update of Crash Modification Factors for the Highway Safety Manual) is expected to re-calibrate many of the old (HSM-1) and new (e.g., NCHRP 17-70) models to data from a single (or small number of) states, that would allow results from all models to be directly compared.]

The models produced for NCHRP Project 17-70 have independent value in terms of informing the design of a roundabout and assessing the effects of different design characteristics on the expected safety performance of a roundabout.

The HSM-1 interim method previously included in IHSDM for evaluating roundabouts on urban/suburban arterials (i.e., evaluating an existing intersection and then applying a Crash Modification Factor for replacing the existing intersection with a roundabout) has been deactivated in IHSDM, to minimize any confusion with the new roundabout methodology.

## Section Types

## Roundabout Site Set CPM Evaluation

## Site Type

Type: Roundabout RTL 41R
Calibration Factor: RTL 41R $=1.0$

Table 1. Evaluation and Crash Data (CSD) (if applicable) Roundabout - Homogeneous Sites

| Site No. | Type | Roundabout | Area Type | Entering AADT |
| :---: | :---: | :---: | :---: | :---: |
|  | 4IR - Roundabout with 4 legs and a single circulating lane | Sand Pit Road | Rural | Leg 1:2027: 629; 2028: 633; 2029: 637; 2030: 640; 2031: 644; 2032: 648; 2033: 651; 2034: 655; 2035: 659; 2036: 662; Leg 2:2027-2036: 7170; Leg 3:2027: 629; 2028: 633; 2029: 637; 2030: 640; 2031: 644; 2032: 648; 2033: 651; 2034: 655; 2035: 659; 2036: 662; Leg 4:2027-2036: 7170 |

Table 2. Predicted Crash Frequencies and Rates by Site

| $\begin{aligned} & \text { Site } \\ & \text { No. } \end{aligned}$ | Type | Roundabout | Site Description | Total Predicted Crashes for Evaluation Period | Predicted Total Crash Frequency (crashes/yr) | Predicted FI Crash Frequency (crashes/yr) | Predicted PDO <br> Crash <br> Frequency <br> (crashes/yr) | Predicted Intersection Travel Crash Rate (crashes/million veh) | Intersection Crash Rate (crashes/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 41R - Roundabout with 4 legs and a single circulating lane | Sand Pit Road |  | 21.610 | 2.1610 | 0.2965 | 1.8645 | 0.76 | 2.1610 |
|  |  | Total | Total | 21.610 | 2.1610 | 0.2965 | 1.8645 | 0.76 | 2.1610 |

Table 3. Predicted Crash Frequencies by Year (Roundabout RTL 41R)

| Year | Total Crashes | FI Crashes | Percent FI (\%) | PDO Crashes | Percent PDO (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2027 | 2.16 | 0.30 | 13.715 | 1.86 | 86.285 |
| 2028 | 2.16 | 0.30 | 13.716 | 1.86 | 86.284 |
| 2029 | 2.16 | 0.30 | 13.717 | 1.86 | 86.282 |
| 2030 | 2.16 | 0.30 | 13.718 | 1.86 | 86.282 |
| 2031 | 2.16 | 0.30 | 13.720 | 1.86 | 86.280 |
| 2032 | 2.16 | 0.30 | 13.721 | 1.86 | 86.279 |
| 2033 | 2.16 | 0.30 | 13.722 | 1.86 | 86.278 |
| 2034 | 2.16 | 0.30 | 13.723 | 1.87 | 86.277 |
| 2035 | 2.16 | 0.30 | 13.725 | 1.87 | 86.275 |
| 2036 | 2.16 | 0.30 | 13.726 | 1.87 | 86.275 |
| Total | 21.61 | 2.96 | 13.720 | 18.64 | 86.280 |
| Average | 2.16 | $0.30$ | 13.720 | 1.86 | 86.280 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

Table 4. Predicted Roundabout RTL 41R Crash Severity

| Site No. | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating Injury <br> (B) Crashes (crashes) | Possible Injury <br> (C) Crashes <br> (crashes) | No Injury <br> (O) Crashes <br> (crashes) |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 1 | 0.0191 | 0.1898 | 1.2209 | 1.5353 | 18.6452 |
| Total | 0.0191 | 0.1898 | 1.2209 | 1.5353 | 18.6452 |

Table 5. Predicted Roundabout RTL 41R Crash Type Distribution

| Element Type | Crash Type | FI <br> Crashes | Percent <br> FI (\%) | PDO <br> Crashes | Percent <br> PDO <br> $(\%)$ | Total <br> Crashes |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Potal (\%) |  |  |  |  |  |  |$|$| Percent |  |
| ---: | :--- |
| Intersection | Collision with Animal |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

## ATTACHMENT E

## Safety Mitigation Certification Documentation

IHSDM Economic Analysis Report

# Interactive Highway Safety Design Model 

## Economic Analysis Report

## STH 21 \& CTH FF

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## Economic Analysis Report

## Economic Analysis Report Overview

Report Generated: Aug 6, 2020 9:19 AM
Report Template: System: Multi-Page [System] (eam2, Jan 20, 2020 2:20 PM)

Evaluation Title: EAAnalysis Updated 8/6/2020
Evaluation Comment: Created Thu Aug 06 09:06:21 CDT 2020
Evaluation Date: Thu Aug 06 09:06:46 CDT 2020

User Name: Scott Nelson
Organization Name: WisDOT NE Region
Phone: 920.366.2109
E-Mail: scott.nelson@dot.wi.gov

Project Title: 6180-30-00, STH 21 \& CTH FF Evaluation
Project Comment: Created Wed Jul 01 14:29:10 CDT 2020

## Configuration Summary

Crash Cost Configuration: WisDOT Economics_v15-0
Configuration Comment: WisDOT Crash Costs

Table 1. Economic Analysis Configuration

| Configuration Data |  |
| ---: | ---: |
| Crash Unit Cost Zero Year | 2016 |
| Crash Cost Index | 0.00 |
| Discount Rate | 0.03 |
| KABCO Unit Costs | $\mathbf{1 0 , 8 9 7 , 5 8 0 . 0 0}$ |
| K Cost (\$/Crash) | $\mathbf{6 1 3 , 7 8 1 . 0 0}$ |
| A Cost (\$/Crash) | $\mathbf{1 9 4 , 0 2 2 . 0 0}$ |
| B Cost (\$/Crash) | $\mathbf{1 1 0 , 8 3 0 . 0 0}$ |
| C Cost (\$/Crash) | $\mathbf{1 0 , 1 7 3 . 0 0}$ |

Table 2. RTL Segment FI Proportion Data

| Segment Type | Fatal Crash (K) <br> Proportion of FI <br> $(\%)$ | Incapacitating Injury <br> Crash (A) Proportion of <br> FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of FI <br> (\%) |
| :---: | :---: | ---: | ---: | :---: |
| Two-Lane Undivided | 3.502 | 12.638 | 43.370 | 40.490 |

Table 3. RTL Intersection FI Proportion Data

| Intersection Type | Fatal Crash <br> (K) Proportion <br> of FI (\%) | Incapacitating Injury <br> Crash (A) Proportion <br> of FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of <br> FI (\%) |
| ---: | ---: | ---: | ---: | ---: |
| Three-Legged w/STOP control | 3.070 | 15.070 | 42.380 | 39.480 |
| Four-Legged w/STOP control | 3.980 | 15.280 | 42.860 | 37.880 |
| Four-Legged Signalized | 2.960 | 11.750 | 35.290 | 50.000 |

Table 4. RML Segment FI Proportion Data

| Segment Type | Fatal Crash (K) <br> Proportion of FI <br> (\%) | Incapacitating Injury <br> Crash (A) Proportion of <br> FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of FI <br> (\%) |
| ---: | ---: | ---: | ---: | ---: |
| Four-Lane Undivided | 3.502 | 12.638 | 43.370 | 40.490 |
| Four-Lane Divided | 3.502 | 12.638 | 43.370 | 40.490 |

Table 5. RML Intersection FI Proportion Data

| Intersection Type | Fatal Crash <br> (K) Proportion <br> of FI (\%) | Incapacitating Injury <br> Crash (A) Proportion <br> of FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of <br> FI (\%) |
| ---: | ---: | ---: | ---: | ---: |
| Three-Legged w/STOP control | 4.090 | 14.090 | 40.630 | 41.190 |
| Four-Legged w/STOP control | 4.710 | 15.910 | 41.990 | 37.390 |
| Four-Legged Signalized | 0.600 | 10.010 | 37.180 | 52.210 |

Table 6. USA Segment FI Proportion Data

| Segment Type | Fatal Crash (K) <br> Proportion of <br> FI (\%) | Incapacitating Injury <br> Crash (A) Proportion <br> of FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of <br> FI (\%) |
| ---: | ---: | ---: | ---: | ---: |
| Two-Lane Undivided | 1.012 | 5.785 | 33.011 | 60.192 |
| Three-Lane w/Center TWLTL | 1.012 | 5.785 | 33.011 | 60.192 |
| Four-Lane Undivided | 1.012 | 5.785 | 33.011 | 60.192 |
| Four-Lane Divided | 1.012 | 5.785 | 33.011 | 60.192 |
| Five-Lane w/Center TWLTL | 1.012 | 5.785 | 33.011 | 60.192 |

Table 7. USA Intersection FI Proportion Data

| Intersection Type | Fatal Crash <br> (K) Proportion <br> of FI (\%) | Incapacitating Injury <br> Crash (A) Proportion <br> of FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of <br> FI (\%) |
| ---: | ---: | ---: | ---: | ---: |
| Three-Legged w/STOP control | 0.744 | 6.558 | 36.725 | 55.973 |
| Three-Legged Signalized | 0.451 | 4.957 | 32.024 | 62.568 |
| Four-Legged w/STOP control | 0.864 | 6.637 | 38.161 | 54.338 |
| Four-Legged Signalized | 0.715 | 5.263 | 32.359 | 61.663 |

## Analysis Output Summary

Analysis Type: Benefit/Cost

Table 8. Case Cost Summary

| Is <br> Base <br> Case | Title | Present Value <br> of Crash Cost <br> $\mathbf{( \$ )}$ | Present <br> Value of <br> Other Cost <br> $\mathbf{( \$ )}$ | Net Present <br> Value of <br> Benefits (B) <br> $\mathbf{( \$ )}$ | Net Present <br> Value of <br> Costs (C) <br> $\mathbf{( \$ )}$ | Present Value <br> of Net Benefit <br> (B-C) <br> $\mathbf{( \$ )}$ | Benefit <br> Cost Ratio <br> $(\mathbf{B} / \mathbf{C})$ |
| :--- | :--- | :---: | :---: | :---: | :---: | ---: | ---: |
| Yes | Overlay and Concrete Repairs | $3,443,820.60$ | $170,000.00$ |  |  |  |  |
|  | STH 21 Left Turn Lanes Added | $1,790,786.71$ | $830,000.00$ | $1,653,033.89$ | $660,000.00$ | $993,033.89$ | 2.5046 |
|  | STH 21 \& CTH FF Roundabout | $698,966.63$ | $950,000.00$ | $2,744,853.97$ | $780,000.00$ | $1,964,853.97$ | 3.5190 |

Table 9. Case Crash Summary

| Is <br> Base <br> Case | Title | Fatal (K) <br> Crashes (crashes) | Incapacitating Injury (A) Crashes (crashes) | Non-Incapacitating Injury (B) Crashes (crashes) | Possible <br> Injury (C) <br> Crashes (crashes) | No <br> Injury <br> (O) <br> Crashes (crashes) | Total Crashes (crashes) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Yes | Overlay and Concrete Repairs | 0.2311 | 0.8872 | 2.4887 | 2.1995 | 13.1690 | 18.9755 |
|  | STH 21 Left Turn Lanes Added | 0.1202 | 0.4614 | 1.2941 | 1.1437 | 6.8479 | 9.8672 |
|  | STH 21 \& CTH FF Roundabout | 0.0178 | 0.1766 | 1.1362 | 1.0295 | 15.6510 | 18.0111 |

## Crash Cost Data

## Overlay and Concrete Repairs Data

Case Title: Overlay and Concrete Repairs
Is Base Case: true
Present Value of Crash Cost: $3,443,820.60$
Present Value of Other Cost: 170,000.00

## Table 10. Overlay and Concrete Repairs Evaluation Cost

| Project or Interchange | Selected Facility | Selected Evaluation | Present Value of Crash Cost (\$) |
| :---: | :--- | :--- | ---: |
| $6180-30-00$, STH 21 from STH 116 to Leonard Point | CTH FF Intersection Overlay \& Concrete Repair | CTH FF Predicted Crashes Overlay \& Concrete Repair | $3,443,820.60$ |
| Total |  |  | $3,443,820.60$ |

Table 11. Overlay and Concrete Repairs Evaluation Crashes

| Project or Interchange | Selected Facility | Selected Evaluation | Fatal (K) Crashes (crashes) | Incapacitating Injury (A) Crashes (crashes) | Non-Incapacitating Injury (B) Crashes (crashes) | Possible Injury (C) Crashes (crashes) | No Injury (O) <br> $\begin{array}{c}\text { Crashes } \\ \text { (crashes) }\end{array}$ | Total Crashes (crashes) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6180-30-00, STH 21 from STH 116 to Leonard Point | CTH FF Intersection Overlay \& Concrete Repair | CTH FF Predicted Crashes Overlay \& Concrete Repair | 0.2311 | 0.8872 | 2.4887 | 2.1995 | 13.1690 | 18.9755 |
| Total |  |  | 0.2311 | 0.8872 | 2.4887 | 2.1995 | 13.1690 | 18.9755 |

Table 12. CTH FF Intersection Overlay \& Concrete Repair Facility Type Crashes

| Facility Type | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating Injury (B) <br> Crashes (crashes) | Possible Injury <br> (C) Crashes <br> (crashes) | No Injury (0) <br> Crashes <br> (crashes) | Total Crashes <br> (crashes) |
| :---: | :---: | ---: | ---: | ---: | ---: | ---: |
| Rural Two-Lane Intersection | 0.2311 | 0.8872 | 2.4887 | 2.1995 | 13.1690 | 18.9755 |
| Total | 0.2311 | 0.8872 | 2.4887 | 2.1995 | 13.1690 | 18.9755 |

## STH 21 Left Turn Lanes Added Data

Case Title: STH 21 Left Turn Lanes Added
Is Base Case: false
Present Value of Crash Cost: $1,790,786.71$
Present Value of Other Cost: 830,000.00

Table 13. STH 21 Left Turn Lanes Added Evaluation Cost

| Project or Interchange | Selected Facility | Selected Evaluation | Present Value of Crash <br> Cost $(\$)$ |
| :---: | :---: | :---: | :---: |
| $6180-30-00$, STH 21 from STH 116 to Leonard Point | CTH FF Intersection with STH 21 Left Turn Lanes | CTH FF Predicted Crashes Left Turn Lanes | $1,790,786.71$ |
| Total |  |  | $1,790,786.71$ |

Table 14. STH 21 Left Turn Lanes Added Evaluation Crashes

| Project or Interchange | Selected Facility | Selected Evaluation | Fatal (K) Crashes (crashes) | Incapacitating Injury (A) Crashes (crashes) | Non-Incapacitating Injury (B) Crashes (crashes) | Possible Injury <br> (C) Crashes (crashes) | $\begin{aligned} & \text { No Injury (O) } \\ & \text { Crashes } \\ & \text { (crashes) } \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { Total Crashes } \\ \text { (crashes) } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6180-30-00, STH 21 from STH 116 to Leonard Point | CTH FF Intersection with STH 21 Left Turn Lanes | CTH FF Predicted Crashes Left Turn Lanes | 0.1202 | 0.4614 | 1.2941 | 1.1437 | 6.8479 | 9.8672 |
| Total |  |  | 0.1202 | 0.4614 | 1.2941 | 1.1437 | 6.8479 | 9.8672 |

Table 15. CTH FF Intersection with STH 21 Left Turn Lanes Facility Type Crashes

| Facility Type | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating Injury (B) <br> Crashes (crashes) | Possible Injury <br> (C) Crashes <br> (crashes) | No Injury (O) <br> Crashes <br> (crashes) | Total Crashes <br> (crashes) |
| :---: | :---: | ---: | ---: | ---: | ---: | ---: |
| Rural Two-Lane Intersection | 0.1202 | 0.4614 | 1.2941 | 1.1437 | 6.8479 | 9.8672 |
| Total | 0.1202 | 0.4614 | 1.2941 | 1.1437 | 6.8479 | 9.8672 |

## STH 21 \& CTH FF Roundabout Data

Case Title: STH 21 \& CTH FF Roundabout
Is Base Case: false
Present Value of Crash Cost: 698,966.63
Present Value of Other Cost: $950,000.00$

Table 16. STH 21 \& CTH FF Roundabout Evaluation Cost

| Project or Interchange | Selected Facility | Selected Evaluation | Present Value of <br> Crash Cost (\$) |
| :---: | :---: | :---: | :---: |
| 6180-30-00, STH 21 from STH 116 to Leonard <br> Point | CTH FF Intersection Single Lane Roundabout | CTH FF Crash Prediction |  |
| Total |  |  | $698,966.63$ |
| Roundabout |  |  |  |

Table 17. STH 21 \& CTH FF Roundabout Evaluation Crashes

| Project or Interchange | Selected Facility | Selected Evaluation | Fatal (K) Crashes (crashes) | Incapacitating Injury (A) Crashes (crashes) | Non-Incapacitating Injury (B) Crashes (crashes) | Possible Injury (C) Crashes (crashes) | $\begin{array}{\|c\|} \hline \text { No Injury (0) } \\ \text { Crashes } \\ \text { (crashes) } \\ \hline \end{array}$ | $\begin{gathered} \text { Total Crashes } \\ \text { (crashes) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6180-30-00, STH 21 from STH 116 to Leonard Point | CTH FF Intersection Single Lane Roundabout | CTH FF Crash Prediction Roundabout | 0.0178 | 0.1766 | 1.1362 | 1.0295 | 15.6510 | 18.0111 |
| Total |  |  | 0.0178 | 0.1766 | 1.1362 | 1.0295 | 15.6510 | 18.011 |

Table 18. CTH FF Intersection Single Lane Roundabout Facility Type Crashes

| Facility Type | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating Injury (B) <br> Crashes (crashes) | Possible Injury <br> (C) Crashes <br> (crashes) | No Injury (O) <br> Crashes <br> (crashes) | Total Crashes <br> (crashes) |
| :---: | :---: | ---: | ---: | ---: | ---: | ---: |
| Roundabout | 0.0178 | 0.1766 | 1.1362 | 1.0295 | 15.6510 | 18.0111 |
| Total | 0.0178 | 0.1766 | 1.1362 | 1.0295 | 15.6510 | 18.0111 |

## Evaluation Message

# Interactive Highway Safety Design Model 

 Economic Analysis Report
## STH 21 \& Sand Pit Road

## Disclaimer

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## Economic Analysis Report

## Economic Analysis Report Overview

Report Generated: Aug 6, 2020 10:05 AM
Report Template: System: Multi-Page [System] (eam2, Jan 20, 2020 2:20 PM)

Evaluation Title: EAAnalysis 4 Updated 8/6/2020
Evaluation Comment: Created Thu Aug 06 10:04:25 CDT 2020
Evaluation Date: Thu Aug 06 10:04:44 CDT 2020

User Name: Scott Nelson
Organization Name: WisDOT NE Region
Phone: 920.366.2109
E-Mail: scott.nelson@dot.wi.gov

Project Title: 6180-30-00, STH 21 \& Sand Pit Road Evaluation
Project Comment: Created Wed Jul 01 16:09:50 CDT 2020

## Configuration Summary

Crash Cost Configuration: WisDOT Economics_v15-0
Configuration Comment: WisDOT Crash Costs

Table 1. Economic Analysis Configuration

| Configuration Data |  |
| ---: | ---: |
| Crash Unit Cost Zero Year | 2016 |
| Crash Cost Index | 0.00 |
| Discount Rate | 0.03 |
| KABCO Unit Costs | $\mathbf{1 0 , 8 9 7 , 5 8 0 . 0 0}$ |
| K Cost (\$/Crash) | $\mathbf{6 1 3 , 7 8 1 . 0 0}$ |
| A Cost (\$/Crash) | $\mathbf{1 9 4 , 0 2 2 . 0 0}$ |
| B Cost (\$/Crash) | $\mathbf{1 1 0 , 8 3 0 . 0 0}$ |
| C Cost (\$/Crash) | $\mathbf{1 0 , 1 7 3 . 0 0}$ |

Table 2. RTL Segment FI Proportion Data

| Segment Type | Fatal Crash (K) <br> Proportion of FI <br> $(\%)$ | Incapacitating Injury <br> Crash (A) Proportion of <br> FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of FI <br> (\%) |
| :---: | :---: | ---: | ---: | :---: |
| Two-Lane Undivided | 3.502 | 12.638 | 43.370 | 40.490 |

Table 3. RTL Intersection FI Proportion Data

| Intersection Type | Fatal Crash <br> (K) Proportion <br> of FI (\%) | Incapacitating Injury <br> Crash (A) Proportion <br> of FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of <br> FI (\%) |
| ---: | ---: | ---: | ---: | ---: |
| Three-Legged w/STOP control | 3.070 | 15.070 | 42.380 | 39.480 |
| Four-Legged w/STOP control | 3.980 | 15.280 | 42.860 | 37.880 |
| Four-Legged Signalized | 2.960 | 11.750 | 35.290 | 50.000 |

Table 4. RML Segment FI Proportion Data

| Segment Type | Fatal Crash (K) <br> Proportion of FI <br> (\%) | Incapacitating Injury <br> Crash (A) Proportion of <br> FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of FI <br> (\%) |
| ---: | ---: | ---: | ---: | ---: |
| Four-Lane Undivided | 3.502 | 12.638 | 43.370 | 40.490 |
| Four-Lane Divided | 3.502 | 12.638 | 43.370 | 40.490 |

Table 5. RML Intersection FI Proportion Data

| Intersection Type | Fatal Crash <br> (K) Proportion <br> of FI (\%) | Incapacitating Injury <br> Crash (A) Proportion <br> of FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of <br> FI (\%) |
| ---: | ---: | ---: | ---: | ---: |
| Three-Legged w/STOP control | 4.090 | 14.090 | 40.630 | 41.190 |
| Four-Legged w/STOP control | 4.710 | 15.910 | 41.990 | 37.390 |
| Four-Legged Signalized | 0.600 | 10.010 | 37.180 | 52.210 |

Table 6. USA Segment FI Proportion Data

| Segment Type | Fatal Crash (K) <br> Proportion of <br> FI (\%) | Incapacitating Injury <br> Crash (A) Proportion <br> of FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of <br> FI (\%) |
| ---: | ---: | ---: | ---: | ---: |
| Two-Lane Undivided | 1.012 | 5.785 | 33.011 | 60.192 |
| Three-Lane w/Center TWLTL | 1.012 | 5.785 | 33.011 | 60.192 |
| Four-Lane Undivided | 1.012 | 5.785 | 33.011 | 60.192 |
| Four-Lane Divided | 1.012 | 5.785 | 33.011 | 60.192 |
| Five-Lane w/Center TWLTL | 1.012 | 5.785 | 33.011 | 60.192 |

Table 7. USA Intersection FI Proportion Data

| Intersection Type | Fatal Crash <br> (K) Proportion <br> of FI (\%) | Incapacitating Injury <br> Crash (A) Proportion <br> of FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of <br> FI (\%) |
| ---: | ---: | ---: | ---: | ---: |
| Three-Legged w/STOP control | 0.744 | 6.558 | 36.725 | 55.973 |
| Three-Legged Signalized | 0.451 | 4.957 | 32.024 | 62.568 |
| Four-Legged w/STOP control | 0.864 | 6.637 | 38.161 | 54.338 |
| Four-Legged Signalized | 0.715 | 5.263 | 32.359 | 61.663 |

## Analysis Output Summary

Analysis Type: Benefit/Cost

Table 8. Case Cost Summary

| Is Base Case | Title | Present Value of Crash Cost (\$) | Present Value of Other Cost (\$) | Net Present Value of Benefits (B) (\$) | Net Present Value of Costs (C) $(\$)$ | Present Value of Net Benefit (B-C) <br> (\$) | Benefit Cost <br> Ratio (B/C) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Yes | Sand Pit Overylay \& Concrete Repair | 2,917,076.43 | 170,000.00 |  |  |  |  |
|  | Sand Pit STH 21 Left Turn Lanes | 1,516,879.75 | 720,000.00 | 1,400,196.68 | 550,000.00 | 850,196.68 | 2.5458 |
|  | Sand Pit Road Roundabout | 809,019.74 | 900,000.00 | 2,108,056.68 | 730,000.00 | 1,378,056.68 | 2.8878 |

Table 9. Case Crash Summary

| Is Base Case | Title | Fatal (K) <br> Crashes (crashes) | Incapacitating Injury (A) Crashes (crashes) | Non-Incapacitating Injury <br> (B) Crashes (crashes) | Possible Injury (C) Crashes (crashes) | No Injury (O) Crashes (crashes) | Total Crashes (crashes) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Yes | Sand Pit Overylay \& Concrete Repair | 0.1957 | 0.7514 | 2.1077 | 1.8628 | 11.1530 | 16.0705 |
|  | Sand Pit STH 21 Left Turn Lanes | 0.1018 | 0.3907 | 1.0960 | 0.9686 | 5.7995 | 8.3567 |
|  | Sand Pit Road Roundabout | 0.0191 | 0.1897 | 1.2204 | 1.5359 | 18.6452 | 21.6102 |

## Crash Cost Data

## Sand Pit Overylay \& Concrete Repair Data

Case Title: Sand Pit Overylay \& Concrete Repair
Is Base Case: true
Present Value of Crash Cost: 2,917,076.43
Present Value of Other Cost: 170,000.00

Table 10. Sand Pit Overylay \& Concrete Repair Evaluation Cost

| Project or Interchange | Selected Facility | Selected Evaluation |
| :---: | :--- | :--- | :--- |
| $6180-30-00$, STH 21 from STH 116 to Leoonard Point | Sand Pit Road Intersection Overlay \& Concrete Repair |  |
| Total |  | Sand Pit Predicted Crashes Overlay Crash Cost (\$) |

Table 11. Sand Pit Overylay \& Concrete Repair Evaluation Crashes

| Project or Interchange | Selected Facility | Selected Evaluation | Fatal (K) Crashes (crashes) | Incapacitating Injury (A) Crashes (crashes) | Non-Incapacitating Injury <br> (B) Crashes (crashes) | Possible Injury (C) Crashes (crashes) | $\begin{gathered} \text { No Injury (O) } \\ \begin{array}{c} \text { Crashes } \\ \text { (crashes) } \end{array} \\ \hline \end{gathered}$ | $\begin{array}{\|l} \text { Total Crashes } \\ \text { (crashes) } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6180-30-00, STH 21 from STH 116 to Leonard Point | Sand Pit Road Intersection Overlay \& Concrete Repair | Sand Pit Predicted Crashes Overlay and Concrete Repair | 0.1957 | 0.7514 | 2.1077 | 1.8628 | 11.1530 | 16.0705 |
| Total |  |  | 0.1957 | 0.7514 | 2.1077 | 1.8628 | 11.1530 | 16.0705 |

Table 12. Sand Pit Road Intersection Overlay \& Concrete Repair Facility Type Crashes

| Facility Type | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating Injury (B) <br> Crashes (crashes) | Possible Injury <br> (C) Crashes <br> (crashes) | No Injury (O) <br> Crashes <br> (crashes) | Total Crashes <br> (crashes) |
| :---: | :---: | ---: | ---: | ---: | ---: | ---: |
| Rural Two-Lane Intersection | 0.1957 | 0.7514 | 2.1077 | 1.8628 | 11.1530 | 16.0705 |
| Total | 0.1957 | 0.7514 | 2.1077 | 1.8628 | 11.1530 | 16.0705 |

## Sand Pit STH 21 Left Turn Lanes Data

Case Title: Sand Pit STH 21 Left Turn Lanes
Is Base Case: false
Present Value of Crash Cost: $1,516,879.75$
Present Value of Other Cost: 720,000.00

Table 13. Sand Pit STH 21 Left Turn Lanes Evaluation Cost

| Project or Interchange | Selected Facility | Selected Evaluation | Present Value of Crash <br> Cost (\$) |
| :---: | :---: | :---: | :---: |
| 6180-30-00, STH 21 from STH 116 to Leonard Point | Sand Pit Road Intersection STH 21 Left Turn Lanes | Sand Pit Predicted Crashes Left Turn Lanes | $1,516,879.75$ |
| Total |  |  | $1,516,879.75$ |

Table 14. Sand Pit STH 21 Left Turn Lanes Evaluation Crashes

| Project or Interchange | Selected Facility | Selected Evaluation | Fatal (K) Crashes (crashes) | Incapacitating Injury (A) Crashes (crashes) | Non-Incapacitating Injury (B) Crashes (crashes) | Possible Injury <br> (C) Crashes (crashes) | $\begin{array}{\|c} \text { No Injury ( } \mathbf{O} \text { ( } \\ \begin{array}{c} \text { Crashes } \\ \text { (crashes) } \end{array} \\ \hline \end{array}$ | Total Crashes (crashes) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6180-30-00, STH 21 from STH 116 to Leonard Point | Sand Pit Road Intersection STH 21 Left Turn Lanes | Sand Pit Predicted Crashes Left Turn Lanes | 0.1018 | 0.3907 | 1.0960 | 0.9686 | 5.7995 | 8.3567 |
| Total |  |  | 0.1018 | 0.3907 | 1.0960 | 0.9686 | 5.7995 | 8.3567 |

Table 15. Sand Pit Road Intersection STH 21 Left Turn Lanes Facility Type Crashes

| Facility Type | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating Injury (B) <br> Crashes (crashes) | Possible Injury <br> (C) Crashes <br> (crashes) | No Injury (O) <br> Crashes <br> (crashes) | Total Crashes <br> (crashes) |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Rural Two-Lane Intersection | 0.1018 | 0.3907 | 1.0960 | 0.9686 | 5.7995 | 8.3567 |
| Total | 0.1018 | 0.3907 | 1.0960 | 0.9686 | 5.7995 | 8.3567 |

## Sand Pit Road Roundabout Data

Case Title: Sand Pit Road Roundabout
Is Base Case: false
Present Value of Crash Cost: 809,019.74
Present Value of Other Cost: $900,000.00$

Table 16. Sand Pit Road Roundabout Evaluation Cost

| Project or Interchange | Selected Facility | Selected Evaluation | Present Value of <br> Crash Cost (\$) |
| :---: | :---: | :---: | :---: |
| 6180-30-00, STH 21 from STH 116 to Leonard <br> Point | Sand Pit Road Intersection Roundabout | Sand Pit Predicted Crashes Roundabout | $809,019.74$ |
| Total |  |  | $809,019.74$ |

Table 17. Sand Pit Road Roundabout Evaluation Crashes

| Project or Interchange | Selected Facility | Selected Evaluation | Fatal (K) Crashes (crashes) | Incapacitating Injury (A) Crashes (crashes) | Non-Incapacitating Injury (B) Crashes (crashes) | Possible Injury (C) Crashes (crashes) | $\begin{gathered} \text { No Injury (O) } \\ \text { Crashes } \\ \text { (crashes) } \end{gathered}$ | $\begin{array}{\|l\|} \text { Total Crashes } \\ \text { (crashes) } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6180-30-00, STH 21 from STH 116 to Leonard Point | Sand Pit Road Intersection Roundabout | Sand Pit Predicted Crashes Roundabout | 0.0191 | 0.1897 | 1.2204 | 1.5359 | 18.6452 | 21.6102 |
| Total |  |  | 0.0191 | 0.1897 | 1.2204 | 1.5359 | 18.6452 | 21.6102 |

Table 18. Sand Pit Road Intersection Roundabout Facility Type Crashes

| Facility Type | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating Injury (B) <br> Crashes (crashes) | Possible Injury <br> (C) Crashes <br> (crashes) | No Injury (O) <br> Crashes <br> (crashes) | Total Crashes <br> (crashes) |
| :---: | :---: | ---: | ---: | ---: | ---: | ---: |
| Roundabout | 0.0191 | 0.1897 | 1.2204 | 1.5359 | 18.6452 | 21.6102 |
| Total | 0.0191 | 0.1897 | 1.2204 | 1.5359 | 18.6452 | 21.6102 |

## Evaluation Message

## Wisconsin Department of Transportation Traffic Signal Warrant Summary Worksheet

The Worksheet(s) attached are provided as an attachment to the Engineering Investigation Study for:

Intersection: WIS 21 \& Sand Pit Road
County: Winnebago
Select one:

| Major Street: WIS 21 |  | Minor Street: Sand Pit Road |  |
| :--- | :---: | :--- | :--- |
| Critical Approach Speed: | 55 mph | Critical Approach Speed: | 55 mph |
| Lanes: | 1 lane |  | Lanes: |


| \% Right Turns Included | In built-up area of isolated community of < 10,000 population? Yes |
| :--- | ---: |
| From North (SB) $100 \%$ | Total number of approaches at intersection? 4 or more |
| From East (WB) $0 \%$ | If it is a "T" intersection, inflate minor threshold to $150 \%$ ? No |
| From South (NB) $100 \%$ | Manually set volume level? No |
| From West (EB) $0 \%$ |  |



| Warrant Evaluation Summary | Warrant Met: |
| :--- | :---: |
| Warrant 1: Eight - Hour Vehicular Volume | No |
| Condition A: Minimum Vehicular Volume <br> Condition B: Interruption of Continuous Traffic <br> Condition C: Combination: $80 \%$ of A and B | No |
| Warrant 2: Four-Hour Volume | No |
| Warrant 3: Peak Hour Volume | No |
| Warrant 4: Pedestrian Volume | No |
| Criterion A: Four-Hour | N/A |
| Warrant 5: School Crossing | N/A |
| Warrant 6: Coordinated Signal System | N/A |
| Warrant 7: Crash Experience | N/A |
| Warrant 8: Roadway Network | Yes |
| Warrant 9: Intersection Near a Grade Crossing | N/A |

## Warrant Analysis Conducted By:

Name: Randy Asman
Agency: WisDOT

Date: $1 / 23 / 2020$



# Warrant 4: Pedestrian Volume 

Warrant Evaluated?

Criterion A: Four Hour

| Hour <br> (Start) | Pedestrian <br> Volume | Major Road <br> Vol. |
| :---: | :---: | :---: |
|  |  | 0 |
|  |  | 0 |
|  |  | 0 |
|  |  | 0 |

Manually Set Major Rd Vol?
Avg. walk speed less than $3.5 \mathrm{ft} / \mathrm{s}$ ?

Criterion A Satisfied?

Criterion B: Peak Hour

| Peak Hour | Pedestrian <br> Vol. | Major Road <br> Vol. |
| :---: | :---: | :---: |
| $0: 00$ | 0 | 0 |

## Criterion B Satisfied?

Warrant Satisfied? N/A
Manually Set To:


Figure 4C-8 Warrant 4, Pedestrian Peak Hour (70\% Factor)


| $\cup \sim$ | 500 | 1000 | 1500 | 2000 |
| :---: | :---: | :---: | :---: | :---: |


| Warrant 5: School Crossing |  |  |  | 70\% |
| :---: | :---: | :---: | :---: | :---: |
|  | Warrant Evaluated? | Warrant Satisfied? N/A | Manually Set |  |
| Criteria |  |  |  | Fulfilled? |
| 1 | There are a MINIMUM of 20 school | hest crossing hour. |  |  |
| 2 | There are fewer adequate gaps in t using the crossing than the number | ream during the period whe period. | ool children are |  |
| 3 | The nearest traffic signal along the within 300 ft but the proposed traffic | ore than 300 ft away. Or, th t the progressive movemen | t traffic signal is c. |  |

# Warrant 6: Coordinated Signal System 

| Warrant Evaluated? $\quad$ Warrant Satisfied? N/A Manually Set To: |
| :--- |
| Criteria |
| 1 |$|$| Signal spacing > 1000 ft | Fulfilled? |
| :--- | :--- |
| 2 | On a one-way road or a road that has traffic predominantly in one direction, the adjacent signals are so far apart <br> that they do not provide the necessary degree of vehicle platooning. |
| 3 | On a two-way road, adjacent signals do not provide the necessary degree of platooning and the proposed and the <br> adjacent signals will collectively provide a progressive operation. |



## Warrant 8: Roadway Network



| 2 | Rural or suburban highway outside of, entering, or traversing a city |
| :--- | :--- |

3 Appears as a major route on an official plan

# Warrant 9: Intersection Near a Grade Crossing 

## Manually Set To:

| Adjustment Factors |  |  |  | Manually Set Peak Hour? |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rail Traffic <br> per Day | \% High Occupancy <br> Buses on Minor Road | \% Tractor-Trailer Trucks <br> on Minor Road | D | Peak Hour | Major <br> Road Vol. | Minor Road <br> Vol. | Adjusted <br> Minor Vol. |
| 1 | 0 | $0 \%$ to $2.5 \%$ | 660 | $16: 00$ | 980 | 48 | 16.08 |



Conclusions/Comments:

Updated: 12/6/2017

## HCS7 Two-Way Stop-Control Report

| General Information |  | Site Information |  |
| :--- | :--- | :--- | :--- |
| Analyst | CRF | Intersection | STH 21 and Sand Pit Rd |
| Agency/Co. | Westwood | Jurisdiction | WisDOT NE |
| Date Performed | $1 / 21 / 2021$ | East/West Street | STH 21 |
| Analysis Year | 2027 | North/South Street | Sand Pit Road |
| Time Analyzed | AM Peak Existing Geometry | Peak Hour Factor | 0.92 |
| Intersection Orientation | East-West | Analysis Time Period (hrs) | 0.25 |
| Project Description | STH 21, Omro - Oshkosh |  |  |

Lanes


## Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority | 1 U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |  | 7 | 8 | 9 |  | 10 | 11 | 12 |
| Number of Lanes | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 1 |  | 0 | 1 | 0 |  | 0 | 1 | 0 |
| Configuration |  | LT |  | R |  | LT |  | R |  |  | LTR |  |  |  | LTR |  |
| Volume (veh/h) |  | 4 | 557 | 14 |  | 6 | 262 | 11 |  | 6 | 14 | 4 |  | 83 | 46 | 13 |
| Percent Heavy Vehicles (\%) |  | 3 |  |  |  | 3 |  |  |  | 3 | 3 | 3 |  | 3 | 3 | 3 |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  |  |  |  |  | 0 |  |  |  | 0 |  |  |  |
| Right Turn Channelized | No |  |  |  | No |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \\| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Critical and Follow-up Headways

| Base Critical Headway (sec) | 4.1 |  |  |  | 4.1 |  |  |  | 7.1 | 6.5 | 6.2 |  | 7.1 | 6.5 | 6.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Critical Headway (sec) | 4.13 |  |  |  | 4.13 |  |  |  | 7.13 | 6.53 | 6.23 |  | 7.13 | 6.53 | 6.23 |
| Base Follow-Up Headway (sec) | 2.2 |  |  |  | 2.2 |  |  |  | 3.5 | 4.0 | 3.3 |  | 3.5 | 4.0 | 3.3 |
| Follow-Up Headway (sec) | 2.23 |  |  |  | 2.23 |  |  |  | 3.53 | 4.03 | 3.33 |  | 3.53 | 4.03 | 3.33 |

## Delay, Queue Length, and Level of Service



## HCS7 Two-Way Stop-Control Report

| General Information |  | Site Information |  |
| :--- | :--- | :--- | :--- |
| Analyst | CRF | Intersection | STH 21 and Sand Pit Rd |
| Agency/Co. | Westwood | Jurisdiction | WisDOT NE |
| Date Performed | $1 / 21 / 2021$ | East/West Street | STH 21 |
| Analysis Year | 2027 | North/South Street | Sand Pit Road |
| Time Analyzed | PM Peak Existing Geometry | Peak Hour Factor | 0.92 |
| Intersection Orientation | East-West | Analysis Time Period (hrs) | 0.25 |
| Project Description | STH 21, Omro - Oshkosh |  |  |

Lanes


## Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority | 1 U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |  | 7 | 8 | 9 |  | 10 | 11 | 12 |
| Number of Lanes | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 1 |  | 0 | 1 | 0 |  | 0 | 1 | 0 |
| Configuration |  | LT |  | R |  | LT |  | R |  |  | LTR |  |  |  | LTR |  |
| Volume (veh/h) |  | 16 | 436 | 10 |  | 11 | 527 | 86 |  | 7 | 34 | 12 |  | 30 | 22 | 6 |
| Percent Heavy Vehicles (\%) |  | 3 |  |  |  | 3 |  |  |  | 3 | 3 | 3 |  | 3 | 3 | 3 |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  |  |  |  |  | 0 |  |  |  | 0 |  |  |  |
| Right Turn Channelized | No |  |  |  | No |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Critical and Follow-up Headways

| Base Critical Headway (sec) | 4.1 |  |  |  | 4.1 |  |  |  | 7.1 | 6.5 | 6.2 |  | 7.1 | 6.5 | 6.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Critical Headway (sec) | 4.13 |  |  |  | 4.13 |  |  |  | 7.13 | 6.53 | 6.23 |  | 7.13 | 6.53 | 6.23 |
| Base Follow-Up Headway (sec) | 2.2 |  |  |  | 2.2 |  |  |  | 3.5 | 4.0 | 3.3 |  | 3.5 | 4.0 | 3.3 |
| Follow-Up Headway (sec) | 2.23 |  |  |  | 2.23 |  |  |  | 3.53 | 4.03 | 3.33 |  | 3.53 | 4.03 | 3.33 |

## Delay, Queue Length, and Level of Service

| Flow Rate, v (veh/h) | 17 |  |  |  | 12 |  |  |  |  | 58 |  |  |  | 63 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity, c (veh/h) | 918 |  |  |  | 1073 |  |  |  |  | 204 |  |  |  | 174 |  |
| v/c Ratio | 0.02 |  |  |  | 0.01 |  |  |  |  | 0.28 |  |  |  | 0.36 |  |
| 95\% Queue Length, Q ${ }_{95}$ (veh) | 0.1 |  |  |  | 0.0 |  |  |  |  | 1.1 |  |  |  | 1.5 |  |
| Control Delay (s/veh) | 9.0 |  |  |  | 8.4 |  |  |  |  | 29.5 |  |  |  | 37.1 |  |
| Level of Service (LOS) | A |  |  |  | A |  |  |  |  | D |  |  |  | E |  |
| Approach Delay (s/veh) |  | 0.5 |  |  |  | 0.3 |  |  |  | 29.5 |  |  |  | 37.1 |  |
| Approach LOS |  |  |  |  |  |  |  |  |  | D |  |  |  | E |  |

## HCS7 Two-Way Stop-Control Report

| General Information |  | Site Information |  |
| :--- | :--- | :--- | :--- |
| Analyst | CRF | Intersection | STH 21 and Sand Pit Rd |
| Agency/Co. | Westwood | Jurisdiction | WisDOT NE |
| Date Performed | $1 / 21 / 2021$ | East/West Street | STH 21 |
| Analysis Year | 2047 | North/South Street | Sand Pit Road |
| Time Analyzed | AM Peak Existing Geometry | Peak Hour Factor | 0.92 |
| Intersection Orientation | East-West | Analysis Time Period (hrs) | 0.25 |
| Project Description | STH 21, Omro - Oshkosh |  |  |

Lanes


## Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority | 1 U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |  | 7 | 8 | 9 |  | 10 | 11 | 12 |
| Number of Lanes | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 1 |  | 0 | 1 | 0 |  | 0 | 1 | 0 |
| Configuration |  | LT |  | R |  | LT |  | R |  |  | LTR |  |  |  | LTR |  |
| Volume (veh/h) |  | 5 | 583 | 16 |  | 7 | 276 | 14 |  | 7 | 19 | 4 |  | 103 | 64 | 16 |
| Percent Heavy Vehicles (\%) |  | 3 |  |  |  | 3 |  |  |  | 3 | 3 | 3 |  | 3 | 3 | 3 |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  |  |  |  |  | 0 |  |  |  | 0 |  |  |  |
| Right Turn Channelized | No |  |  |  | No |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Critical and Follow-up Headways

| Base Critical Headway (sec) | 4.1 |  |  |  | 4.1 |  |  |  | 7.1 | 6.5 | 6.2 |  | 7.1 | 6.5 | 6.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Critical Headway (sec) | 4.13 |  |  |  | 4.13 |  |  |  | 7.13 | 6.53 | 6.23 |  | 7.13 | 6.53 | 6.23 |
| Base Follow-Up Headway (sec) | 2.2 |  |  |  | 2.2 |  |  |  | 3.5 | 4.0 | 3.3 |  | 3.5 | 4.0 | 3.3 |
| Follow-Up Headway (sec) | 2.23 |  |  |  | 2.23 |  |  |  | 3.53 | 4.03 | 3.33 |  | 3.53 | 4.03 | 3.33 |

## Delay, Queue Length, and Level of Service



## HCS7 Two-Way Stop-Control Report

| General Information |  | Site Information |  |
| :--- | :--- | :--- | :--- |
| Analyst | CRF | Intersection | STH 21 and Sand Pit Rd |
| Agency/Co. | Westwood | Jurisdiction | WisDOT NE |
| Date Performed | $1 / 21 / 2021$ | East/West Street | STH 21 |
| Analysis Year | 2047 | North/South Street | Sand Pit Road |
| Time Analyzed | PM Peak Existing Geometry | Peak Hour Factor | 0.92 |
| Intersection Orientation | East-West | Analysis Time Period (hrs) | 0.25 |
| Project Description | STH 21, Omro - Oshkosh |  |  |

Lanes


## Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority | 1 U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |  | 7 | 8 | 9 |  | 10 | 11 | 12 |
| Number of Lanes | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 1 |  | 0 | 1 | 0 |  | 0 | 1 | 0 |
| Configuration |  | LT |  | R |  | LT |  | R |  |  | LTR |  |  |  | LTR |  |
| Volume (veh/h) |  | 21 | 458 | 12 |  | 13 | 547 | 107 |  | 9 | 47 | 14 |  | 36 | 31 | 8 |
| Percent Heavy Vehicles (\%) |  | 3 |  |  |  | 3 |  |  |  | 3 | 3 | 3 |  | 3 | 3 | 3 |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  |  |  |  |  | 0 |  |  |  | 0 |  |  |  |
| Right Turn Channelized | No |  |  |  | No |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \\| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Critical and Follow-up Headways

| Base Critical Headway (sec) | 4.1 |  |  |  | 4.1 |  |  |  | 7.1 | 6.5 | 6.2 |  | 7.1 | 6.5 | 6.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Critical Headway (sec) | 4.13 |  |  |  | 4.13 |  |  |  | 7.13 | 6.53 | 6.23 |  | 7.13 | 6.53 | 6.23 |
| Base Follow-Up Headway (sec) | 2.2 |  |  |  | 2.2 |  |  |  | 3.5 | 4.0 | 3.3 |  | 3.5 | 4.0 | 3.3 |
| Follow-Up Headway (sec) | 2.23 |  |  |  | 2.23 |  |  |  | 3.53 | 4.03 | 3.33 |  | 3.53 | 4.03 | 3.33 |

## Delay, Queue Length, and Level of Service



## HCS7 Two-Way Stop-Control Report

| General Information |  | Site Information |  |
| :--- | :--- | :--- | :--- |
| Analyst | CRF | Intersection | STH 21 and Sand Pit Rd |
| Agency/Co. | Westwood | Jurisdiction | WisDOT NE |
| Date Performed | $1 / 21 / 2021$ | East/West Street | STH 21 |
| Analysis Year | 2027 | North/South Street | Sand Pit Road |
| Time Analyzed | AM Peak LTLs | Peak Hour Factor | 0.92 |
| Intersection Orientation | East-West | Analysis Time Period (hrs) | 0.25 |
| Project Description | STH 21, Omro - Oshkosh |  |  |

## Lanes



## Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority | 1 U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |  | 7 | 8 | 9 |  | 10 | 11 | 12 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |  | 0 | 1 | 0 |  | 0 | 1 | 0 |
| Configuration |  | L | T | R |  | L | T | R |  |  | LTR |  |  |  | LTR |  |
| Volume (veh/h) |  | 4 | 557 | 14 |  | 6 | 262 | 11 |  | 6 | 14 | 4 |  | 83 | 46 | 13 |
| Percent Heavy Vehicles (\%) |  | 3 |  |  |  | 3 |  |  |  | 3 | 3 | 3 |  | 3 | 3 | 3 |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  |  |  |  |  | 0 |  |  |  | 0 |  |  |  |
| Right Turn Channelized | No |  |  |  | No |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Critical and Follow-up Headways

| Base Critical Headway (sec) | 4.1 |  |  |  | 4.1 |  |  |  | 7.1 | 6.5 | 6.2 |  | 7.1 | 6.5 | 6.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Critical Headway (sec) | 4.13 |  |  |  | 4.13 |  |  |  | 7.13 | 6.53 | 6.23 |  | 7.13 | 6.53 | 6.23 |
| Base Follow-Up Headway (sec) | 2.2 |  |  |  | 2.2 |  |  |  | 3.5 | 4.0 | 3.3 |  | 3.5 | 4.0 | 3.3 |
| Follow-Up Headway (sec) | 2.23 |  |  |  | 2.23 |  |  |  | 3.53 | 4.03 | 3.33 |  | 3.53 | 4.03 | 3.33 |

Delay, Queue Length, and Level of Service


| General Information |  | Site Information |  |
| :--- | :--- | :--- | :--- |
| Analyst | CRF | Intersection | STH 21 and Sand Pit Rd |
| Agency/Co. | Westwood | Jurisdiction | WisDOT NE |
| Date Performed | $1 / 21 / 2021$ | East/West Street | STH 21 |
| Analysis Year | 2027 | North/South Street | Sand Pit Road |
| Time Analyzed | PM Peak LTLs | Peak Hour Factor | 0.92 |
| Intersection Orientation | East-West | Analysis Time Period (hrs) | 0.25 |
| Project Description | STH 21, Omro - Oshkosh |  |  |

Lanes


## Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority | 1 U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |  | 7 | 8 | 9 |  | 10 | 11 | 12 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |  | 0 | 1 | 0 |  | 0 | 1 | 0 |
| Configuration |  | L | T | R |  | L | T | R |  |  | LTR |  |  |  | LTR |  |
| Volume (veh/h) |  | 16 | 436 | 10 |  | 11 | 527 | 86 |  | 7 | 34 | 12 |  | 30 | 22 | 6 |
| Percent Heavy Vehicles (\%) |  | 3 |  |  |  | 3 |  |  |  | 3 | 3 | 3 |  | 3 | 3 | 3 |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  |  |  |  |  | 0 |  |  |  | 0 |  |  |  |
| Right Turn Channelized | No |  |  |  | No |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \\| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Critical and Follow-up Headways

| Base Critical Headway (sec) | 4.1 |  |  |  | 4.1 |  |  |  | 7.1 | 6.5 | 6.2 |  | 7.1 | 6.5 | 6.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Critical Headway (sec) | 4.13 |  |  |  | 4.13 |  |  |  | 7.13 | 6.53 | 6.23 |  | 7.13 | 6.53 | 6.23 |
| Base Follow-Up Headway (sec) | 2.2 |  |  |  | 2.2 |  |  |  | 3.5 | 4.0 | 3.3 |  | 3.5 | 4.0 | 3.3 |
| Follow-Up Headway (sec) | 2.23 |  |  |  | 2.23 |  |  |  | 3.53 | 4.03 | 3.33 |  | 3.53 | 4.03 | 3.33 |

## Delay, Queue Length, and Level of Service



## HCS7 Two-Way Stop-Control Report

| General Information |  | Site Information |  |
| :--- | :--- | :--- | :--- |
| Analyst | CRF | Intersection | STH 21 and Sand Pit Rd |
| Agency/Co. | Westwood | Jurisdiction | WisDOT NE |
| Date Performed | $1 / 21 / 2021$ | East/West Street | STH 21 |
| Analysis Year | 2047 | North/South Street | Sand Pit Road |
| Time Analyzed | AM Peak LTLs | Peak Hour Factor | 0.92 |
| Intersection Orientation | East-West | Analysis Time Period (hrs) | 0.25 |
| Project Description | STH 21, Omro - Oshkosh |  |  |

Lanes


## Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority | 1U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |  | 7 | 8 | 9 |  | 10 | 11 | 12 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |  | 0 | 1 | 0 |  | 0 | 1 | 0 |
| Configuration |  | L | T | R |  | L | T | R |  |  | LTR |  |  |  | LTR |  |
| Volume (veh/h) |  | 5 | 583 | 16 |  | 7 | 276 | 14 |  | 7 | 19 | 4 |  | 103 | 64 | 16 |
| Percent Heavy Vehicles (\%) |  | 3 |  |  |  | 3 |  |  |  | 3 | 3 | 3 |  | 3 | 3 | 3 |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  |  |  |  |  | 0 |  |  |  | 0 |  |  |  |
| Right Turn Channelized | No |  |  |  | No |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Critical and Follow-up Headways

| Base Critical Headway (sec) | 4.1 |  |  |  | 4.1 |  |  |  | 7.1 | 6.5 | 6.2 |  | 7.1 | 6.5 | 6.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Critical Headway (sec) | 4.13 |  |  |  | 4.13 |  |  |  | 7.13 | 6.53 | 6.23 |  | 7.13 | 6.53 | 6.23 |
| Base Follow-Up Headway (sec) | 2.2 |  |  |  | 2.2 |  |  |  | 3.5 | 4.0 | 3.3 |  | 3.5 | 4.0 | 3.3 |
| Follow-Up Headway (sec) | 2.23 |  |  |  | 2.23 |  |  |  | 3.53 | 4.03 | 3.33 |  | 3.53 | 4.03 | 3.33 |

## Delay, Queue Length, and Level of Service



## HCS7 Two-Way Stop-Control Report

| General Information |  | Site Information |  |
| :--- | :--- | :--- | :--- |
| Analyst | CRF | Intersection | STH 21 and Sand Pit Rd |
| Agency/Co. | Westwood | Jurisdiction | WisDOT NE |
| Date Performed | $1 / 21 / 2021$ | East/West Street | STH 21 |
| Analysis Year | 2047 | North/South Street | Sand Pit Road |
| Time Analyzed | PM Peak LTLs | Peak Hour Factor | 0.92 |
| Intersection Orientation | East-West | Analysis Time Period (hrs) | 0.25 |
| Project Description | STH 21, Omro - Oshkosh |  |  |

Lanes


## Vehicle Volumes and Adjustments

| Approach | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Priority | 1 U | 1 | 2 | 3 | 4 U | 4 | 5 | 6 |  | 7 | 8 | 9 |  | 10 | 11 | 12 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |  | 0 | 1 | 0 |  | 0 | 1 | 0 |
| Configuration |  | L | T | R |  | L | T | R |  |  | LTR |  |  |  | LTR |  |
| Volume (veh/h) |  | 21 | 458 | 12 |  | 13 | 547 | 107 |  | 9 | 47 | 14 |  | 36 | 31 | 8 |
| Percent Heavy Vehicles (\%) |  | 3 |  |  |  | 3 |  |  |  | 3 | 3 | 3 |  | 3 | 3 | 3 |
| Proportion Time Blocked |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Grade (\%) |  |  |  |  |  |  |  |  | 0 |  |  |  | 0 |  |  |  |
| Right Turn Channelized | No |  |  |  | No |  |  |  |  |  |  |  |  |  |  |  |
| Median Type \| Storage | Undivided |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Critical and Follow-up Headways

| Base Critical Headway (sec) | 4.1 |  |  |  | 4.1 |  |  |  | 7.1 | 6.5 | 6.2 |  | 7.1 | 6.5 | 6.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Critical Headway (sec) | 4.13 |  |  |  | 4.13 |  |  |  | 7.13 | 6.53 | 6.23 |  | 7.13 | 6.53 | 6.23 |
| Base Follow-Up Headway (sec) | 2.2 |  |  |  | 2.2 |  |  |  | 3.5 | 4.0 | 3.3 |  | 3.5 | 4.0 | 3.3 |
| Follow-Up Headway (sec) | 2.23 |  |  |  | 2.23 |  |  |  | 3.53 | 4.03 | 3.33 |  | 3.53 | 4.03 | 3.33 |

Delay, Queue Length, and Level of Service


## SITE LAYOUT

$\nabla$ Site: 101 [AM 2027 Sand Pit (Site Folder: General)]
New Site
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT FLOWS FOR SITE (INPUT)

Approach movement input flow rates (veh/h)
All Movement Classes
$\forall$ Site: 101 [AM 2027 Sand Pit (Site Folder: General)]
New Site
Site Category: (None)
Roundabout

Use the button below to open or close all popup boxes. Click value labels to open selected ones.
Click and drag popup boxes to move to preferred positions.

## Close All Popups

iN


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## INPUT COMPARISON

Site A: 101 [AM 2027 Sand Pit (Site Folder: General)]
Site B:

| Intersection - Site Data |  |  |  |
| :--- | :--- | :--- | :--- |
| SITE |  |  |  |
|  | AM 2027 Sand Pit | No Difference |  |
| Intersection - Site Properties |  |  |  |
| SITE | AM 2027 Sand Pit | NA | Defaults - US HCM (Customary) |
|  |  |  |  |


| Intersection - Approach \& Exit Data |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Type | No. of App. <br> Lanes | No. of Exit Lanes | Approach Distance <br> ft | Extra Bunching (Site Analysis) \% | Extra Bunching (Network Analysis) \% | Exit Distance <br> ft | Approach Control | Area Type Factor |
| AM 2027 Sand Pit | South | $\begin{aligned} & \text { Sand Pit } \\ & \text { Rd } \end{aligned}$ | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | South | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| AM 2027 Sand Pit | East | STH 21 | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | East | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| AM 2027 Sand Pit | North | $\begin{aligned} & \text { Sand Pit } \\ & R d \end{aligned}$ | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | North | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| AM 2027 Sand Pit | West | STH 21 | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | West | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |


| Movement Definitions - Included Movement Classes |  | Model |  |
| :---: | :---: | :---: | :---: |
| SITE | Included | Name | ID |

Movement Definitions - Origin-Destination Movements

| SITE | To | Turn |
| :--- | :---: | :---: |
| Approach | OD Mov ID |  |
| No Difference | U-Turn Before Intersection | Exclude U-Turn Before Intersection From |
| Signal Analysis |  |  |

Lane Geometry - Lane Configuration

| SITE | Leg Item | Config | Type | Control | Slip/ <br> Bypass | Length Width Grade |  | Island |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | [ Front | Back | Fill | Cnct | For | Short |
|  |  |  |  |  | Control |  |  | Width | Width | Style | To | Ped | Strip |



| Lane Geometry - Lane Disciplines - Lane Change Data |  |  |  |
| :---: | :---: | :---: | :---: |
| SITE | Movement Class | \% Lane <br> Change to Left \% | \% Lane <br> Change to Right \% |

No Difference


| Lane Movements - Flow Proportions |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Exit Lane | South \% | To East $\%$ | eg North \% | West \% |
| Light Vehicles (LV) |  |  |  |  |  |
| From: South App. Lane 1 |  |  |  |  |  |
| AM 2027 Sand Pit | Exit Lane 1 | - | 100 | 100 | 100 |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | - | 100 | 100 |
| From: East App. Lane 1 |  |  |  |  |  |
| AM 2027 Sand Pit | Exit Lane 1 | 100 | - | 100 | 100 |
| Defaults - US HCM (Customary) | Exit Lane 1 | 100 | - | - | 100 |
| From: North App. Lane 1 |  |  |  |  |  |
| AM 2027 Sand Pit | Exit Lane 1 | 100 | 100 | - | 100 |
| Defaults - US HCM (Customary) | Exit Lane 1 | 100 | 100 | - | - |
| From: West App. Lane 1 |  |  |  |  |  |
| AM 2027 Sand Pit | Exit Lane 1 | 100 | 100 | 100 | - |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | 100 | 100 | - |
| Heavy Vehicles (HV) |  |  |  |  |  |
| From: South | App. Lane 1 |  |  |  |  |



Lane Movements - Blockage Calibration

|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Exit Lane | South | East | North | West |
| From: South | App. Lane 1 |  |  |  |  |
| AM 2027 Sand Pit | Exit Lane 1 | - | 1 | 1 | 1 |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | - | 1 | 1 |
| From: East | App. Lane 1 |  |  |  |  |
| AM 2027 Sand Pit | Exit Lane 1 | 1 | - | 1 | 1 |
| Defaults - US HCM (Customary) | Exit Lane 1 | 1 | - | - | 1 |
| From: North | App. Lane 1 |  |  |  |  |
| AM 2027 Sand Pit | Exit Lane 1 | 1 | 1 | - | 1 |
| Defaults - US HCM (Customary) | Exit Lane 1 | 1 | 1 | - | - |
| From: West | App. Lane 1 |  |  |  |  |
| AM 2027 Sand Pit | Exit Lane 1 | 1 | 1 | 1 | - |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | 1 | 1 | - |

## Roundabouts - Options

SITE

| Roundabouts - Geometry |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Circ. <br> Lanes | Circ. Width <br> ft | Island Diamete <br> ft | Inscribed Diameter <br> ft | Entry Radius <br> ft | Entry Angle | Raindrop Design | Circ <br> Trans Line | Downstre am Circ Lanes |
| AM 2027 Sand Pit | South | Sand Pit Rd | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | South | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| AM 2027 Sand Pit | East | STH 21 | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | East | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| AM 2027 Sand Pit | North | Sand Pit Rd | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | North | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| AM 2027 Sand Pit | West | STH 21 | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM (Customary) | West | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |


| HCM 2010 Roundabout Model Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Single Single Para. A | L.Circ: L.Entry Para. B | Single Multi <br> Para. A | L.Circ: .Entry <br> Para. B | Multi Single <br> Para. A | L.Circ: <br> L.Entry <br> Para. B | Multi Domina <br> Para. A | L.Circ: ant Lane Para. B | Multi Subdo La Para. A | L.Circ: minant ne Para. B |
| AM 2027 Sand Pit | South | Sand Pit Rd | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM <br> (Customary) | South | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| AM 2027 Sand Pit | East | STH 21 | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM (Customary) | East | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| AM 2027 Sand Pit | North | Sand Pit Rd | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM (Customary) | North | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| AM 2027 Sand Pit | West | STH 21 | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM (Customary) | West | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |




| Volumes - Volume Factors |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| SITE | To | Peak Flow | Flow | Growth |
|  | Approach | Factor | Scale | Rate |
|  | No Difference | $\%$ |  |  |
|  |  |  | \%/year |  |
|  |  |  |  |  |






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## MOVEMENT SUMMARY

바 Site: 101 [AM 2027 Sand Pit (Site Folder: General)]
New Site
Site Category: (None)
Roundabout


Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## $\square$ Site: 101 [AM 2027 Sand Pit (Site Folder: General)]

New Site
Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DEMAND FLOWS |  | Cap. <br> veh/h | Deg. Satn <br> v/c | Lane Util. \% | Aver. Delay <br> sec | Level of Service | 95\% BACK OF QUEUE |  | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. <br> Block. \% |
| South: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 26 | 3.0 | 681 | 0.038 | 100 | 5.7 | LOS A | 0.1 | 3.5 | Full | 1600 | 0.0 | 0.0 |
| Approach | 26 | 3.0 |  | 0.038 |  | 5.7 | LOS A | 0.1 | 3.5 |  |  |  |  |
| East: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 303 | 3.0 | 1311 | 0.231 | 100 | 4.7 | LOS A | 1.1 | 28.6 | Full | 1600 | 0.0 | 0.0 |
| Approach | 303 | 3.0 |  | 0.231 |  | 4.7 | LOS A | 1.1 | 28.6 |  |  |  |  |
| North: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 154 | 3.0 | 1007 | 0.153 | 100 | 5.0 | LOS A | 0.6 | 16.1 | Full | 1600 | 0.0 | 0.0 |
| Approach | 154 | 3.0 |  | 0.153 |  | 5.0 | LOS A | 0.6 | 16.1 |  |  |  |  |
| West: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 625 | 3.0 | 1166 | 0.536 | 100 | 9.3 | LOS A | 3.6 | 93.1 | Full | 1600 | 0.0 | 0.0 |
| Approach | 625 | 3.0 |  | 0.536 |  | 9.3 | LOS A | 3.6 | 93.1 |  |  |  |  |
| Intersection | 1109 | 3.0 |  | 0.536 |  | 7.4 | LOS A | 3.6 | 93.1 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

| Approach Lane Flows (veh/h) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Sand Pit Rd |  |  |  |  |  |  |  |  |  |
| Mov. <br> From S <br> To Exit: | L2 W | T1 N | R2 E | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 7 | 15 | 4 | 26 | 3.0 | 681 | 0.038 | 100 NA | NA |
| Approach | 7 | 15 | 4 | 26 | 3.0 |  | 0.038 |  |  |
| East: STH 21 |  |  |  |  |  |  |  |  |  |
| Mov. <br> From E <br> To Exit: | L2 S | T1 W | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 7 | 285 | 12 | 303 | 3.0 | 1311 | 0.231 | 100 NA | NA |
| Approach | 7 | 285 | 12 | 303 | 3.0 |  | 0.231 |  |  |


| North: Sand Pit Rd |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov. <br> From N To Exit: | L2 E | T1 S | R2 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 90 | 50 | 14 | 154 | 3.0 | 1007 | 0.153 | 100 NA | NA |
| Approach | 90 | 50 | 14 | 154 | 3.0 |  | 0.153 |  |  |
| West: STH 21 |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W <br> To Exit: | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov Lane No. |
| Lane 1 | 4 | 605 | 15 | 625 | 3.0 | 1166 | 0.536 | 100 NA | NA |
| Approach | 4 | 605 | 15 | 625 | 3.0 |  | 0.536 |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |
| Intersection | 1109 | 3.0 |  | 0.536 |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

| Merge Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \text { Exit } \\ \text { Lane } \\ \text { Number } \end{array}$ | Short Percent Opposing Lane Opng in Flow Rate Length Lane ft $\%$ veh/h pcu/h | Critical Gap sec | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h | Deg. Satn v/c |  | Merge Delay <br> sec |
| South Exit: Sand Pit Rd Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |
| East Exit: STH 21 <br> Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |
| North Exit: Sand Pit Rd Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |
| West Exit: STH 21 Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |

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## SITE LAYOUT

$\forall$ Site: 101 [PM 2027 Sand Pit (Site Folder: General)]
New Site
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT FLOWS FOR SITE (INPUT)

Approach movement input flow rates (veh/h)

## All Movement Classes

$\forall$ Site: 101 [PM 2027 Sand Pit (Site Folder: General)]
New Site
Site Category: (None)
Roundabout

Use the button below to open or close all popup boxes. Click value labels to open selected ones.
Click and drag popup boxes to move to preferred positions.

## Close All Popups

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## INPUT COMPARISON

Site A: 101 [PM 2027 Sand Pit (Site Folder: General)]
Site B:

| Intersection - Site Data |  |  |  |
| :--- | :--- | :--- | :--- |
| SITE | PM 2027 Sand Pit |  |  |
|  |  | No Difference |  |
|  |  |  |  |
| Intersection - Site Properties |  |  |  |
| SITE | PM 2027 Sand Pit | NA | Defaults - US HCM (Customary) |
|  |  |  |  |


| Intersection - Approach \& Exit Data |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Type | No. of App. Lanes | No. of Exit Lanes | Approach Distance <br> ft | Extra Bunching (Site Analysis) \% | Extra Bunching (Network Analysis) \% | Exit Distance $\qquad$ <br> ft | Approach Control | Area Type Factor |
| PM 2027 Sand Pit | South | $\begin{aligned} & \text { Sand Pit } \\ & R d \end{aligned}$ | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | South | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| PM 2027 Sand Pit | East | STH 21 | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | East | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| PM 2027 Sand Pit | North | Sand Pit $\mathrm{Rd}$ | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | North | $\underset{\mathrm{e}}{\text { RoadNam }}$ | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| PM 2027 Sand Pit | West | STH 21 | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | West | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |


| Movement Definitions - Included Movement Classes |  |  |
| :--- | :---: | :---: | :---: | :---: |
| $\left.\begin{array}{llll}\text { SITE } & \text { Included } & \text { Name } & \text { Model } \\ & & \text { No Difference } & \text { Designation } \\ & & \end{array}\right)$ |  |  |

Movement Definitions - Origin-Destination Movements

| SITE | To | Turn |
| :--- | :---: | :---: |
| Approach | OD Mov ID |  |
| No Difference | Exclude U-Turn Before Intersection From |  |
| Signal Analysis |  |  |

Lane Geometry - Lane Configuration

| SITE |  | Config | Type Control |  | Slip/ Bypass | Length Width Grade |  | Island |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Leg Item |  |  |  | [ Front |  |  | Back | Fill | Cnct | For | Short |
|  |  |  |  |  | Control |  |  | Width | Width | Style | To | Ped | Strip |



| Lane Geometry - Lane Disciplines - Lane Change Data |  |  |  |
| :---: | :---: | :---: | :---: |
| SITE | Movement Class | \% Lane <br> Change to Left \% | $\begin{gathered} \text { \% Lane } \\ \text { Change to Right } \\ \text { \% } \end{gathered}$ |

No Difference



| PM 2027 Sand Pit | Exit Lane 1 | - | 100 | 100 | 100 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | - | 100 | 100 |
| From: East | App. Lane 1 |  |  |  |  |
| PM 2027 Sand Pit | Exit Lane 1 | 100 | - | 100 | 100 |
| Defaults - US HCM (Customary) | Exit Lane 1 | 100 | - | - | 100 |
| From: North | App. Lane 1 |  |  |  |  |
| PM 2027 Sand Pit | Exit Lane 1 | 100 | 100 | - | 100 |
| Defaults - US HCM (Customary) | Exit Lane 1 | 100 | 100 | - | - |
| From: West | App. Lane 1 |  |  |  |  |
| PM 2027 Sand Pit | Exit Lane 1 | 100 | 100 | 100 | - |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | 100 | 100 | - |

## Lane Movements - Blockage Calibration

| SITE | Exit Lane | South | To Exit Leg |  | West |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | East | North |  |
| From: South | App. Lane 1 |  | 1 | 1 | 1 |
| PM 2027 Sand Pit | Exit Lane 1 | - |  |  |  |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | - | 1 | 1 |
| From: East App. Lane 1 | App. Lane 1 |  |  | 1 | 1 |
| PM 2027 Sand Pit | Exit Lane 1 | 1 | - |  |  |
| Defaults - US HCM (Customary) | Exit Lane 1 | 1 | - | - | 1 |
| From: North App. Lane 1 |  |  |  |  | 1 |
| PM 2027 Sand Pit | Exit Lane 1 | 1 | 1 | - |  |
| Defaults - US HCM (Customary) | Exit Lane 1 | 1 | 1 | - |  |
| From: West | App. Lane 1 |  |  |  |  |
| PM 2027 Sand Pit | Exit Lane 1 | 1 | 1 | 1 | - |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | 1 | 1 | - |

## Roundabouts - Options

| Roundabouts - Geometry |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Circ. <br> Lanes | Circ. Width | Island Diameter <br> ft | Inscribed Diameter <br> ft | Entry Radius <br> ft | Entry Angle | Raindrop Design | Circ Trans Line | $\begin{gathered} \text { Downstre } \\ \text { am } \\ \text { Circ } \\ \text { Lanes } \end{gathered}$ |
| PM 2027 Sand Pit | South | Sand Pit Rd | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM (Customary) | South | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| PM 2027 Sand Pit | East | STH 21 | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | East | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| PM 2027 Sand Pit | North | Sand Pit Rd | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | North | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| PM 2027 Sand Pit | West | STH 21 | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | West | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |


| HCM 2010 Roundabout Model Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Single Single Para. A | L.Circ: L.Entry Para. B | Single Multi <br> Para. A | L.Circ: .Entry <br> Para. B | Multi Single <br> Para. A | L.Circ: <br> L.Entry <br> Para. B | Multi Domina <br> Para. A | L.Circ: ant Lane Para. B | Multi Subdo La Para. A | L.Circ: minant ne Para. B |
| PM 2027 Sand Pit | South | Sand Pit Rd | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM <br> (Customary) | South | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| PM 2027 Sand Pit | East | STH 21 | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM <br> (Customary) | East | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| PM 2027 Sand Pit | North | Sand Pit Rd | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM (Customary) | North | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| PM 2027 Sand Pit | West | STH 21 | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM (Customary) | West | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |




| Volumes - Volume Factors |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| SITE | To Approach | Peak Flow Factor \% | Flow Scale \% | Growth Rate \%/year |


| Gap Acceptance - Gap Acceptance Data |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Opposed Movement | Critica Gap sec | Follow-up Headway sec | Minimum Departures veh/min | Exiting Flow Effect \% | \% Opp. By Nearest Lane \% | Opng. Peds (UnSig) |



| Parameter Settings - Cost |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Efficiency Parameters |  |  |  |  |  |  |  |
| SITE | Movement Class |  |  | Desired Speed | Lower Limit of Speed Efficiency for TTI |  |  |
|  | No Difference |  |  |  |  |  |  |
| Vehicle Cost Parameters |  |  |  |  |  |  |  |
| SITE | Movement Class | Veh Cost Method | Veh Operating Cost |  |  | Veh Time Cost |  |
|  |  |  | [ Pump Price of Fuel | Fuel Res. Cost Factor | Ratio of Running Cost to Fuel Cost ] | [Avg. Income | Time Value Factor ] |
|  |  |  | \$/Gal |  |  | \$/h |  |
| PM 2027 Sand Pit | Light Vehicles (LV) | Operating Cost | 2.3 | 0.7 | 3 | 27 | 0.4 |
| Defaults - US HCM (Customary) | Light Vehicles (LV) | Operating Cost | 2.5 | 0.7 | 3 | 29 | 0.4 |
| PM 2027 Sand Pit | Heavy Vehicles (HV) | Operating Cost | 2.3 | 0.7 | 3 | 27 | 0.4 |
| Defaults - US HCM (Customary) | Heavy Vehicles (HV) | Operating Cost | 2.5 | 0.7 | 3 | 29 | 0.4 |



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## MOVEMENT SUMMARY

$\forall$ Site: 101 [PM 2027 Sand Pit (Site Folder: General)]
New Site
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{ft} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver Speed <br> mph |
| South: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 L2 | 7 | 3.0 | 8 | 3.0 | 0.071 | 5.2 | LOS A | 0.3 | 6.8 | 0.51 | 0.43 | 0.51 | 34.8 |
| 8 T1 | 34 | 3.0 | 37 | 3.0 | 0.071 | 5.2 | LOS A | 0.3 | 6.8 | 0.51 | 0.43 | 0.51 | 34.7 |
| 18 R2 | 12 | 3.0 | 13 | 3.0 | 0.071 | 5.2 | LOS A | 0.3 | 6.8 | 0.51 | 0.43 | 0.51 | 33.7 |
| Approach | 53 | 3.0 | 58 | 3.0 | 0.071 | 5.2 | LOS A | 0.3 | 6.8 | 0.51 | 0.43 | 0.51 | 34.5 |
| East: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 11 | 3.0 | 12 | 3.0 | 0.536 | 8.8 | LOS A | 3.9 | 101.0 | 0.31 | 0.14 | 0.31 | 33.3 |
| 6 T1 | 527 | 3.0 | 573 | 3.0 | 0.536 | 8.8 | LOS A | 3.9 | 101.0 | 0.31 | 0.14 | 0.31 | 33.2 |
| 16 R2 | 86 | 3.0 | 93 | 3.0 | 0.536 | 8.8 | LOS A | 3.9 | 101.0 | 0.31 | 0.14 | 0.31 | 32.3 |
| Approach | 624 | 3.0 | 678 | 3.0 | 0.536 | 8.8 | LOS A | 3.9 | 101.0 | 0.31 | 0.14 | 0.31 | 33.1 |
| North: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 30 | 3.0 | 33 | 3.0 | 0.083 | 5.6 | LOS A | 0.3 | 7.9 | 0.54 | 0.48 | 0.54 | 33.5 |
| 4 T1 | 22 | 3.0 | 24 | 3.0 | 0.083 | 5.6 | LOS A | 0.3 | 7.9 | 0.54 | 0.48 | 0.54 | 33.4 |
| 14 R2 | 6 | 3.0 | 7 | 3.0 | 0.083 | 5.6 | LOS A | 0.3 | 7.9 | 0.54 | 0.48 | 0.54 | 32.5 |
| Approach | 58 | 3.0 | 63 | 3.0 | 0.083 | 5.6 | LOS A | 0.3 | 7.9 | 0.54 | 0.48 | 0.54 | 33.3 |
| West: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 L2 | 16 | 3.0 | 17 | 3.0 | 0.399 | 6.7 | LOS A | 2.4 | 60.2 | 0.26 | 0.12 | 0.26 | 34.3 |
| 2 T 1 | 436 | 3.0 | 474 | 3.0 | 0.399 | 6.7 | LOS A | 2.4 | 60.2 | 0.26 | 0.12 | 0.26 | 34.2 |
| 12 R 2 | 10 | 3.0 | 11 | 3.0 | 0.399 | 6.7 | LOS A | 2.4 | 60.2 | 0.26 | 0.12 | 0.26 | 33.2 |
| Approach | 462 | 3.0 | 502 | 3.0 | 0.399 | 6.7 | LOS A | 2.4 | 60.2 | 0.26 | 0.12 | 0.26 | 34.2 |
| All Vehicles | 1197 | 3.0 | 1301 | 3.0 | 0.536 | 7.7 | LOS A | 3.9 | 101.0 | 0.31 | 0.17 | 0.31 | 33.6 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: N:\3001091.00\Traffic\AnalysislSand Pit Rd\Roundabout|Sand Pit Rd.sip9

## LANE SUMMARY

## $\forall$ Site: 101 [PM 2027 Sand Pit (Site Folder: General)]

New Site
Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. $\qquad$ \% | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE [ Veh Dist ] |  | Lane Config | Lane Length | Cap. Adj. \% | Prob. Block. \% |
| South: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 58 | 3.0 | 808 | 0.071 | 100 | 5.2 | LOS A | 0.3 | 6.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 58 | 3.0 |  | 0.071 |  | 5.2 | LOS A | 0.3 | 6.8 |  |  |  |  |
| East: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 678 | 3.0 | 1266 | 0.536 | 100 | 8.8 | LOS A | 3.9 | 101.0 | Full | 1600 | 0.0 | 0.0 |
| Approach | 678 | 3.0 |  | 0.536 |  | 8.8 | LOS A | 3.9 | 101.0 |  |  |  |  |
| North: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 63 | 3.0 | 756 | 0.083 | 100 | 5.6 | LOS A | 0.3 | 7.9 | Full | 1600 | 0.0 | 0.0 |
| Approach | 63 | 3.0 |  | 0.083 |  | 5.6 | LOS A | 0.3 | 7.9 |  |  |  |  |
| West: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 502 | 3.0 | 1258 | 0.399 | 100 | 6.7 | LOS A | 2.4 | 60.2 | Full | 1600 | 0.0 | 0.0 |
| Approach | 502 | 3.0 |  | 0.399 |  | 6.7 | LOS A | 2.4 | 60.2 |  |  |  |  |
| Intersection | 1301 | 3.0 |  | 0.536 |  | 7.7 | LOS A | 3.9 | 101.0 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

| Approach Lane Flows (veh/h) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Sand Pit Rd |  |  |  |  |  |  |  |  |  |
| Mov. <br> From S <br> To Exit: | L2 W | T1 N | R2 E | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 8 | 37 | 13 | 58 | 3.0 | 808 | 0.071 | 100 NA | NA |
| Approach | 8 | 37 | 13 | 58 | 3.0 |  | 0.071 |  |  |
| East: STH 21 |  |  |  |  |  |  |  |  |  |
| Mov. <br> From E <br> To Exit: | L2 S | T1 W | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 12 | 573 | 93 | 678 | 3.0 | 1266 | 0.536 | 100 NA | NA |
| Approach | 12 | 573 | 93 | 678 | 3.0 |  | 0.536 |  |  |


| North: Sand Pit Rd |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov. <br> From N To Exit: | L2 E | T1 S | R2 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 33 | 24 | 7 | 63 | 3.0 | 756 | 0.083 | 100 NA | NA |
| Approach | 33 | 24 | 7 | 63 | 3.0 |  | 0.083 |  |  |
| West: STH 21 |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W To Exit: | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 17 | 474 | 11 | 502 | 3.0 | 1258 | 0.399 | 100 NA | NA |
| Approach | 17 | 474 | 11 | 502 | 3.0 |  | 0.399 |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |
| Intersection | 1301 | 3.0 |  | 0.536 |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

| Merge Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Short Percent Opposing Lane Opng in Flow Rate Length Lane <br> ft \% veh/h pcu/h | Critical Gap <br> sec | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h | Deg. Satn v/c |  | Merge Delay <br> sec |
| South Exit: Sand Pit Rd Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |
| East Exit: STH 21 Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |
| North Exit: Sand Pit Rd Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |
| West Exit: STH 21 <br> Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |

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## SITE LAYOUT

$\nabla$ Site: 101 [AM 2047 Sand Pit (Site Folder: General)]
New Site
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT FLOWS FOR SITE (INPUT)

Approach movement input flow rates (veh/h)
All Movement Classes

- Site: 101 [AM 2047 Sand Pit (Site Folder: General)]

New Site
Site Category: (None)
Roundabout

Use the button below to open or close all popup boxes. Click value labels to open selected ones.
Click and drag popup boxes to move to preferred positions.

## Close All Popups

iN


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## INPUT COMPARISON

Site A: 101 [AM 2047 Sand Pit (Site Folder: General)]
Site B:

| Intersection - Site Data |  |  |  |
| :--- | :--- | :--- | :--- |
| SITE |  |  |  |
|  | AM 2047 Sand Pit | No Difference |  |
| Intersection - Site Properties |  |  |  |
| SITE | AM 2047 Sand Pit | NA | Defaults - US HCM (Customary) |
|  |  |  |  |


| Intersection - Approach \& Exit Data |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Type | No. of App. <br> Lanes | No. of Exit Lanes | Approach Distance <br> ft | Extra Bunching (Site Analysis) \% | Extra Bunching (Network Analysis) \% | Exit Distance <br> ft | Approach Control | Area Type Factor |
| AM 2047 Sand Pit | South | $\begin{aligned} & \text { Sand Pit } \\ & \text { Rd } \end{aligned}$ | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | South | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| AM 2047 Sand Pit | East | STH 21 | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | East | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| AM 2047 Sand Pit | North | $\begin{aligned} & \text { Sand Pit } \\ & R d \end{aligned}$ | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | North | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| AM 2047 Sand Pit | West | STH 21 | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | West | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |


| Movement Definitions - Included Movement Classes |  |  |
| :--- | :---: | :---: | :---: | :---: |
| $\left.\begin{array}{llll}\text { SITE } & \text { Included } & \text { Name } & \text { Model } \\ & & \text { No Difference } & \text { Designation } \\ & & \end{array}\right)$ |  |  |

Movement Definitions - Origin-Destination Movements

| SITE | To | Turn |
| :--- | :---: | :---: |
| Approach | OD Mov ID |  |
| No Difference | U-Turn Before Intersection | Exclude U-Turn Before Intersection From |
| Signal Analysis |  |  |

Lane Geometry - Lane Configuration

| SITE | Leg Item | Config | Type | Control | Slip/ <br> Bypass | Length Width Grade |  | Island |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | [ Front | Back | Fill | Cnct | For | Short |
|  |  |  |  |  | Control |  |  | Width | Width | Style | To | Ped | Strip |



| Lane Geometry - Lane Disciplines - Lane Change Data |  |  |  |
| :---: | :---: | :---: | :---: |
| SITE | Movement Class | \% Lane <br> Change to Left \% | $\begin{gathered} \text { \% Lane } \\ \text { Change to Right } \\ \text { \% } \end{gathered}$ |

No Difference




Lane Movements - Blockage Calibration

| SITE | Exit Lane | South | To Exit Leg |  | West |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | East | North |  |
| From: South | App. Lane 1 |  | 1 |  |  |
| AM 2047 Sand Pit | Exit Lane 1 | - |  | 1 | 1 |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | - | 1 | 1 |
| From: East | App. Lane 1 |  |  |  |  |
| AM 2047 Sand Pit | Exit Lane 1 | 1 | - | 1 | 1 |
| Defaults - US HCM (Customary) | Exit Lane 1 | 1 | - | - | 1 |
| From: North | App. Lane 1 |  |  |  |  |
| AM 2047 Sand Pit | Exit Lane 1 | 1 | 1 | - | 1 |
| Defaults - US HCM (Customary) | Exit Lane 1 | 1 | 1 | - | - |
| From: West | App. Lane 1 |  |  |  |  |
| AM 2047 Sand Pit | Exit Lane 1 | 1 | 1 | 1 | - |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | 1 | 1 | - |

## Roundabouts - Options

SITE

| Roundabouts - Geometry |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Circ. <br> Lanes | Circ. Width <br> ft | Island Diamete <br> ft | Inscribed Diameter <br> ft | Entry Radius <br> ft | Entry Angle | Raindrop Design | Circ <br> Trans Line | Downstre am Circ Lanes |
| AM 2047 Sand Pit | South | Sand Pit Rd | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | South | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| AM 2047 Sand Pit | East | STH 21 | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | East | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| AM 2047 Sand Pit | North | Sand Pit Rd | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | North | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| AM 2047 Sand Pit | West | STH 21 | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM (Customary) | West | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |


| HCM 2010 Roundabout Model Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Single Single Para. A | L.Circ: L.Entry Para. B | Single Multi <br> Para. A | L.Circ: .Entry <br> Para. B | Multi Single <br> Para. A | L.Circ: <br> L.Entry <br> Para. B | Multi Domina <br> Para. A | L.Circ: ant Lane Para. B | Multi Subdo La Para. A | L.Circ: minant ne Para. B |
| AM 2047 Sand Pit | South | Sand Pit Rd | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM <br> (Customary) | South | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| AM 2047 Sand Pit | East | STH 21 | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM (Customary) | East | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| AM 2047 Sand Pit | North | Sand Pit Rd | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM (Customary) | North | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| AM 2047 Sand Pit | West | STH 21 | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM (Customary) | West | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |




| Volumes - Volume Factors |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| SITE | To Approach | Peak Flow Factor \% | Flow Scale \% | Growth Rate \%/year |


| Gap Acceptance - Gap Acceptance Data |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Opposed Movement | Critica Gap sec | Follow-up Headway sec | Minimum Departures veh/min | Exiting Flow Effect \% | \% Opp. By Nearest Lane \% | Opng. Peds (UnSig) |



| Parameter Settings - Cost |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Efficiency Parameters |  |  |  |  |  |  |  |
| SITE | Movement Class |  |  | Desired Speed | Lower Limit of Speed Efficiency for TTI |  |  |
|  | No Difference |  |  |  |  |  |  |
| Vehicle Cost Parameters |  |  |  |  |  |  |  |
| SITE | Movement Class | Veh Cost Method | Veh Operating Cost |  |  | Veh Time Cost |  |
|  |  |  | [ Pump Price of Fuel | Fuel Res. Cost Factor | Ratio of Running Cost to Fuel Cost ] | [Avg. Income | Time Value Factor ] |
|  |  |  | \$/Gal |  |  | \$/h |  |
| AM 2047 Sand Pit | Light Vehicles (LV) | Operating Cost | 2.3 | 0.7 | 3 | 27 | 0.4 |
| Defaults - US HCM (Customary) | Light Vehicles (LV) | Operating Cost | 2.5 | 0.7 | 3 | 29 | 0.4 |
| AM 2047 Sand Pit | Heavy Vehicles (HV) | Operating Cost | 2.3 | 0.7 | 3 | 27 | 0.4 |
| Defaults - US HCM (Customary) | Heavy Vehicles (HV) | Operating Cost | 2.5 | 0.7 | 3 | 29 | 0.4 |



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## MOVEMENT SUMMARY

바 Site: 101 [AM 2047 Sand Pit (Site Folder: General)]
New Site
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { ft } \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> mph |
| South: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 L2 | 7 | 3.0 | 8 | 3.0 | 0.050 | 6.1 | LOS A | 0.2 | 4.5 | 0.58 | 0.53 | 0.58 | 34.0 |
| 8 T1 | 19 | 3.0 | 21 | 3.0 | 0.050 | 6.1 | LOS A | 0.2 | 4.5 | 0.58 | 0.53 | 0.58 | 34.0 |
| 18 R2 | 4 | 3.0 | 4 | 3.0 | 0.050 | 6.1 | LOS A | 0.2 | 4.5 | 0.58 | 0.53 | 0.58 | 33.0 |
| Approach | 30 | 3.0 | 33 | 3.0 | 0.050 | 6.1 | LOS A | 0.2 | 4.5 | 0.58 | 0.53 | 0.58 | 33.8 |
| East: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 7 | 3.0 | 8 | 3.0 | 0.248 | 4.9 | LOS A | 1.2 | 31.2 | 0.14 | 0.05 | 0.14 | 35.3 |
| 6 T1 | 276 | 3.0 | 300 | 3.0 | 0.248 | 4.9 | LOS A | 1.2 | 31.2 | 0.14 | 0.05 | 0.14 | 35.2 |
| 16 R2 | 14 | 3.0 | 15 | 3.0 | 0.248 | 4.9 | LOS A | 1.2 | 31.2 | 0.14 | 0.05 | 0.14 | 34.2 |
| Approach | 297 | 3.0 | 323 | 3.0 | 0.248 | 4.9 | LOS A | 1.2 | 31.2 | 0.14 | 0.05 | 0.14 | 35.2 |
| North: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 103 | 3.0 | 112 | 3.0 | 0.201 | 5.6 | LOS A | 0.9 | 21.9 | 0.45 | 0.35 | 0.45 | 33.4 |
| 4 T1 | 64 | 3.0 | 70 | 3.0 | 0.201 | 5.6 | LOS A | 0.9 | 21.9 | 0.45 | 0.35 | 0.45 | 33.3 |
| 14 R2 | 16 | 3.0 | 17 | 3.0 | 0.201 | 5.6 | LOS A | 0.9 | 21.9 | 0.45 | 0.35 | 0.45 | 32.4 |
| Approach | 183 | 3.0 | 199 | 3.0 | 0.201 | 5.6 | LOS A | 0.9 | 21.9 | 0.45 | 0.35 | 0.45 | 33.3 |
| West: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 L2 | 5 | 3.0 | 5 | 3.0 | 0.587 | 10.6 | LOS B | 4.1 | 105.7 | 0.56 | 0.41 | 0.56 | 32.5 |
| 2 T1 | 583 | 3.0 | 634 | 3.0 | 0.587 | 10.6 | LOS B | 4.1 | 105.7 | 0.56 | 0.41 | 0.56 | 32.4 |
| 12 R 2 | 16 | 3.0 | 17 | 3.0 | 0.587 | 10.6 | LOS B | 4.1 | 105.7 | 0.56 | 0.41 | 0.56 | 31.5 |
| Approach | 604 | 3.0 | 657 | 3.0 | 0.587 | 10.6 | LOS B | 4.1 | 105.7 | 0.56 | 0.41 | 0.56 | 32.4 |
| All Vehicles | 1114 | 3.0 | 1211 | 3.0 | 0.587 | 8.1 | LOS A | 4.1 | 105.7 | 0.43 | 0.31 | 0.43 | 33.3 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## LANE SUMMARY

## $\sqrt{7}$ Site: 101 [AM 2047 Sand Pit (Site Folder: General)]

New Site
Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Cap. <br> veh/h | Deg. Satn <br> v/c | Lane Util. \% | Aver. Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \\ \text { Q } \\ \text { [ Veh } \end{gathered}$ | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | Cap. <br> Adj. <br> \% | Prob. <br> Block. <br> \% |
| South: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 33 | 3.0 | 648 | 0.050 | 100 | 6.1 | LOS A | 0.2 | 4.5 | Full | 1600 | 0.0 | 0.0 |
| Approach | 33 | 3.0 |  | 0.050 |  | 6.1 | LOS A | 0.2 | 4.5 |  |  |  |  |
| East: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 323 | 3.0 | 1301 | 0.248 | 100 | 4.9 | LOS A | 1.2 | 31.2 | Full | 1600 | 0.0 | 0.0 |
| Approach | 323 | 3.0 |  | 0.248 |  | 4.9 | LOS A | 1.2 | 31.2 |  |  |  |  |
| North: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 199 | 3.0 | 990 | 0.201 | 100 | 5.6 | LOS A | 0.9 | 21.9 | Full | 1600 | 0.0 | 0.0 |
| Approach | 199 | 3.0 |  | 0.201 |  | 5.6 | LOS A | 0.9 | 21.9 |  |  |  |  |
| West: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 657 | 3.0 | 1119 | 0.587 | 100 | 10.6 | LOS B | 4.1 | 105.7 | Full | 1600 | 0.0 | 0.0 |
| Approach | 657 | 3.0 |  | 0.587 |  | 10.6 | LOS B | 4.1 | 105.7 |  |  |  |  |
| Intersection | 1211 | 3.0 |  | 0.587 |  | 8.1 | LOS A | 4.1 | 105.7 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

| Approach Lane Flows (veh/h) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Sand Pit Rd |  |  |  |  |  |  |  |  |  |
| Mov. <br> From S <br> To Exit: | L2 W | T1 N | R2 E | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 8 | 21 | 4 | 33 | 3.0 | 648 | 0.050 | 100 NA | NA |
| Approach | 8 | 21 | 4 | 33 | 3.0 |  | 0.050 |  |  |
| East: STH 21 |  |  |  |  |  |  |  |  |  |
| Mov. <br> From E <br> To Exit: | L2 S | T1 W | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 8 | 300 | 15 | 323 | 3.0 | 1301 | 0.248 | 100 NA | NA |
| Approach | 8 | 300 | 15 | 323 | 3.0 |  | 0.248 |  |  |


| North: Sand Pit Rd |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov. <br> From N To Exit: | L2 E | T1 S | R2 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 112 | 70 | 17 | 199 | 3.0 | 990 | 0.201 | 100 NA | NA |
| Approach | 112 | 70 | 17 | 199 | 3.0 |  | 0.201 |  |  |
| West: STH 21 |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W To Exit: | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 5 | 634 | 17 | 657 | 3.0 | 1119 | 0.587 | 100 NA | NA |
| Approach | 5 | 634 | 17 | 657 | 3.0 |  | 0.587 |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |
| Intersection | 1211 | 3.0 |  | 0.587 |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

| Merge Analysis |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Short Percent Opposing Lane Opng in Flow Rate Length Lane <br> $\mathrm{ft} \quad \%$ veh/h pcu/h | Critical Gap sec | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h | Deg. Min. Satn Delay v/c sec | Merge Delay <br> sec |
| South Exit: Sand Pit Rd Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |
| East Exit: STH 21 Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |
| North Exit: Sand Pit Rd Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |
| West Exit: STH 21 <br> Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |

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## SITE LAYOUT

$\forall$ Site: 101 [PM 2047 Sand Pit (Site Folder: General)]
New Site
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT FLOWS FOR SITE (INPUT)

Approach movement input flow rates (veh/h)

## All Movement Classes

- Site: 101 [PM 2047 Sand Pit (Site Folder: General)]

New Site
Site Category: (None)
Roundabout

Use the button below to open or close all popup boxes. Click value labels to open selected ones.
Click and drag popup boxes to move to preferred positions.

## Close All Popups

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## INPUT COMPARISON

Site A: 101 [PM 2047 Sand Pit (Site Folder: General)]
Site B:
$\left.\begin{array}{|llll|}\hline \text { Intersection - Site Data } & & & \\ \hline \text { SITE } & \text { PM } 2047 \text { Sand Pit } & & \text { No Difference }\end{array}\right)$

| Intersection - Approach \& Exit Data |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Type | No. of App. Lanes | No. of Exit Lanes | Approach Distance <br> ft | Extra Bunching (Site Analysis) \% | Extra Bunching (Network Analysis) \% | Exit Distance $\qquad$ <br> ft | Approach Control | Area Type Factor |
| PM 2047 Sand Pit | South | $\begin{aligned} & \text { Sand Pit } \\ & R d \end{aligned}$ | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | South | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| PM 2047 Sand Pit | East | STH 21 | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | East | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| PM 2047 Sand Pit | North | Sand Pit $\mathrm{Rd}$ | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | North | $\underset{\mathrm{e}}{\text { RoadNam }}$ | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| PM 2047 Sand Pit | West | STH 21 | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |
| Defaults - US HCM <br> (Customary) | West | RoadNam e | Two Way | 1 | 1 | 1600.0 | 0 | - | - | Yield | - |


| Movement Definitions - Included Movement Classes |  |  |
| :--- | :---: | :---: | :---: | :---: |
| $\left.\begin{array}{llll}\text { SITE } & \text { Included } & \text { Name } & \text { Model } \\ & & \text { No Difference } & \text { Designation } \\ & & \end{array}\right)$ |  |  |

Movement Definitions - Origin-Destination Movements

| SITE | To | Turn |
| :--- | :---: | :---: |
| Approach | OD Mov ID |  |
| No Difference | Exclude U-Turn Before Intersection From |  |
| Signal Analysis |  |  |

Lane Geometry - Lane Configuration

| SITE | Leg Item | Config | Type | Control | Slip/ <br> Bypass | Length Width Grade |  | Island |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | [ Front | Back | Fill | Cnct | For | Short |
|  |  |  |  |  | Control |  |  | Width | Width | Style | To | Ped | Strip |



| Lane Geometry - Lane Disciplines - Lane Change Data |  |  |  |
| :---: | :---: | :---: | :---: |
| SITE | Movement Class | \% Lane <br> Change to Left \% | $\begin{gathered} \text { \% Lane } \\ \text { Change to Right } \\ \text { \% } \end{gathered}$ |

No Difference



| PM 2047 Sand Pit <br> Defaults - US HCM <br> (Customary) | Exit Lane 1 | Exit Lane 1 | - | 100 | 100 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 100 |  |  |  |  |  |

## Lane Movements - Blockage Calibration

| SITE | Exit Lane | South | To Exit Leg |  | West |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | East | North |  |
| From: South App. Lane 1 | App. Lane 1 |  | 1 | 1 | 1 |
| PM 2047 Sand Pit | Exit Lane 1 | - |  |  |  |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | - | 1 | 1 |
| From: East PM 2047 Sand Pit <br> Defaults - US HCM (Customary) | App. Lane 1 |  |  |  |  |
|  | Exit Lane 1 | 1 | - | 1 | 1 |
|  | Exit Lane 1 | 1 | - | - | 1 |
| From: North | App. Lane 1 |  |  |  |  |
| PM 2047 Sand Pit | Exit Lane 1 | 1 | 1 | - | 1 |
| Defaults - US HCM (Customary) | Exit Lane 1 | 1 | 1 | - | - |
| From: West | App. Lane 1 |  |  |  |  |
| PM 2047 Sand Pit | Exit Lane 1 | 1 | 1 | 1 | - |
| Defaults - US HCM (Customary) | Exit Lane 1 | - | 1 | 1 | - |

## Roundabouts - Options

| Roundabouts - Geometry |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Circ. <br> Lanes | Circ. Width | Island Diameter <br> ft | Inscribed Diameter <br> ft | Entry Radius <br> ft | Entry Angle | Raindrop Design | Circ Trans Line | $\begin{gathered} \text { Downstre } \\ \text { am } \\ \text { Circ } \\ \text { Lanes } \end{gathered}$ |
| PM 2047 Sand | South | Sand Pit Rd | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM (Customary) | South | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| PM 2047 Sand Pit | East | STH 21 | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | East | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| PM 2047 Sand Pit | North | Sand Pit Rd | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | North | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |
| PM 2047 Sand Pit | West | STH 21 | 1 | 20 | 100 | - | 100 | 30 | No | No | - |
| Defaults - US HCM <br> (Customary) | West | RoadName | 2 | 30 | 100 | - | 65 | 30 | No | No | - |


| HCM 2010 Roundabout Model Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Location | Name | Single <br> Single <br> Para. A | L.Circ: L.Entry Para. B | Single Multi <br> Para. A | L.Circ: .Entry <br> Para. B | Multi Single <br> Para. A | L.Circ: <br> L.Entry <br> Para. B | Multi Domina <br> Para. A | L.Circ: ant Lane Para. B | Multi Subdo La Para. A | L.Circ: minant ne Para. B |
| PM 2047 Sand Pit | South | Sand Pit Rd | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM <br> (Customary) | South | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| PM 2047 Sand Pit | East | STH 21 | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM <br> (Customary) | East | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| PM 2047 Sand Pit | North | Sand Pit Rd | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM (Customary) | North | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| PM 2047 Sand Pit | West | STH 21 | 1385 | $\begin{gathered} 0.00094 \\ 4 \end{gathered}$ | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |
| Defaults - US HCM (Customary) | West | RoadName | 1380 | 0.00102 | 1420 | 0.00091 | 1420 | 0.00085 | 1420 | 0.00085 | 1350 | $\begin{gathered} 0.0009 \\ 2 \end{gathered}$ |




| Volumes - Volume Factors |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| SITE | To Approach | Peak Flow Factor \% | Flow Scale \% | Growth Rate \%/year |


| Gap Acceptance - Gap Acceptance Data |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SITE | Opposed Movement | Critica Gap sec | Follow-up Headway sec | Minimum Departures veh/min | Exiting Flow Effect \% | \% Opp. By Nearest Lane \% | Opng. Peds (UnSig) |



| Parameter Settings - Cost |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Efficiency Parameters |  |  |  |  |  |  |  |
| SITE | Movement Class |  |  | Desired Speed | Lower Limit of Speed Efficiency for TTI |  |  |
|  | No Difference |  |  |  |  |  |  |
| Vehicle Cost Parameters |  |  |  |  |  |  |  |
| SITE | Movement Class | Veh Cost Method | Veh Operating Cost |  |  | Veh Time Cost |  |
|  |  |  | [ Pump Price of Fuel | Fuel Res. Cost Factor | Ratio of Running Cost to Fuel Cost ] | [Avg. Income | Time Value Factor ] |
|  |  |  | \$/Gal |  |  | \$/h |  |
| PM 2047 Sand Pit | Light Vehicles (LV) | Operating Cost | 2.3 | 0.7 | 3 | 27 | 0.4 |
| Defaults - US HCM (Customary) | Light Vehicles (LV) | Operating Cost | 2.5 | 0.7 | 3 | 29 | 0.4 |
| PM 2047 Sand Pit | Heavy Vehicles (HV) | Operating Cost | 2.3 | 0.7 | 3 | 27 | 0.4 |
| Defaults - US HCM (Customary) | Heavy Vehicles (HV) | Operating Cost | 2.5 | 0.7 | 3 | 29 | 0.4 |



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## MOVEMENT SUMMARY

$\forall \sqrt{ } \sqrt{ }$ Site: 101 [PM 2047 Sand Pit (Site Folder: General)]
New Site
Site Category: (None)
Roundabout


Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: N:\3001091.00\Traffic\AnalysislSand Pit Rd\Roundabout|Sand Pit Rd.sip9

## LANE SUMMARY

## $\forall$ Site: 101 [PM 2047 Sand Pit (Site Folder: General)]

New Site
Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Cap. <br> veh/h | Deg. Satn <br> v/c | Lane Util. \% | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Lane Config | Lane Length ft | Cap. <br> Adj. <br> \% | Prob. Block. \% |
| South: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 76 | 3.0 | 780 | 0.098 | 100 | 5.6 | LOS A | 0.4 | 9.3 | Full | 1600 | 0.0 | 0.0 |
| Approach | 76 | 3.0 |  | 0.098 |  | 5.6 | LOS A | 0.4 | 9.3 |  |  |  |  |
| East: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 725 | 3.0 | 1240 | 0.585 | 100 | 9.8 | LOS A | 4.6 | 117.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 725 | 3.0 |  | 0.585 |  | 9.8 | LOS A | 4.6 | 117.8 |  |  |  |  |
| North: Sand Pit Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 82 | 3.0 | 737 | 0.111 | 100 | 6.0 | LOS A | 0.4 | 10.5 | Full | 1600 | 0.0 | 0.0 |
| Approach | 82 | 3.0 |  | 0.111 |  | 6.0 | LOS A | 0.4 | 10.5 |  |  |  |  |
| West: STH 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane ${ }^{\text {d }}$ | 534 | 3.0 | 1236 | 0.432 | 100 | 7.3 | LOS A | 2.6 | 67.4 | Full | 1600 | 0.0 | 0.0 |
| Approach | 534 | 3.0 |  | 0.432 |  | 7.3 | LOS A | 2.6 | 67.4 |  |  |  |  |
| Intersection | 1416 | 3.0 |  | 0.585 |  | 8.4 | LOS A | 4.6 | 117.8 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

| Approach Lane Flows (veh/h) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Sand Pit Rd |  |  |  |  |  |  |  |  |  |
| Mov. <br> From S <br> To Exit: | L2 W | T1 N | R2 E | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 10 | 51 | 15 | 76 | 3.0 | 780 | 0.098 | 100 NA | NA |
| Approach | 10 | 51 | 15 | 76 | 3.0 |  | 0.098 |  |  |
| East: STH 21 |  |  |  |  |  |  |  |  |  |
| Mov. <br> From E <br> To Exit: | L2 S | T1 W | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 14 | 595 | 116 | 725 | 3.0 | 1240 | 0.585 | 100 NA | NA |
| Approach | 14 | 595 | 116 | 725 | 3.0 |  | 0.585 |  |  |


| North: Sand Pit Rd |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov. <br> From N To Exit: | L2 E | T1 S | R2 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 39 | 34 | 9 | 82 | 3.0 | 737 | 0.111 | 100 NA | NA |
| Approach | 39 | 34 | 9 | 82 | 3.0 |  | 0.111 |  |  |
| West: STH 21 |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W To Exit: | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 23 | 498 | 13 | 534 | 3.0 | 1236 | 0.432 | 100 NA | NA |
| Approach | 23 | 498 | 13 | 534 | 3.0 |  | 0.432 |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |
| Intersection | 1416 | 3.0 |  | 0.585 |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

| Merge Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Short Percent Opposing Lane Opng in Flow Rate Length Lane <br> ft \% veh/h pcu/h | Critical Gap <br> sec | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h | Deg. Satn v/c |  | Merge Delay <br> sec |
| South Exit: Sand Pit Rd Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |
| East Exit: STH 21 Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |
| North Exit: Sand Pit Rd Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |
| West Exit: STH 21 <br> Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |  |

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